# HP $11729 C$ <br> CARRIER NOISE TEST SET (Including Options 003, 007,011,015,019, 023, 027, 130 and 140) 

## SERIAL NUMBERS

This manual applies directly to instruments with serial numbers prefixed 2509A.

For additional importantinformation about serial numbers, see INSTRUMENTS COVERED BY THIS MANUAL in Section I.

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## SAFETY CONSIDERATIONS

## GENERAL

This product and related documentation must be reviewed for familiarization with safety markings and instructions before operation.

This product is a Safety Class I instrument (provided with a protective earth terminal).

## BEFORE APPLYING POWER

Verify that the product is set to match the available line voltage and the correct fuse is installed.

## SAFETY EARTH GROUND

An uninterruptible safety earth ground must be provided from the main power source to the product input wiring terminals, power cord, or supplied power cord set.

## WARNINGS

Any interruption of the protective (grounding) conductor (inside or outside the instrument) or disconnecting the protective earth terminal will cause a potential shock hazard that could result in personal injury. (Grounding one conductor of a two conductor outlet is not sufficient protection.) In addition, verify that a common ground exists between the unit under test and this instrument prior to energizing either unit.

Whenever it is likely that the protection has been impaired, the instrument must be made inoperative and be secured against any unintended operation.

If this instrument is to be energized via an autotransformer (for voltage reduction) make sure the common terminal is connected to neutral (that is, the grounded side of the mains supply).

Servicing instructions are for use by servicetrained personnel only. To avoid dangerous electric shock, do not perform any servicing unless qualified to do so.

Adjustments described in the manual are performed with power supplied to the instrument
while protective covers are removed. Energy available at many points may, if contacted, result in personal injury.

Capacitors inside the instrument may still be charged even if the instrument has been disconnected from its source of supply.

For continued protection against fire hazard, replace the line fuse(s) only with 250 V fuse(s) of the same current rating and type (for example, normal blow, time delay, etc.). Do not use repaired fuses or short circuited fuseholders.

## SAFETY SYMBOLS



Instruction manual symbol: the product will be marked with this symbol when it is necessary for the user to refer to the instruction manual (see Table of Contents for page references).
 Indicates hazardous voltages.
$\underset{=}{\perp}$ Indicates earth (ground) terminal.

WARNING


The WARNING sign denotes a hazard. It calls attention to a procedure, practice, or the like, which, if not correctly performed or adhered to, could result in personal injury. Do not proceed beyond a WARNING sign until the indicated conditions are fully understood and met.

The CAUTION sign denotes a hazard. It calls attention to an operating procedure, practice, or the like, which, if not correctly performed or adhered to, could result in damage to or destruction of part or all of the product. Do not proceed beyond a CAUTION sign until the indicated conditions are fully understood and met.

## CONTENTS

Section I
GENERAL INFORMATION
Introduction ..... 1-1
Specifications ..... 1-1
Safety Considerations ..... 1-1
Instruments Covered by This Manual ..... 1-1
Manual Changes Supplement ..... 1-1
Description ..... 1-1
Options ..... 1-2
Electrical Options ..... 1-2
Mechanical Options ..... 1-3
Accessories Supplied ..... 1-3
Equipment Required But Not Supplied ..... 1-3
Electrical Equipment Available ..... 1-7
Recommended Test Equipment ..... 1-7
Section II
INSTALLATION
Introduction ..... 2-1
Initial Inspection ..... 2-1
Preparation For Use ..... 2-1
Power Requirements ..... 2-1
Line Voltage and Fuse Selection ..... 2-1
Power Cables ..... 2-1
HP-IB Address Selection ..... 2-2
Interconnections ..... 2-3
Mating Connectors ..... 2-3
Operating Environment ..... 2-5
Bench Operation ..... 2-5
Rack Mounting ..... 2-5
Storage and Shipment ..... 2-5
Environment ..... 2-5
Packaging ..... 2-5
Section III
OPERATION
Introduction ..... 3-1
Local Operation ..... 3-1
Remote Operation (HP-IB) ..... 3-1
Operator's Checks ..... 3-1
Operator's Maintenance ..... 3-1
Operator's Checks ..... 3-7
General Operating Instructions ..... 3-14
Turn On ..... 3-14
Phase Noise Measurement ..... 3-14
Phase Detector Method ..... 3-14
Frequency Discriminator Method ..... 3-22
AM Measurement (Option 130 only) ..... 3-25
Section IV
PERFORMANCE TESTS
Introduction ..... 4-1
Equipment Required ..... 4-1
Test Record ..... 4-1
Calib ation Cycle ..... 4-1
Page Page
Measurement Frequency Range,IF Output Bandwidth andLevel Performance Tests4-1
Residual Phase Noise Performance Test
(Using a test signal less than 1280 MHz ) ..... 4-4
Residual Phase Noise Performance Test
(Using a test signal of 10 GHz ) ..... 4-9
AM Noise Floor Performance Test ..... 4-14
Section V
ADJUSTMENTS
Introduction ..... 5-1
Safety Considerations ..... 5-1
Equipment Required ..... 5-1
Factory Selected Components ..... 5-1
Related Adjustments ..... 5-1
Power Supply Adjustment ..... 5-2
Phase Lock Indicator Adjustment ..... 5-3
Option Switch Adjustment ..... 5-8
Pulse Balance Adjustment ..... 5-10
Section VI REPLACEABLE PARTS
Introduction ..... 6-1
Abbreviations ..... 6-1
Replaceable Parts List ..... 6-1
Factory Selected Parts (*) ..... 6-1
Parts List Backdating ( $\dagger$ ) ..... 6-1
Parts List Updating (Change Sheet) ..... 6-1
Illustrated Parts Breakdown ..... 6-1
Hardware ..... 6-1
Ordering Information ..... 6-1
Recommended Spares List ..... 6-2
Section VII
REPLACEABLE PARTS
Introduction ..... 7-1
Section VIII
REPLACEABLE PARTS
Introduction ..... 8-1
Service Sheets ..... 8-1
Block Diagrams ..... 8-1
Schematics ..... 8-1
Safety Considerations ..... 8-1
Before Applying Power ..... 8-1
Safety ..... 8-1
Recommended Test Equipment ..... 8-1
Service Tools, Aids and Information ..... 8-1
Pozidriv Screwdrivers ..... 8-1
Tuning Tools ..... 8-2
Heat Staking Tools ..... 8-2
Hardware ..... 8-2
Maintenance ..... 8-2

## CONTENTS (cont'd)

Page Page
Appendix A ..... A-1
Phase Noise Measurement Correction Factors
Normalization to 1 Hz Equivalent Noise Bandwidth ..... A-1
Calibration Attenuation ..... A-2
$\mathcal{L}_{\mathrm{f}}$ Conversion Factor ..... A-2
Correction for Log Amplifiers and Peak
Detectors in Analog Spectrum Analyzers ..... A-3
Frequency Discriminator Correction Factor ..... A-3
Appendix B ..... B-1
Phase Lock Loop Characterization

## ILLUSTRATIONS

Figure Page
1-1. HP Model 11729C Carrier Noise
Test Set with Accessories Supplied ..... 1-0
2-1. Line Voltage and Fuse Selection ..... 2-2
2-2. Power Cable and Mains Plug Part Numbers ..... 2-2
2-3. Hewlett-Packard Interface Bus
Connection ..... 2-4
3-1. Front Panel Features ..... 3-2
3-2. Rear Panel Features ..... 3-5
3-3. Basic Functional Checks Test Setup ..... 3-7
3-4. Interconnections to the Carrier Noise Test Set when making a Phase Noise Measurement (Using the Phase Detector Method ..... 3-15
3-5. Spectrum Analyzer Displays Used for Acquiring Phase Lock (Quadrature) ..... 3-19
3-6. Front Panel Phase Lock (Quadrature) Indicator ..... 3-20
3-7. Interconnections to the Carrier Noise Test Set When Making a Phase Noise Mea- surement (Using the Frequency Discriminator Method) ..... 3-22
3-8. Interconnections to the Carrier Noise Test Set When Making an AM Noise Measurement ..... 3-25
4-1. Measurement Frequency Range, IF Output Bandwidth and Level Test Setup ..... 4-2
4-2. Residual Phase Noise Test Setup (Using a Test Signal of Less Than 1280 MHz) ..... 4-5
4-3. Residual Phase Noise Test Setup (Using a Test Signal of 10 GHz ) ..... 4-10
4-4. AM Noise Floor Test Setup ..... 4-15
$5-1 . \quad+5.0$ Vdc Power Supply Adjustment Setup ..... 5-2
5-2. Phase Lock Indicator Adjustment Setup ..... 5-3
6-1. External Mechanical Parts ..... 6-19
6-2. Chassis Parts ..... 6-21
6-3. Front Panel Parts ..... 6-23
Figure Page
6-4. Rear Panel Parts ..... 6-25
6-5. Switch Assembly Mechanical Parts ..... 6-27
6-6. Power Supply and Low Noise Amplifier Mechanical Parts ..... 6-29
6-7. A9 Assembly Mechanical Parts ..... 6-31
8-1. Overall Functional Block Diagram ..... 8-17
8-2. Reference Up-Conversion, Test Signal Down-Conversion and Phase Detecting Assembly Component Locations ..... 8-19
8-3. Reference Up-Conversion, Test Signal Down-Conversion and Phase Detecting Circuits Schematic Diagram ..... 8-19
8-4. Front Panel Key and Display Board Assembly Component Locations ..... 8-20
8-5. Low Pass Filter Board Assembly Component Locations ..... 8-20
8-6. Low Noise Amplifier Assembly Component Locations ..... 8-21
8-7. Low Pass Filter and Low Noise Amplifier Schematic Diagrams ..... 8-21
8-8. Phase Lock Board Troubleshooting Test Setup ..... 8-22
8-9. Indicator Board Assembly Component Locations ..... 8-23
8-10. Phase Lock Board Assembly Component Locations ..... 8-23
8-11. Phase Lock Circuit Schematic Diagram ..... 8-23
8-12. Simplified HP-IB Handshake between a Talker (Computer Controller) and One Listener (Carrier Noise Test Set) ..... 8-24
8-13. Indicator Board Assembly Component Locations ..... 8-24
8-14. HP-IB Interconnect Board Assembly Component Locations ..... 8-25
8-15. Front Panel Key and Display Board Assembly Component Locations ..... 8-25
8-16. Microprocessor Board Assembly Component Locations ..... 8-27
8-17. Data Input Circuit Schematic Diagram ..... 8-27
8-18. HP-IB Interconnect Board Assembly Component Locations ..... 8-30

## ILLUSTRATIONS (cont'd)

FigurePage
8-19. Microprocessor Board Assembly Component Locations ..... 8-31
8-20. Data Processing Circuits Schematic Diagram ..... 8-31
8-21. Front Panel Key and Display Board Assembly Component Locations ..... 8-34
8-22. Microprocessor Board Assembly Component Locations ..... 8-35
8-23. Switch and LED Control Circuits Schematic Diagram ..... 8-35
Figure Page
8-24. Power Supply Board Assembly Component Locations ..... 8-37
8-25. Power Supply Circuits
Schematic Diagram ..... 8-37
APPENDIX B
B-1. Typical Phase Lock Loop Filter
Transfer Characteristic ..... B-2
TABLES
Table Page Table ..... Page
1-1. Specifications ..... 1-4
1-2. Supplemental Characteristics ..... 1-6
1-3. System Specifications ..... 1-8
1-4. Recommended Test Equipment ..... 1-10
1-5. Recommended Alternate
Test Equipment ..... 1-12
2-1. Allowable HP-IB Address Codes ..... 2-3
3-1. IF Output Check ..... 3-9
3-2. Status Bits and Their Decimal Equivalents for Two Phase Lock Conditions ..... 3-12
3-3. HP-IB Message Reference Table ..... 3-27
3-4. HP-IB Program Codes ..... 3-29
3-5. Allowable HP-IB Address Codes ..... 3-30
4-1. IF Output Level ..... 4-3
4-2. Performance Test Record ..... 4-18
5-1. Phase Lock and Unlock Status Bits ..... 5-7
5-2. Definition of Option Switch S1 ..... 5-8
6-1. Reference Designations and Abbreviations ..... 6-3
6-2. Replaceable Parts ..... 6-5
6-3. Code List of Manufacturers ..... 6-35
8-1. Etched Circuit Soldering Equipment ..... 8-2
8-2. Schematic Diagram Notes ..... 8-3
8 -3. Signatures for Verifying Address Decoding ..... 8-24
8-4. Signatures for Verifying Microprocessor and Input/Output Operation ..... 8-24
$8-5$. Signatures for Verifying Address Decoding ..... 8-28
8-6. Signatures for Verifying ROM Operation and Data Stored in ROM ..... 8-28
8-7. Signatures for Verifying Microprocessor, ROM, RAM and Data Buffer Operation ..... 8-29
8-8. Signatures Verifying Address Decoding Using a Falling Edge Clock Trigger ..... 8-32
8-9. Signatures Verifying Address Decoding Using a Rising Edge Clock Trigger ..... 8-32
8-10. Signatures Verifying Microprocessor and Relay Circuitry Operation ..... 8-32


CABLE AND ATTENUATOR
Cable-attenuator assembly used to configure the internal 640 MHz oscillator.


SMA TERMINATION


## BNC TERMINATION

The $50 \Omega$ termination is installed on the IF OUTPUT port as shown in the photograph.

Figure 1-1. HP Model 11729C Carrier Noise Test Set with Accessories Supplied

# SECTION I <br> GENERAL INFORMATION 

## 1-1. INTRODUCTION

This manual contains information required to install, operate, test, adjust and service the HewlettPackard Model 11729C Carrier Noise Test Set. Figure 1-1 shows the Carrier Noise Test Set with all of its externally supplied accessories.
The Carrier Noise Test Set Operating and Service manual has eight sections. The subjects addressed are:

Section I, General Information
Section II, Installation
Section III, Operation
Section IV, Performance Tests
Section V, Adjustments
Section VI, Replaceable Parts
Section VII, Manual Changes
Section VIII, Service
Listed on the title page of this manual, below the manual part number, is a microfiche part number. This number may be used to order $100 \times 150$ millimetre ( $4 \times 6 \mathrm{inch}$ ) microfilm transparencies of this manual. Each microfiche contains up to 96 photoduplicates of the manual pages. The microfiche package also includes the latest Manual Changes supplement, as well as all pertinent Service Notes.

## 1-2. SPECIFICATIONS

Instrument specifications are listed in Table 1-1. These specifications are the performance standards or limits against which the instrument may be tested. Supplemental characteristics are listed in Table 1-2. Supplemental characteristics are not warranted specifications, but are typical characteristics included as additional information for the user. Typical system performance when using the Carrier Noise Test Set with the HP 8662A or 8663A is given in Table 1-3.

## 1-3. SAFETY CONSIDERATIONS

This product is a Safety Class I instrument, that is, one provided with a protective earth terminal. The Carrier Noise Test Set and all related documentation should be reviewed for familiarization with safety markings and instructions before operation. Refer to the Safety Considerations page found at the beginning of this manual for a summary of the safety information. Safety information for installation, operation, performance testing, adjustment, or service is found in appropriate places throughout this manual.

## 1-4. INSTRUMENTS COVERED BY THIS MANUAL

Attached to the rear panel of the instrument is a serial number plate. The serial number is in the form: 0000 A 00000 . The first four digits and the letter are the serial number prefix. The last five digits are the suffix. The prefix is the same for identical instruments; it changes only when a configuration change is made to the instrument. The suffix however, is assigned sequentially and is different for each instrument. The contents of this manual apply directly to instruments having the serial number prefix(es) listed under SERIAL NUMBERS on the title page.

## 1-5. MANUAL CHANGES SUPPLEMENT

An instrument manufactured after the printing of this manual may have a serial number prefix that is not listed on the title page. This unlisted serial number prefix indicates that the instrument is different from those documented in this manual. The manual for this newer instrument is accompanied by a Manual Changes supplement. The supplement contains "change information" that explains how to adapt this manual to the newer instrument.
In addition to change information, the supplement may contain information for correcting errors in the manual. To keep the manual as current and as accurate as possible, Hewlett-Packard recommends that you periodically request the latest Manual Changes supplement. The supplement is identified with the manual print date and part number, both of which appear on the manual title page. Complimentary copies of the supplement are available from Hewlett-Packard.

For information concerning a serial number prefix that is not listed on the title page or in the Manual Changes supplement, contact your nearest Hewlett-Packard office.

## 1-6. DESCRIPTION

The Hewlett-Packard Model 11729C Carrier Noise Test Set is an integral part of a phase noise measurement system.
The Carrier Noise Test Set can perform the following operations:

- Up converts an external (or internal) reference signal.


## DESCRIPTION (cont'd)

- Down converts the signal under test to an intermediate frequency (IF).
- Phase demodulates the phase noise of the test signal using the Phase Detector Method.
-When the Phase Detector Method is used the signal under test is phase locked to a reference signal.
-The signal under test is then phase detected against the same reference signal.
- Frequency demodulates the phase noise of the test signal using the Frequency Discriminator Method.
With the addition of Option 130 the Carrier Noise Test Set is capable of detecting the signal under test for making AM noise measurements.
The Carrier Noise Test Set can be used in two methods of making phase noise measurements:
- Phase Detector Method
- Frequency Discriminator Method

The number of drive signals required for the Carrier Noise Test Set to be completely operational depends on the phase noise measurement method used and the frequency of the signal under test. The drive signals are supplied from an external RF source.In addition to the external RF source, one of the drive signals ( 640 MHz ) can be supplied by the Carrier Noise Test Set. The Carrier Noise Test Set can be configured to provide an internally generated 640 MHz signal; the 640 MHz signal is available by connecting the provided cable-attenuator assembly (HP 11729-60096 or HP 11729-60098 [Option 140]) between two rear panel connectors. The absolute system noise floor will be degraded close-in to the carrier when using the internally generated 640 MHz signal, compared to the 640 MHz signal being supplied by the HP 8662A Synthesized Signal Generator.
The following table lists when the drive signals are required:

| Drive Signals | Phase Detector Method |  | Frequency Discriminator Method |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Frequency Range of Signal Under Test |  | Frequency Range of Signal Under Test |  |
|  | $\begin{aligned} & \text { 10 MHz to } \\ & 1.28 \mathrm{GHz} \end{aligned}$ | $\begin{gathered} 1.28 \mathrm{GHz} \text { to } \\ 18 \mathrm{GHz} \end{gathered}$ | 10 MHz to 1.28 GHz | $\begin{array}{\|l\|l} 1.28 \mathrm{GHz} \text { to } \\ 18 \mathrm{GHz} \end{array}$ |
| $\begin{aligned} & \text { Fixed } \\ & 640 \mathrm{MHz} \end{aligned}$ | Not Needed | X | Not Needed | X |
| Tunable 5 MHz 1280 MHz | X | X | Not <br> Needed | Not <br> Needed |
| $\mathrm{X}=$ Drive signal is used. |  |  |  |  |

When using the Phase Detector Method the signal under test is first down-converted to the 5 MHz 1280 MHz range and then phase detected against the tunable $5 \mathrm{MHz}-1280 \mathrm{MHz}$ signal. Phase detecting produces a dc signal with simultaneous ac voltage fluctuations. These ac components are proportional to the combined phase noise of the two input signals (the signal under test and the tunable $5 \mathrm{MHz}-1280 \mathrm{MHz}$ signal), at rates corresponding to the offset frequency from the signal under test. The phase detected output signal is also used as an error voltage to keep the signal under test and the tunable $5 \mathrm{MHz}-1280 \mathrm{MHz}$ signal in phase quadrature (that is, 90 degrees out-of-phase).

When using the Frequency Discriminator Method, the down-converted signal under test is phase detected against itself using an external delay line and the internal mixer/phase detector. The phase detected signal is proportional to the phase noise on the signal under test. In the Frequency Discriminator Method the signal under test does not have to be phase locked to an external reference signal.

The Carrier Noise Test Set accepts test signals from $10 \mathrm{MHz}-18 \mathrm{GHz}$, at a level of +7 dBm to +20 dBm . The broad frequency range is user selectable from the front panel (local) or by using the Hewlett-Packard Interface Bus (remote). When using the Carrier Noise Test Set in the Phase Detector Method the controls for acquiring and maintaining phase lock are user selectable from the front panel (local) or by using the HewlettPackard Interface Bus (remote).

The Carrier Noise Test Set is compatible with HPIB to the extent indicated by the following codes: SH1, AH1, T5, TE0, L3, LE0, SR1, RL1, PP1, DC1, DT0, and C0. The Carrier Noise TestSet interfaces with the bus via three-state TTL circuitry. An explanation of the compatibility code can be found in IEEE Standard 488 (1978), "IEEE Standard Digital Interface for Programmable Instrumentation" or the identical ANSI Standard MC1.1.

## 1-7. OPTIONS

## 1-8. Electrical Options

Option 003. Option 003 has two bands installed, 10 MHz to 1.28 GHz and 1.28 GHz to 3.2 GHz .

Option 007. Option 007 has two bands installed, 10 MHz to 1.28 GHz and 3.2 GHz to 5.76 GHz .

## Electrical Options (cont'd)

Option 011. Option 011 has two bands installed, 10 MHz to 1.28 GHz and 5.76 GHz to 8.32 GHz .

Option 015. Option 015 has two bands installed, 10 MHz to 1.28 GHz and 8.32 GHz to 10.88 GHz .

Option 019. Option 019 has two bands installed, 10 MHz to 1.28 GHz and 10.88 GHz to 13.44 GHz .

Option 023. Option 023 has two bands installed, 10 MHz to 1.28 GHz and 13.44 GHz to 16.00 GHz .

Option 027. Option 027 has two bands installed, 10 MHz to 1.28 GHz and 16.00 GHz to 18.00 GHz .

Option 130. Option 130 adds AM noise measurement capabilities.
Option 140. Option 140 places all front panel connectors on the rear panel.

## 1-9. Mechanical Options

The following options may have been ordered and received with the Carrier Noise Test Set. If they were not ordered with the original shipment and are now desired, they can be ordered from the nearest Hewlett-Packard office using the part numbers included in each of the following paragraphs.

Instrument Slide Kit (Option 160). The Carrier Noise Test Set can be easily removed from the instrument rack by using the instrument slide kit. The part number of the slide kit is HP 1494-0026.

Front Handle Kit (Option 907). Ease of handling is increased with the front panel handles. The Front Handle Kit part number is HP 5061-0088.

Rack Flange Kit (Option 908). The Carrier Noise Test Set can be solidly mounted to the instrument rack using the flange kit. The Rack Flange Kit part number is HP 5061-9674.

Rack Flange and Front Handle Combination Kit (Option 909). This is a unique part which combines both functions. It is not simply a front handle kit and a rack flange kit packaged together. The Rack Flange and Front Panel Combination Kit part number is HP 5061-9675.

## 1-10. ACCESSORIES SUPPLIED

The accessories supplied with the Carrier Noise Test Set are shown in Figure 1-1.
a. The line power cable is supplied in several configurations, depending on the destination of
the original shipment. Refer to Power Cables in Section II of this manual.
b. An additional fuse is shipped only with instruments that are factory configured for $100 / 120$ Vac operation. This fuse has a 0.5 A rating and is for reconfiguring the instrument for 220/240 Vac operation.
c. A 50 ohm BNC termination is supplied to be connected to the IF OUTPUT on the front panel. With the 50 ohm termination in place the Carrier Noise TestSet meets the requirements of MILSTD 461 RE02.

## NOTE

The 50 ohm termination must be connected to the IF OUTPUT if the IF OUTPUT is not being used.
d. The Carrier Noise Test Set has two connectors on the rear panel labeled 640 MHz OUT and 640 MHz IN. The 640 MHz OUT is connected to the 640 MHz IN to configure the internally generated 640 MHz signal for use during a measurement. A cable-attenuator assembly (HP 11729-60096 or HP 11729-60098 [Option 140]) is supplied to make this connection. The length and attenuation of this cable assembly is critical for the generation of the 640 MHz signal.
e. A $50 \Omega$ SMA termination is supplied to be connected to the 640 MHz OUT connector on the rear panel. For proper operation of an amplifier, in the Carrier Noise Test Set, the termination must be in place when the 640 MHz OUT connector is not being used.

## 1-11. EQUIPMENT REQUIRED BUT NOT SUPPLIED

For the Carrier Noise Test Set to be completely operational it will require one or two drive signals (either a fixed 640 MHz signal or a $5 \mathrm{MHz}-$ 1280 MHz signal or both) that are supplied from an external RF source. Critical specifications of the RF source are in Table 1-4 in this section.

If desired the 640 MHz drive signal can be supplied by the Carrier Noise Test Set. On the rear panel of the Carrier Noise Test Set the 640 MHz OUT connector is connected to the 640 MHz IN connector, using the cable-attenuator assembly (HP 1172960096 or HP 11729-60098 [Option 140] ) supplied with the instrument. The absolute system noise floor will be degraded close-in to the carrier when

## EQUIPMENT REQUIRED BUT NOT SUPPLIED (cont'd)

using the internally generated 640 MHz signal, compared to the 640 MHz signal being supplied by the HP 8662A Synthesized Signal Generator.
The following table lists the coaxial cables required to connect the Carrier Noise Test Set to the HP 8662A or 8663A Synthesized Signal Generators. Also listed are the cables necessary to connect the Carrier Noise Test Set to a spectrum analyzer.

| $\begin{gathered} \text { HP } \\ \text { Part No. } \end{gathered}$ | Description | Use on Carrier Noise Test Set |
| :---: | :---: | :---: |
| 11170B | BNC(M)-BNC(M) (24 inches) | $\begin{aligned} & 5 \text { to } 1280 \mathrm{MHz} \\ & \text { INPUT } \end{aligned}$ |
| 11170C | BNC(M)-BNC(M) (48 inches) | 640 MHz IN <br> FREQ-CONT DC-FM FREQ-CONT X-OSC NOISE SPECTRUM $<10 \mathrm{MHz}$ OUTPUT $<1 \mathrm{MHz}$ OUTPUT |

Table 1-1. Specifications (1 of 2)

| Electrical Characteristics | Performance Limits | Conditions |
| :---: | :---: | :---: |
| TEST SIGNAL <br> Frequency Range ${ }^{1}$ <br> Band Center Frequencies | 10 MHz to 18 GHz $\begin{array}{r} 1.92 \mathrm{GHz} \\ 4.48 \mathrm{GHz} \\ 7.04 \mathrm{GHz} \\ 9.60 \mathrm{GHz} \\ 12.16 \mathrm{GHz} \\ 14.72 \mathrm{GHz} \\ 17.28 \mathrm{GHz} \end{array}$ | External low-pass filtering may be required for test signals $<20 \mathrm{MHz}$ and $\pm 20 \mathrm{MHz}$ around band centers |
| IF OUTPUT <br> Bandwidth <br> Level | 5 MHz to 1280 MHz +7 dBm Minimum |  |
| AM NOISE DETECTION (Option 130) <br> Frequency Range <br> Input level <br> AM Noise Floor <br> Offset from Carrier (Hz) 1k 10k <br> 100k <br> 1M | 10 MHz to 18 GHz <br> 0 dBm to +18 dBm <br> AM Noise ( $\mathrm{dBc} / \mathrm{Hz}$ ) $\begin{aligned} & -138 \\ & -145 \\ & -155 \end{aligned}$ $-160$ | At +10 dBm input level |
| RESIDUAL NOISE Offset From Carrier(Hz) 10 100 1 k 10 k 10 k 1 M | $\begin{gathered} \mathrm{dBc} / \mathrm{Hz} \\ -115 \\ -126 \\ -135 \\ -142 \\ -151 \\ -156 \end{gathered}$ | With a $<1.28$ GHz input signal |
| ${ }^{1}$ In eight (8) bands, excluding $\pm 5 \mathrm{MHz}$ around band center frequencies. |  |  |

Table 1-1. Specifications (2 of 2)

| Electrical Characteristics | Performance Limits | Conditions |
| :---: | :---: | :---: |
| RESIDUAL NOISE (cont'd) | $\begin{aligned} & \mathrm{dBc} / \mathrm{Hz} \\ & -90 \\ & -105 \\ & -115 \\ & -127 \\ & -137 \\ & -142 \end{aligned}$ | With a 10 GHz input signal |
| GENERAL <br> Line Voltage <br> Line Frequency <br> Power Dissipation <br> Temperature: <br> Operating <br> Weight: <br> Net <br> Dimensions ${ }^{2}$ : <br> Height <br> Width <br> Depth <br> Remote Operation <br> (HP-IB) ${ }^{3}$ <br> IEEE STD 488-1978 Compatibility Code: SH1, AH1, T5,TE0, L3, LE0, SR1, RL1,PP1, DC1, DT0,C0. | $\begin{aligned} & 100,120,220 \text { or } 240 \mathrm{~V} \\ & (+5 \%,-10 \%) \\ & 48 \text { to } 66 \mathrm{~Hz} \\ & 75 \mathrm{~V} \cdot \mathrm{~A} \text { maximum } \\ & 0 \text { to }+55^{\circ} \mathrm{C} \\ & \\ & 10.4 \mathrm{~kg}(23 \mathrm{lb} .) \\ & \\ & 99 \mathrm{~mm}(3.9 \mathrm{in} .) \\ & 425 \mathrm{~mm}(16.8 \mathrm{in} .) \\ & 551 \mathrm{~mm}(21.7 \mathrm{in} .) \end{aligned}$ |  |
| ELECTROMAGNETIC COMPATIBILITY <br> Electromagnetic Interference | Conducted and radiated interference is within the requirements of CE03 and RE02 as called out in MIL-STD 461, and within the requirements of VDE 0871 and CISPR Publication 11. |  |
| ${ }^{2}$ For ordering cabinet accessories the module sizes are $3-1 / 2 \mathrm{H}, 1 \mathrm{MW}$ (module width), 20D. <br> ${ }^{3}$ The Hewlett-Packard Interface Bus (HP-IB) is Hewlett-Packard's implementation of IEEE STD 488-1978, "Digital Interface Programmable Instrumentation." All front panel functions with the exception of the line switch are HP-IB programmable. |  |  |

Table 1-2. Supplemental Characteristics (1 of 2)
Supplemental characteristics are intended to provide information useful in applying the instrument by giving typical, but non-warranted, performance parameters.

## TEST SIGNAL

Level: For test signals $>1.28 \mathrm{GHz}:+7 \mathrm{dBm}$ to +20 dBm
Typically useable down to -15 dBm with potential noise floor degradation.
For test frequencies $<1.28 \mathrm{GHz}:-5 \mathrm{dBm}$ to +10 dBm . Typically usable down to -15 dBm with potential noise floor degradation; optimal level from -2 dBm to +3 dBm .

## IF OUTPUT

Typically useable to 1500 MHz dependent on the test frequency.

## NOISE SPECTRUM OUTPUTS

$<10 \mathrm{MHz}$ Output (The $<10 \mathrm{MHz}$ Output is amplified by an internal 40 dB Low Noise Amplifier)

Bandwidth: 10 Hz to 10 MHz . ( 3 dB BW: 10 Hz to 15 MHz typical.)
Flatness: $\pm 1 \mathrm{~dB}$ typical, 50 Hz to 10 MHz
Output impedance: $50 \Omega$ nominal
$<1 \mathrm{MHz}$ Output (The $<1 \mathrm{MHz}$ Output is a non-amplified output)
Bandwidth: dc to 1 MHz . ( 3 dB BW: dc to 1.5 MHz typical.)
Flatness: $\pm 1 \mathrm{~dB}$ typical
Output impedance: 600 $\mathbf{\Omega}$ nominal

## Auxiliary Noise

Output impedance: $600 \Omega$ nominal
Bandwidth: dc to 1 MHz typical

## PHASE LOCK LOOP FUNCTION

FREQUENCY CONTROL OUTPUTS
Freq-Cont X-Osc
Output level: $\pm 10 \mathrm{~V}$ nominal
Nominal Output impedance: $100 \Omega$.
Freq-Cont DC-FM
Output level: $\pm 1 \mathrm{~V}$ nominal
Nominal Output impedance: $50 \Omega$.
Lock Bandwidth Factor: $1,10,100,1 \mathrm{k}, 10 \mathrm{k}$ nominal. (Selectable by front panel pushbuttons.)

Loop characteristics: dependent on method of phase lock (crystal or DC-FM) used and loop VCO chosen.

Loop Characteristics when using the HP 8662A Elec-
tronic Frequency Control input for phase locking with the HP 8662A front panel output at 0 dBm :
Loop Holding Range (LHR):

$$
\frac{ \pm \mathrm{f}_{\text {dut }}}{10^{7}} \quad \text { (Hz nominal) }
$$

Loop Bandwidth (LBW):

$$
\frac{\mathrm{HP} 11729 \mathrm{C} \text { LBF } \times \mathrm{f}_{\mathrm{dut}}}{10^{10}}=(\mathrm{Hz} \text { nominal })
$$

Loop Bandwidth Maximum: 2 kHz typical

$$
\mathrm{f}=\text { frequency }
$$

dut $=$ Device under test
LBF = Lock Bandwith Factor set on HP 11729C
Loop Characteristics when using the HP 8662A dc FM modulation input for phase locking with the HP 8662A front panel output at 0 dBm :
Loop Holding Range (LHR): $\pm$ FM deviation set on HP 8662A (Hz nominal).
Loop Bandwidth (LBW):
$\left.\frac{(\mathrm{HP} \text { 8662A FPD) } \times \text { HP 11729C LBF nom. }}{10^{3}}=\begin{array}{c}(\mathrm{Hz} \\ \text { nom. }\end{array}\right)$
Loop Bandwidth Maximum: 100 kHz typical.
LBF = Lock Bandwidth Factor set on HP 11729C FPD $=$ Front Panel Deviation

## LOOP TEST PORTS

Loop Test Input:
Source: random noise source, tracking generator, or sinusoidal input.
Bandwidth: dc to 100 kHz typical.
Input level: less than 0.1 V peak, typical.
Input impedance: dc coupled, $10 \mathrm{k} \Omega$ nominal
Loop Test Output:
Bandwidth: dc to 100 kHz , typical.
Output level: gain outside loop bandwidth = 1
Output impedance: dc coupled, $1 \mathrm{k} \Omega$. nominal
AM NOISE DETECTION
(Option 130)
AM Noise Floor (at +10 dBm input level):
Offset From Carrier (Hz) Typical AM Noise(dBc/Hz)

| 1 k | -147 |
| ---: | :--- |
| 10 k | -152 |
| 100 k | -161 |
| 1 M | -165 |

Table 1-2. Supplemental Characteristics (2 of 2)

| Offiset | Carrier |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| carrier (Hz) | $\begin{aligned} & <1.28 \mathrm{GHz} \\ & (\mathrm{dBc} / \mathrm{Hz}) \end{aligned}$ | $\begin{gathered} 5 \mathrm{GHz} \\ (\mathrm{dBc} / \mathrm{Hz}) \end{gathered}$ | $\begin{gathered} 10 \mathrm{GHz} \\ (\mathrm{dBc} / \mathrm{Hz}) \end{gathered}$ | $\begin{gathered} 18 \mathrm{GHz} \\ (\mathrm{dBc} / \mathrm{Hz}) \end{gathered}$ |
| 10 | -125 | -112 | -106 | -100 |
| 100 | -133 | -120 | -116 | -110 |
| 1k | -140 | -130 | -125 | -119 |
| 10k | -147 | -137 | -132 | -126 |
| 100k | -156 | -146 | -141 | -135 |
| 1M | -160 | -148 | -144 | -138 |
| 10M | -160 | -148 | -144 | -138 |

The absolute phase noise of the internal saw oscillator with a 10 GHz input signal.

Sensitivity of the HP 11729C using the internal saw oscillator and a 10 GHz input signal. The Frequency Discriminator Method was used which had a delay line with the following characteristics: delay was 100 ns, attenuation was $<10 \mathrm{~dB}$ and the cable used was RG-223.

| Offset From Carrier (Hz) | $\mathbf{d B c} / \mathrm{Hz}$ |
| :---: | :---: |
| $1 \mathbf{k}$ | -80 |
| $10 \mathbf{k}$ | -106 |
| $100 \mathbf{k}$ | -131 |
| 1 M | -144 |


| Offset From Carrier (Hz) | $\mathrm{dBc} / \mathrm{Hz}$ |
| :---: | :---: |
| 1 k | -86 |
| 10 k | -116 |
| 100 k | -135 |
| 1 M | -145 |
| 10 M | -147 |

## 1-12. ELECTRICAL EQUIPMENT AVAILABLE

 The Carrier Noise Test Set has an HP-IB interface and can be used with any HP-IB compatible computing controller or computer for automatic systems applications.
## 1-13. RECOMMENDED TEST EQUIPMENT

Table 1-4 lists the test equipment recommended for use in testing, adjusting and servicing the Carrier Noise Test Set. The Critical Specification
column describes the essential requirements for each piece of test equipment. Other equipment can be substituted if it meets or exceeds these critical specifications.

Table 1-4 also includes some alternate equipment listings. These alternate instruments are highlighted in Table 1-5 which also indicates the possible advantages of using them as substitutes.

The following information is supplied to aid the user when configuring the Carrier Noise Test Set in a system. The system specifications are for the HP 11729C and the HP 8662A.
Also given are the general requirements for an unknown RF source being used with the HP 11729C.

Table 1-3. System Specifications (1 of 2)

## ABSOLUTE SYSTEM NOISE FLOOR

System noise is specified only when the HP 11729C is used with an HP 8662A Option $003^{1}$.

## Phase Detector Method (locking via EFC):

HP 11729C/8662A Absolute System Noise ${ }^{2,3}$
(dBc/Hz):

| Offiset from Carrier (Hz) | Band 1 5 to 1280 MHz |  | $\begin{gathered} \text { Band } 2 \\ 1.28 \text { to } 3.2 \\ \text { GHz } \end{gathered}$ |  | $\begin{gathered} \text { Band } 3 \\ 3.2 \text { to } 5.76 \\ \text { GHz } \end{gathered}$ |  | $\begin{gathered} \text { Band } 4 \\ 5.76 \text { to } 8.32 \\ \text { GHz } \end{gathered}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Typ. | Spec. | Typ. | Spec. | Typ. | Spec. | Typ. | Spec. |
| 1 | -58 | -48 | -53 | -43 | -47 | -37 | -43 | -33 |
| 10 | -88 | -78 | -83 | -73 | -77 | -67 | -73 | -63 |
| 100 | -108 | -98 | -103 | -93 | -97 | -87 | -93 | -83 |
| 1k | -119 | -115 | -115 | -110 | -109 | -104 | -105 | -100 |
| 10k | -130 | -125 | -129 | -124 | -127 | -123 | -125 | -121 |
| 100k | -130 | -126 | -130 | -126 | -130 | -126 | -129 | -125 |
| 1M | -140 |  | -140 |  | -138 |  | -135 |  |
| Offiset from Carrier (Hz) | $\begin{gathered} \text { Band } 5 \\ 8.32 \text { to } 10.88 \\ \mathrm{GHz} \end{gathered}$ |  | $\begin{gathered} \text { Band } 6 \\ 10.88 \text { to } 13.44 \\ 6 \mathrm{~Hz} \end{gathered}$ |  | $\begin{gathered} \text { Band } 7 \\ 13.44 \text { to } 16.0 \\ \mathrm{GHz} \end{gathered}$ |  | $\begin{aligned} & \text { Band } 8 \\ & 16.0 \text { to } 18.0 \\ & \text { GHz } \end{aligned}$ |  |
|  | Typ. | Spec. | Typ. | Spec. | Typ. | Spec. | Typ. | Spec. |
| 1 | -40 | -30 | -38 | -28 | -37 | -27 | -35 | -25 |
| 10 | -70 | -60 | -68 | -58 | -67 | -57 | -65 | -55 |
| 100 | -90 | -80 | -88 | -78 | -87 | -77 | -85 | -75 |
| 1k | -102 | -97 | -100 | -95 | -99 | -94 | -97 | -92 |
| 10k | -123 | -119 | -122 | -118 | -121 | -116 | -119 | -115 |
| 100k | -129 | -125 | -128 | -125 | -127 | -124 | -127 | -123 |
| 1M | -134 |  | -132 |  | -131 |  | -129 |  |

${ }^{1}$ The HP 8663A Option 003 (operated below 1280 MHz ) may be used in place of the HP 8662A with no change in system performance.
${ }^{2}$ These system noise floor specifications apply for locking via the EFC of the HP 8662A crystal oscillator. Locking via the HP 8662A dc FM changes the phase noise on the tuna ble HP 8662A signal and therefore total system noise. Use the system phase noise equation at the end of footnote 3 to determine system phase noise when locking via the HP 8662A dc FM.
${ }^{3}$ The absolute system phase noise is dependent on the test signal frequency, therefore, the actual system noise may be lower than specified. Since the noise contribution of the HP 8662A front panel signal is a function of frequency selected, the overall system noise may improve for test frequencies $<640 \mathrm{MHz}$ from band centers. For example, for frequencies over the narrow range of 8.96 to 10.24 GHz , typical system phase noise at a 100 kHz offset is $-134 \mathrm{dBc} / \mathrm{Hz}$. To determine the system phase noise for any test frequency, see the system phase noise equation below.

$$
\mathcal{L}_{\text {system }}=10 \log \left(\mathrm{~N}^{2} \times \frac{\mathcal{L}_{1}}{10^{10}}+\frac{\mathcal{L}_{2}}{10^{10}}+\frac{\mathcal{L}_{3}}{10^{10}}\right)
$$

where $\mathrm{N}=$ center frequency of selected filter $/ 640 \mathrm{MHz}$
$\mathcal{L}_{1}=$ absolute SSB phase noise of the 640 MHz ref-
${ }_{1}$ erence signal ( $\mathrm{dBc} / \mathrm{Hz}$ )
$\mathcal{L}_{2}=$ absolute SSB phase noise of the 5 to 1280 MHz tunable signal ( $\mathrm{dBc} / \mathrm{Hz}$ )
$\mathcal{L}_{3}=$ residual noise of the $\mathrm{HP} 11729 \mathrm{C}(\mathrm{dBc} / \mathrm{Hz})$


Typical HP 11729C/8662A system noise (phase detector method, locking via EFC).

## Frequency Discriminator Method:

HP 11729C/8662A System Noise and Sensitivity: In the frequency discriminator mode, the lower limit of the measurement system sensitivity is set by the noise contribution of the $11729 \mathrm{C} / 8662 \mathrm{~A}$. Typical system noise contribution of the HP 11729C/8662A is shown in the table below.

| Offset <br> from <br> Carrier (Hz) | Typical System Noise (dBc/Hz) <br> firequency discriminator) |  |  |
| :---: | :---: | :---: | :---: |
|  | 1.26 to <br> 3.2 GHz | 8.32 to <br> 10.88 GHz | 16.0 to <br> 18.0 GHz |
|  | -54 | -40 | -35 |
| 10 | -84 | -70 | -65 |
| 100 | -104 | -90 | -85 |
| 1 k | -116 | -102 | -97 |
| 10 k | -139 | -125 | -120 |
| 100 k | -149 | -135 | -130 |
| 1 M | -149 | -135 | -130 |

The actual HP $11729 \mathrm{C} / 8662 \mathrm{~A}$ measurement sensitivity in the frequency discriminator method largely depends on the delay line (delay time) used. The longer the delay time, the closer the measurement sensitivity approaches the system noise limit. The graph shows the HP 11729C/8662A noise contribution, and a typically obtainable system sensitivity. A 34 foot section of flexible $R F$ cable ( $R G 225$ ) was used as the external time delay element $\tau=50 \mathrm{~ns}$.

Table 1-3. System Specifications (2 of 2)

## Frequency Discriminator Method (cont'd]



Typical noise contribution of HP 11729C/8662A (frequency discriminator method) at X-band and typical system sensitivity using a 50 ns delay line discriminator.

Listed below are general requirements for the RF source when used with the HP 11729C in a system:

## 640 MHz signal source:

Frequency: $640 \mathrm{MHz} \pm 50 \mathrm{ppm}$.
Level: +1 dBm minimum, +4 dBm maximum.
Frequency control: dependent on method of phase lock chosen.

5-1280 MHz tunable source:
Frequency: $5-1280 \mathrm{MHz}$.
Level: $0 \mathrm{dBm} \pm 1 \mathrm{~dB}$. Typically usable to $\epsilon 10 \mathrm{dBm}$ with change in loop bandwidth and system noise floor.

Frequency control: dependent on method of phase lock chosen; could require dc coupled frequency controlled input accepting $\pm 1 \mathrm{~V}$ or $\pm 10 \mathrm{~V}$, with necessary deviation dependent on source under test.

Use the following procedure to calculate the Absolute System Noise Floor of the HP 11729C and an RF source other than the HP 8662A.

## Absolute System Noise Floor (general case):

Measurement system noise floor is dependent on the RF reference source(s) used. For the frequency discriminator method, system noise is a composite of the noise on the multiplied 640 MHz signal plus the residual noise of the HP 11729C. For the phase detector method, system noise has the additional noise of the RF tunable source at the phase detector input. System noise can be described by

$$
\mathcal{L}_{\text {system }}=10 \log \left(\mathrm{~N}^{2} \times \frac{\mathcal{L}_{1}}{10^{10}}+\frac{\mathcal{L}_{2}}{10^{10}}+\frac{\mathcal{L}_{3}}{10^{10}}\right)
$$

where $\mathrm{N}=$ center frequency of selected filter/ 640 MHz
$\mathcal{L}_{1}=$ absolute $\operatorname{SSB}$ phase noise of the 640 MHz reference signal ( $\mathrm{dBc} / \mathrm{Hz}$ )
$\begin{aligned} \mathcal{L}_{2}= & \text { absolute } \mathrm{SSB} \text { phase noise of the } 5 \text { to } \\ & 1280 \mathrm{MHz} \text { tunable signal ( } \mathrm{dBc} / \mathrm{Hz} \text { ) }\end{aligned}$
$\mathcal{L}_{3}=$ residual noise of the HP $11729 \mathrm{C}(\mathrm{dBc} / \mathrm{Hz})$

Table 1-4. Recommended Test Equipment (1 of 3)

| Instrument | Critical Specifications | Recommended Model | Use* |
| :---: | :---: | :---: | :---: |
| Amplifier | Input Frequency: 640 MHz <br> Gain: 22 dB <br> Noise Figure: $<10 \mathrm{dBm}$ | HP 8447E/F | P |
| Attenuator | Input Frequency Range: 640 MHz to 1 GHz Incremental Attenuation: 1 dB steps Maximum attenuation: 10 dB | HP 355C | P |
| Cable (RF) | $\mathrm{BNC}(\mathrm{m})$ to $\mathrm{BNC}(\mathrm{m})$ (9 inches) | HP 10502A | P |
| Cable (RF) | $\mathrm{BNC}(\mathrm{m})$ to BNC(m) (24 inches) | HP 11170B | OPAT |
| Carrier Noise Test Set | (There isn't any substitute instrument for the Carrier Noise Test Set) <br> Band Range: 8.32 GHz to 10.88 GHz <br> IF output bandwidth: 400 MHz <br> IF output level: +7 dBm <br> Residual Phase Noise: (Using a 10 GHz Test Signal) | HP 11729C ${ }^{1}$ | P |
| Controller | Minimum controller capability as defined by IEEE Standard 488-1975 and the identical ANSI Standard MC1.1: SH1, AH1, T4, TE0, L2, LE0, SR0, RL1, PP0, DC0, DT0, and C1-4,26. | HP 85B | OA |
| Digital <br> Multimeter | Input Range: 0 to 15 Vdc Accuracy: $\pm 1 \mathrm{mVdc}$ | HP 3468A | AT |
| Function Generator | Frequency: 1 kHz <br> Function: sinewave <br> Amplitude: 500 mVdc to 5 Vdc <br> DC Offset Capability | HP 3312A | P |
| Isolator | Power Input level: +15 dBm <br> Frequency Input: 10 GHz | HP 0955-0178 ${ }^{2}$ | P |

* $\mathrm{A}=$ Adjustments; $\mathrm{O}=$ Operator's Checks; $\mathrm{P}=$ Performance Tests; $\mathbf{T}=$ Troubleshooting
${ }^{1}$ This Carrier Noise Test Set must contain a Band Range that is included in the Carrier Noise Test Set under test.
${ }^{2}$ Under certain conditions an attenuator can be used in place of the isolator. For more information see the AM Noise Floor Performance Test in Section IV.

Table 1-4. Recommended Test Equipment (2 of 3)

| Instrument | Critical Specifications | Recommended Model | Use* |
| :---: | :---: | :---: | :---: |
| Low Frequency Spectrum Analyzer | Frequency Range: 0 Hz to 1 kHz <br> Measurement Range: -75 dBm to 0 dBm <br> Resolution Bandwidth: 30 MHz <br> Video Averaging <br> Video Readout Accuracy: $\pm 0.5 \mathrm{~dB}$ | $\begin{aligned} & \text { HP 3582A } \\ & \text { HP 3561A } \end{aligned}$ | P |
| Low Noise Oscillator | One Frequency between: 5 MHz and 18 GHz Amplitude: +10 dBm <br> AM noise: | MA $86651 \mathrm{~A}^{3}$ <br> (M/A Com) | P |
| Microwave <br> Synthesized Source | Frequency Range: 2 GHz to 10 GHz <br> Amplitude: $>+10 \mathrm{dBm}$ <br> Short term Frequency stability: 1 part in $10^{7}$ External AM Modulation capability | $\begin{aligned} & \text { HP 8340A } \\ & \text { HP 8673B } \end{aligned}$ | OPAT |
| Oscilloscope | Bandwidth: 100 Hz <br> Vertical Sensitivity: $5 \mathrm{mV} /$ div AC Coupled | HP 1740A | T |
| Power Meter | Accuracy: $\pm 0.2 \mathrm{dBm}$ | HP 436A | PA |
| Power Sensor | Frequency Range: 100 MHz to 10 GHz Power Range: 0 dBm to 15 dBm Input Impedance: $50 \Omega$ SWR: < 1.25 | HP 8481A | PA |
| Power Splitter | Input Frequency Range: 400 MHz to 700 MHz Output tracking: $<0.25 \mathrm{~dB}$ | HP 11667A | P |
| Power Splitter | Input Frequency: 10 GHz <br> Output tracking: $<0.25 \mathrm{~dB}$ | HP 11667A | P |
| Power Supply | Voltage Output: +10 Vdc maximum | HP 6214B | P |
| RF Spectrum Analyzer | Frequency Range: $1 \mathbf{k H z}$ to 10 MHz <br> Dynamic Range: -75 dBm to 0 dBm <br> Resolution Bandwidth: 100 Hz and 100 kHz <br> Video Filtering <br> Marker capability <br> Reference Level Control <br> Video Readout Accuracy: $\pm 0.5 \mathrm{~dB}$ <br> Sensitivity: -117 dB | HP 8566B | OPT |
| * $\mathrm{A}=$ Adjustments; $\mathrm{O}=$ Operator's Checks; $\mathrm{P}=$ Performance Tests; $\mathrm{T}=$ Troubleshooting ${ }^{3}$ Commercial Sources Division, M/A-COM, South Avenue, Burlington, MA 01803 |  |  |  |

Table 1-4. Recommended Test Equipment (3 of 3)

| Instrument | Critical Specifications | Recommended Model | Use* |
| :---: | :---: | :---: | :---: |
| RF Synthesized <br> Signal <br> Generator | Auxillary 640 MHz Signal: <br> Absolute Phase Noise: <br> Level: $>+1 \mathrm{dBm}$ to $<+4 \mathrm{dBm}$ <br> Electronic Frequency Control: $\pm 1$ Vdc or $\pm 10$ Vdc <br> RF Output: <br> Frequency Range: 300 MHz to 700 MHz <br> Frequency resolution: 10 Hz <br> Amplitude: -40 dBm to 0 dBm <br> External AM Modulation capability | HP 8662A ${ }^{4}$ <br> (Opt. 003) <br> HP 8663A ${ }^{4}$ <br> (Opt. 003) | OPAT |
| Termination | 50 ohms BNC | HP 11593A | P |
| Waveguide | UG-135/U to N(f) | HP X281C | P |
| * $\mathbf{A}=$ Adjustments; $\mathbf{O}=$ Operator's Checks; $\mathbf{P}=$ Performance Tests; $\mathbf{T}=$ Troubleshooting <br> ${ }^{4}$ For one HP 8662A or 8663A to operate with the Carrier Noise Test Set and give the best phase noise performance, two rear panel connectors are required. One connector must supply 640 MHz and the other connector must accept the Electronic Frequency Control signal from the Carrier Noise TestSet. As of April 1984 these two connectors are on the rear panel of each standard HP 8662A or 8663A. Before April 1984 these two connectors were specified by options H03 and H12. The HP 8662A or 8663A option 003 includes testing the phase noise of the 640 MHz signal. |  |  |  |

Table 1-5. Recommended Alternate Test Equipment

| Instrument <br> Type | Suggested <br> Alternate | Instrument <br> Replaced | Advantages of <br> Alternate |
| :--- | :---: | :---: | :--- |
| RF Synthesized Signal <br> Generator | HP 8663A | HP 8662A | The HP 8663A is a direct <br> substitrite for the <br> HP 8662A. |
| Microwave <br> Synthesized Source | HP 8673B | HP 8340A | Less expensive |
| Low Frequency <br> Spectrum Analyzer | HP 3561A | HP 3582A | Better Accuracy |

# SECTION II <br> INSTALLATION 

## 2-1. INTRODUCTION

This section provides the information needed to install the Carrier Noise Test Set. Included is information pertinent to initial inspection, power requirememts, line voltage selection, power cables, interconnection, environmemt, instrument mounting, storage and shipment.

## 2-2. INITIAL INSPECTION



To avoid hazardous electrical shock, do not perform electrical tests when there are signs of shipping damage to any portion of the outer enclosure (covers, panels, displays).

Inspect the shipping container for damage. If the shipping container or cushioning material is damaged, it should be kept until the contents of the shipment have been checked for completeness and the instrument has been checked mechanically and electrically. The contents of the shipment should be as shown in Figure 1-1. Procedures for checking electrical performance are given in Section IV. If the contents are incomplete, if there is mechanical damage or defect, or if the instrument does not pass the electrical performance test, notify the nearest Hewlett-Packard office. If the shipping container is damaged or the cushioning material shows signs of stress, notify the carrier as well as the Hewlett-Packard office. Keep the shipping materials for the carrier's inspection.

## 2-3. PREPARATION FOR USE

## 2-4. Power Requirements

The Carrier Noise Test Set requires a power source of $100,120,220$ or 240 Vac, $+5 \%$ to $-10 \%, 48$ to 66 Hz single phase. Power consumption is 75 VA maximum.

## WARNINGS

This is a Safety Class I product (that is, provided with a protective earth terminal). An uninterruptible safety earth ground must be provided from the main
power source to the product input wiring terminals through the power cord or supplied power cord set. Whenever it is likely that the protection has been impaired, the product must be made inoperative and be secured against any unintended operation.

If this instrument is to be energized via an external autotransformer, make sure the autotransformer's common terminal is connected to the neutral (that is, the grounded side of the mains supply).

## 2-5. Line Voltage and Fuse Selection



BEFORE PLUGGING THIS INSTRUMENT into the mains (line) voltage, be sure the correct voltage and fuse have been selected.

Verify that the line voltage selection card and the fuse are matched to the power source. Refer to Figure 2-1, Line Voltage and Fuse Selection.

Fuses may be ordered under HP part numbers 2110-0001, 1.0A (250V) for $100 /$ 120 Vac operation and 2110-0012, 0.5A (250V) for 220/240 Vac operation.

## 2-6. Power Cables

WARNING
BEFORE CONNECTING THIS IN. STRUMENT, the protective earth terminal of this instrument must be connected to the protective conductor of the (mains) power cord. The mains plug shall only be inserted in a socket outlet provided with a protective earth contact. The protective action must not be negated by the use of an extension cord (power cable) without a protective conductor (grounding).


Operating voltage is shown in module window.

## SELECTION OF OPERATING VOLTAGE

1. Open cover door, pull the FUSE PULL lever and rotate to left. Remove the fuse.
2. Remove the Line Voltage Selection Card. Position the card so the line voltage appears at top-left corner. Push the card firmly into the slot.
3. Rotate the FUSE PULL lever to its normal position. Insert a fuse of the correct value in the holder. Close the cover door.

## WARNING

To avoid the possibility of hazardous electrical shock, do not operate this instrument at line voltages greater than 126.5 Vac with line frequencies greater than 66 Hz (leakage currents at these line settings may exceed $3.5 m A$ ).

## Power Cables (cont'd)

This instrument is equipped with a three-wire power cable. When connected to an appropriate ac power receptacle, this cable grounds the instrument cabinet. The power cable plug shipped with each instrument depends on the country of destination. Refer to Figure 2-2 for the part numbers of power cables available.

## 2-7. HP-IB Address Selection $\langle\mathrm{HP}-\mathrm{IB}$,

The HP-IB address is switch-selectable through five miniature slide switches located on the rear panel of the Carrier Noise Test Set. These switches provide the means to select one of 31 valid HP-IB addresses ( 00 through 30 ). HP-IB addresses greater than 30 (decimal) are invalid. Refer to Table 2-1 for the allowable HP-IB address codes. Listed are the valid address switch settings and equivalent ASCII character and decimal value. When the instrument is shipped from the factory, the HP-IB address is preset to 06 (decimal). (In binary, this is 00110.) This preset address is shown shaded in Table 2-1.

The following procedure describes how to change the settings of the HP-IB address switches.

Use a small screwdriver to set the switches to the desired HP-IB address in binary. The five switches are labeled A1 through A5, where A1 is the least significant address bit and A5 is the most signifi-
Figure 2-1. Line Voltage and Fuse Selection


Figure 2-2. Power Cable and Mains Plug Part Numbers

Table 2-1. Allowable HP-IB Address Codes

| Decimal Equiva: lent' | Listen Address Character | Talk Address Character | Address Switches ${ }^{1}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | A5 | A4 | A3 | A2 | A1 |
| 0 | SP | ${ }^{(8)}$ | 0 | 0 | 0 | 0 | 0 |
| 1 | ! | A | 0 | 0 | 0 | 0 | 1 |
| 2 | " | B | 0 | 0 | 0 | 1 | 0 |
| 3 | \# | C | 0 | 0 | 0 | 1 | 1 |
| 4 | \$ | D | 0 | 0 | 1 | 0 | 0 |
| 5 | \% | E | 0 | 0 | 1 | 0 | 1 |
| 6 | \& | F | 0 | 0 | 1 | 1 | 0 |
| 7 | , | G | 0 | 0 | 1 | 1 | 1 |
| 8 | 1 | H | 0 | 1 | 0 | 0 | 0 |
| 9 | ) | 1 | 0 | 1 | 0 | 0 | 1 |
| 10 | * | J | 0 | 1 | 0 | 1 | 0 |
| 11 | + | K | 0 | 1 | 0 | 1 | 1 |
| 12 | , | L | 0 | 1 | 1 | 0 | 0 |
| 13 | - | M | 0 | 1 | 1 | 0 | 1 |
| 14 | - | N | 0 | 1 | 1 | 1 | 0 |
| 15 | 1 | 0 | 0 | 1 | 1 | 1 | 1 |
| 16 | 0 | P | 1 | 0 | 0 | 0 | 0 |
| 17 | 1 | Q | 1 | 0 | 0 | 0 | 1 |
| 18 | 2 | R | 1 | 0 | 0 | 1 | 0 |
| 19 | 3 | S | 1 | 0 | 0 | 1 | 1 |
| 20 | 4 | T | 1 | 0 | 1 | 0 | 0 |
| 21 | 5 | U | 1 | 0 | 1 | 0 | 1 |
| 22 | 6 | V | 1 | 0 | 1 | 1 | 0 |
| 23 | 7 | W | 1 | 0 | 1 | 1 | 1 |
| 24 | 8 | X | 1 | 1 | 0 | 0 | 0 |
| 25 | 9 | Y | 1 | 1 | 0 | 0 | 1 |
| 26 | : | Z | 1 | 1 | 0 | 1 | 0 |
| 27 | ; | [ | 1 | 1 | 0 | 1 | 1 |
| 28 | $<$ | 1 | 1 | 1 | 1 | 0 | 0 |
| 29 | $=$ | ] | 1 | 1 | 1 | 0 | 1 |
| 30 | $>$ | 0 | 1 | 1 | 1 | 1 | 0 |
| ${ }^{1}$ Decimal characters and the five address switches relate to the last five bits of both talk and listen addresses. <br> ${ }^{2}$ Factory-set address. |  |  |  |  |  |  |  |

## HP-IB Address Selection (cont'd)

cant address bit. Sliding the switch downward (as viewed from the rear of the instrument) "sets" the corresponding address bit to " 1 " while sliding the switch upwards "clears" the bit (bit=0). Setting all of the address bits to " 1 " will result in an invalid HP-IB address ( 31 decimal). In this case an HP-IB
address of 30 (decimal) will be stored in memory once the instrument is powered up.

If the HP-IB address is changed when the instrument is on the instrument will have to be turned off then turned on again. This is necessary so the new address can be read by the microprocessor and stored in memory.

Along with the five address switches (A1 through A5) there are two other switches. These two switches are labeled "LO" LISTEN ONLY and "TO" TALK ONLY. When either the "LO" or "TO" switch is set to " 1 " the Carrier Noise Test Set becomes either a TALKER ONLY or a LISTENER ONLY and the HP-IB address is overridden. At the factory the "LO" and "TO" switches are set to " 0 ".

## 2-8. Interconnections

For the Carrier Noise Test Set to be fully operational it may have to be connected to an external RF source for one or both of the drive signals (51280 MHz and 640 MHz ). The drive signals are essential to the operation of the Carrier Noise Test Set.

One of the drive signals can be supplied by the Carrier Noise Test Set. An internally generated 640 MHz reference signal can be provided by connecting the supplied cable-attenuator assembly between the proper rear panel connectors. For proper operation, it is essential that the supplied cable-attenuator assembly (HP 11729-60096 or HP 11729-60098 [Option 140]) be used to make the connection.

The following figures, in Section III OPERATION, show the interconnections to the Carrier Noise Test Set:
Figure 3-4 Phase Noise Measurement Setup
(Phase Detector Method)
Figure 3-7 Phase Noise Measurement Setup
(Frequency Discriminator Method)
Figure 3-8 AM Noise Measurement Setup
Interconnection data for the Hewlett-Packard Interface Bus is provided in Figure 2-3.

## 2-9. Mating Connectors

HP-IB Interface Connector. The HP-IB mating connector is shown in Figure 2-3. Note that the two securing screws are metric.


## Logic Levels

The Hewlett-Packard Interface Bus Logic Levels are TTL compatible, i.e., the true (1) state is 0.0 Vdc to +0.4 Vdc and the false (0) state is +2.5 Vdc to +5.0 Vdc .

## Programming and Output Data Format

Refer to Section III, Operation.

## Mating Connector

HP 1251-0293; Amphenol 57-30240.

## Mating Cables Available

HP 10833A, 1 metre ( 3.3 ft ), HP 10833B, 2 metres ( 6.6 ft )
HP 10833C, 4 metres ( 13.2 ft ), HP 10833D, 0.5 metres ( 1.6 ft )

## Cabling Restrictions

1. A Hewlett-Packard Interface Bus system may contain no more than 2 metres ( 6.6 ft ) of connecting cable per instrument.
2. The maximum accumulative length of connecting cable for any HewlettPackard Interface Bus system is 20.0 metres ( 65.5 ft ).

Figure 2-3. Hewlett-Packard Interface Bus Connection

## Mating Connectors (cont'd)

Coaxial Connectors. Coaxial mating connectors used with the Carrier Noise Test Set should be 50 ohm Type N and 50 ohm BNC male connectors.

## 2-10. Operating Environment

The operating environment should be within the following limitations:
 Humidity ........... . . $5 \%$ to $95 \%$ relative at $40^{\circ} \mathrm{C}$ Altitude $. \ldots . . . . . . . .<4600$ metres ( 15000 feet)

## 2-11. Bench Operation

The instrument cabinet has plastic feet and foldaway tilt stands for convenience in bench operation. (The plastic feet are shaped to ensure selfalignment of instruments when they are stacked.) The tilt stands raise the front of the Carrier Noise Test Set for easier viewing of the front panel.

## 2-12. Rack Mounting

## WARNING

The Carrier Noise TestSet weighs 10.4 kg (23 lb.), therefore care must be exercised when lifting to avoid personalinjury. Use equipment slides when rack mounting.

Rack mounting information is provided with the rack mounting kits. If the kits were not ordered with the instrument as options, they may be ordered through the nearest Hewlett-Packard office. Refer to the paragraph entitled Mechanical Options in Section I.

## 2-13. STORAGE AND SHIPMENT

## 2-14. Environment

The instrument should be stored in a clean, dry
environment. The following environmental limitations apply to both storage and shipment:
Temperature..............$-55^{\circ} \mathrm{C}$ to $+75^{\circ} \mathrm{C}$ Humidity $\ldots \ldots \ldots \ldots \ldots<95 \%$ relative at $40^{\circ} \mathrm{C}$ Altitude 15300 metres ( 50000 feet)

## 2-15. Packaging

Tagging for Service. If the instrument is being returned to Hewlett-Packard for service, please complete one of the blue repair tags located at the back of this manual and attach it to the instrument.

Original Packaging. Containers and materials identical to those used in factory packaging are available through Hewlett-Packard offices. Mark the container "FRAGILE" to assure careful handling. In any correspondence refer to the instrument by model number and full serial number.

Other Packaging. The following general instructions should be used for re-packaging with commercially available materials:
a. Wrap the instrument in heavy paper or plastic. (If shipping to a Hewlett-Packard office or service center, complete one of the blue tags mentioned above and attach it to the instrument.)
b. Use a strong shipping container. A doublewall carton made of $2.4 \mathrm{MPa}(350 \mathrm{psi})$ test material is adequate.
c. Use enough shock-absorbing material ( 75 to 100 mm layer; 3 to 4 inches) around all sides of the instrument to provide firm cushion and prevent movement in the container. Protect the front panel with an appropriate type of cushioning material to prevent damage during shipment.
d. Seal the shipping container securely.
e. Mark the shipping container "FRAGILE" to assure careful handling.


## SECTION III OPERATION

## 3-1. INTRODUCTION

This section provides complete operating information for the Carrier Noise Test Set. Included are general operation instructions; detailed descriptions of each front and rear panel key, connector, switch and annunciator; information on remote operation; operator's checks; and operator's maintenance procedures.

## 3-2. Local Operation

Information covering local operation of the Carrier Noise Test Set is given in two places, namely detailed panel features and general operating instructions.

Detailed Panel Features. Figure 3-1 and Figure 3-2 illustrate the front and rear panels of the Carrier Noise Test Set and provide descriptions of each key, connector, switch and annunciator.

General Operating Instructions. Under general operating structions the following topics are covered:

- Power-on sequences
- Power-on procedure
- Phase noise measurement using the Phase Detector Method
- Phase noise measurement using the Frequency Discriminator Method
- AM noise measurement


## 3-3. Remote Operation (HP-IB) $\mathrm{HP}-I B$

The Carrier Noise Test Set is capable of remote operation via the Hewlett-Packard Interface Bus. Knowledge of local operation is essential for HPIB programming since most of the data messages contain the same keystroke-like sequences. HP-IB
information is presented in the following areas of this section:

- A summary of HP-IB capabilities is provided in Table 3-3.
- A summary of program codes is provided in Table 3-4.


## 3-4. Operator's Checks

Operator's checks are simple procedures designed to verify that the main functions of the Carrier Noise Test Set operate properly.

These procedures require a microwave synthesized source, an RF synthesized signal generator, a spectrum analyzer, a controller (for HP-IB checks) and interconnecting cables.

## 3-5. Operator's Maintenance <br> WARNING

For continued protection against fire hazard, replace the line fuse with a 250 V fuse of the same rating only. Do not use repaired fuses or short-circuited fuseholders.

The only maintenance that the operator should normally perform is the replacement of the primary power fuse. All other maintenance should be referred to qualified service personnel.

The primary power fuse is located within the Line Power Module. Refer to Figure 2-1 for instructions on how to change the fuse.

If the instrument does not operate properly and is being returned to Hewlett-Packard for service, please complete one of the blue tags located at the end of this manual and attach it to the instrument. Refer to Section II for packaging instructions.

## FRONT PANEL FEATURES



1. PHASE LOCK INDICATOR. The primary purpose of the PHASE LOCK INDICATOR is to show when the device under test and the tunable $5-1280 \mathrm{MHz}$ source are in phase quadrature (that is, 90 degrees out of phase). When the device under test and the tunable $5-1280 \mathrm{MHz}$ source are in phase quadrature a green LED will be illuminated in the center of the PHASE LOCK INDICATOR. When the two sources are greater than 100 kHz apart a red LED will be illuminated to the left or right of the green LED. As the frequency difference decreases all the LEDs will light up dimly. Finally, as the two sources approach quadrature the LEDs will fully light one at a time, from left to right. When the center green LED is illuminated the two sources are in phase quadrature.
2. BAND RANGE. BAND RANGE describes the range of microwave test signals that can be input for each of the buttons below FILTER RANGE. The BAND RANGE chosen must contain the microwave test signal. The BAND RANGE desired is enabled by pressing the button below that BAND RANGE.
3. FILTER RANGE. FILTER RANGE describes the range of microwave test signals that can be accepted by the Carrier Noise Test Set ( $0.010-$ 18 GHz ).
4. BAND CENTER. The broad range of microwave test signals is possible because of a 640 MHz comb generator in the Carrier Noise Test Set. Through a series of filters certain harmonics from the comb generator are passed. The

BAND CENTER frequency of the BAND RANGE chosen is the only harmonic (combline) from the comb generator that is passed. The filter used for selecting the harmonic is a 200 MHz passband filter centered around the combline.
5. AUX NOISE. This is a female BNC connector with an output impedance of $600 \Omega$. The signal output is a dc level that is proportional to the phase difference between the microwave test signal and the tunable $5-1280 \mathrm{MHz}$ signal. The dc level has ac fluctuations directly proportional to the phase noise of the microwave test signal, if the phase noise of the 640 MHz signal and the tunable $5-1280 \mathrm{MHz}$ signal is less than the microwave test signal. The output and an oscilloscope can be used as an external quadrature monitor, because of the direct proportionality of the dc level to the phase difference of the microwave test signal and the tunable $5-1280 \mathrm{MHz}$ signal.
6. NOISE SPECTRUM $<1 \mathrm{MHz}$ OUTPUT. This is a female BNC connector with an output impedance of $600 \Omega$. This output is useful for measuring the phase noise of the device under test at offsets from the carrier of dc to 1 MHz .

The signal output is a dc level directly proportional to the phase difference between the microwave test signal and the tunable $5-1280 \mathrm{MHz}$ signal. The dc level has ac fluctuations that are directly proportional to the phase noise of the the microwave test signal, if the phase noise of the 640 MHz signal and $5-1280 \mathrm{MHz}$ signal is less than the microwave test signal.

Figure 3-1. Front Panel Features (1 of 3)

## FRONT PANEL FEATURES

## NOTE

The bandwidth (dc to 1 MHz ) is not completely flat. The 3 db points are at dc and 1.5 MHz.
7. $\mathbf{5}$ to $\mathbf{1 2 8 0} \mathbf{~ M H z}$ INPUT. This is a female type-N connector with a $50 \Omega$ input impedance. The frequency of the input signal is $5-1280 \mathrm{MHz}$ from a tunable source. The frequency of the signal input is set to equal the microwave test signal minus the BAND CENTER frequency of the BAND RANGE chosen. The input level should be $0 \mathrm{dBm} \pm 1 \mathrm{dBm}$. The user sets this signal in phase quadrature (that is, 90 degrees out of phase) with the microwave test signal. The IF OUTPUT is connected to this input, through a delay line, for the Frequency Discriminator Method of making a phase noise measurement.
8. MICROWAVE TEST SIGNAL INPUT. This is a female type-N connector with a $50 \Omega$ input impedance. This connector is used to connect the microwave test signal to the Carrier Noise Test Set. The input frequency range is 10 MHz to 18 GHz . The input level should be as follows:

For test frequencies $>1.28 \mathrm{GHz}:+7 \mathrm{dBm}$ to +20 dBm (Typically usable down to -15 dBm with potential noise floor degradation). The optimal level is +7 dBm to +20 dBm .

For test frequencies $<1.28 \mathrm{GHz}:-5 \mathrm{dBm}$ to +10 dBm (Typically usable down to -15 dBm with potential noise floor degradation. The optimal level is from -2 dBm to +3 dBm .)

## 9. NOISE SPECTRUM<10 MHz OUTPUT. This

 is a female BNC connector with an output impedance of $50 \Omega$ and 40 dB of gain over the $<1 \mathrm{MHz}$ OUTPUT. This output is useful for measuring the phase noise or amplitude (AM) noise of the device under test at offsets from the carrier of 10 Hz to 10 MHz .The signal output is a dc level that is directly proportional to the phase difference between the microwave test signal and the tunable 5-1280 MHz signal. The dc level has ac fluctuations
that are directly proportional to the phase noise of the microwave test signal, if the phase noise of the 640 MHz signal and the tunable $5-1280$ MHz signal is less than the microwave test signal.

## NOTE

The bandwidth ( 10 Hz to 10 MHz ) is not completely flat. The 3 dB points are at 10 Hz and 15 MHz .
10. IF OUTPUT $5 \mathbf{- 1 2 8 0} \mathbf{M H z}$. This is a female BNC connector with an output impedance of $50 \Omega$. The output frequency will be 5 to 1280 MHz . The exact frequency is the intermediate difference frequency (IF) from the mixing of the microwave test signal and the BAND CENTER frequency of the BAND RANGE chosen. The output level is +7 dBm minimum.
11. 50 OHM TERMINATION. With the $50 \Omega$ termination connected to the IF OUTPUT the Carrier Noise Test Set meets the requirements of MIL STD 461 RE02. The IF OUTPUT is fully useable, just replace the 50 Ohm termination when the IF OUTPUT is not being used.
12. HP-IB ANNUNCIATORS. Display the HP-IB status. The REMOTE (RMT) annunciator lights when the Carrier Noise Test Set is in the remote mode. The TALK (TLK) annunciator lights when the Carrier Noise Test Set is addressed to talk. The LISTEN (LSN) annunciator lights when the Carrier Noise Test Set is addressed to listen. The SRQ annunciator lights when the Carrier Noise Test Set is sending a Require Service message to the controller.
13. LOCAL. Returns the Carrier Noise Test Set to local operation (front panel control) from remote HP-IB control provided that the instrument is not in Local Lockout.
14. BAL. This adjustment is used when making a measurement on a pulsed signal. This adjustment with the aid of an oscilloscope connected to the AUX NOISE connector on the front panel, is used to eliminate the dc offset in the phase lock loop.

Figure 3-1. Front Panel Features (2 of 3)

## FRONT PANEL FEATURES


15. MEASUREMENT ANNUNCIATORS. When a continuous wave (CW) phase noise measurement is selected the $\phi$, CW annunciator will be illuminated. When a continuous wave (CW) AM noise measurement is selected the AM, CW annunciator will be illuminated. When a pulsed phase noise measurement is selected the $\phi$, PULSED annunciator will be illuminated. When a pulsed AM noise measurement is selected the AM, PULSED annunciator will be illuminated.
16. MODE. Used to select either a phase noise (CW or pulsed) or AM noise (CW or pulsed) measurement. AM noise is only installed with Option 130.
17. LOCK BANDWIDTH FACTOR. These five switches partially control the bandwidth of the phase lock loop, by setting the gain for a number of operational amplifiers in the Carrier Noise Test Set. Another factor in determing the loop
andwidth is the frequency of the microwave test signal or the FM deviation set on the device under test or the tunable $5-1280 \mathrm{MHz}$ source.
18. LINE SWITCH. Applies ac power to the Carrier Noise Test Set when set to the ON position.
19. CAPTURE. When CAPTURE is pressed the phase lock loop is changed from a second order loop to a first order loop. The phase lock loop consists of a voltage controlled oscillator (the tunable $5-1280 \mathrm{MHz}$ source or the device under test), a phase detector and loop filter. The phase detector and loop filter are in the Carrier Noise Test Set. By changing to a first order loop the bandwidth of the loop is widened. By widening the loop bandwidth, acquiring phase quadrature is made easier. When CAPTURE is pressed the LOCK BANDWIDTH FACTOR buttons are overridden.

Figure 3-1. Front Panel Features (3 of 3)

## REAR PANEL FEATURES



1. $\mathbf{6 4 0} \mathbf{~ M H z ~ O U T}$. This is a female SMA connector with an output impedance of 50 Ohms . The output frequency is 640 MHz . The output level is $11-13 \mathrm{dBm}$. This output is used to generate an internal 640 MHz signal when connected to the 640 MHz IN connector. When this output is not in use it must be terminated with the 50 Ohm termination that was shipped with the Carrier Noise Test Set.
2. LOOP TEST PORT IN. If a phase noise measurement is made within the phase lock loop bandwidth some of the phase noise will be suppressed. The LOOP TEST PORT IN connector lets the user input a signal to determine the transfer characteristic of the phase lock loop. Once the transfer characteristic is known the amount of noise suppression at any offset within the loop bandwidth can be determined. The amount of phase noise suppression is then used to correct the measured phase noise level.
This is a dc coupled female BNC connector with a nominal input impedance of $10 \mathrm{k} \Omega$. The signal input should be from a random noise source, a tracking generator or a variable frequency sine wave source. The input level is typically less than 0.1 volts peak. The typical bandwidth is dc to 100 kHz .
3. FREQ-CONT X-OSC. This output is to be connected to the frequency control input of the tunable $5-1280 \mathrm{MHz}$ source or the device under
test (whichever is being used as the loop VCO ) if the loop VCO requires $\pm 10$ volts dc for tuning. When so connected the loop VCO will change frequency to maintain phase quadrature between the device under test and the tunable 5-1280 MHz source.
This is a female BNC connector with an output impedance of $100 \Omega$. The output level is nominal from -10 volts de to +10 volts dc.
4. HP-IB ADDRESS SWITCH. Used to select one of 31 valid HP-IB addresses ( 00 through 30 ). The address is set in binary with A5 as the most significant bit and A1 as the least significant. To set a bit, "bit=", slide the switch down. To clear a bit, "bit=0", slide the switch up. By setting TALK ONLY "TO" or LISTEN ONLY "LO" TO " 1 " the HP-IB address is overriden. When the address is changed the Carrier Noise Test Set must be turned off then back on. This is necessary so the microprocessor will be aware of the address change.
5. SERIAL NUMBER PLATE. First four digits and letter constitute the prefix which defines the instrument configuration. The last five digits form a sequential suffix that is unique to each instrument. The plate also indicates any options supplied with the instrument.
6. PULSED BASEBAND. These connectors are used when making a pulsed measurement. The

## REAR PANEL FEATURES


user connects a filter between the input and output to filter the pulse repetition frequency off the carrier. The filter chosen is dependent on the pulse repetition frequency of the carrier. The design of the filter must be such that the pulse repetition frequency and its multiples are terminated into 50 Ohms.
7. FUSE. Ordering information is presented in Section II, Installation.
8. LINE POWER MODULE. Permits operation from $100,120,220$, or 240 Vac . The number visible in the window indicates nominal line voltage to which the instrument must be connected (see Figure 2-1). Center conductor is connected to the chassis for earth grounding.
9. HP-IB CONNECTOR. 24-pin female connector used to connect the Carrier Noise Test Set to the Hewlett-Packard Interface Bus (HP-IB) for remote operation. Connection information is presented in Section II, Installation.
10. FREQ-CONT DC-FM. This output is to be connected to the frequency control input of the tunable 5-1280 MHz source or the device under test (whichever is being used as the loop VCO) if the loop VCO requires $\pm 1$ volt dc for tuning. When so connected the loop VCO will change
frequency to maintain phase quadrature between the device under test and the tunable 5-1280 MHz source.
This is a female BNC connector with a nominal output impedance of $50 \Omega$. The output level is nominal from -1 volt de to +1 volt dc.
11. LOOP TEST PORT OUT. Once a signal has been input at the LOOP TEST PORT IN connector, this output is connected to a spectrum analyzer for displaying the phase lock loop transfer characteristic.

This is a dc coupled female BNC connector with a nominal output impedance of $1 \mathrm{k} \Omega$. The gain outside the phase lock loop bandwidth is equal to one.
12. 640 MHz INPUT. This is a female BNC connector with a 50 Ohm input impedance. The input frequency must be $640 \mathrm{MHz} \pm 32 \mathrm{kHz}$. The input level must be +1 dBm to +4 dBm .
13. 50 Ohm TERMINATION. For proper operation of an amplifier inside the Carrier Noise Test Set this termination must be connected to the 640 MHz OUT connector. The 640 MHz OUT connector is fully usable, just replace the 50 Ohm termination when the 640 MHz OUT connector is not being used.

Figure 3-2. Rear Panel Features (2 of 2)

## OPERATOR'S CHECKS

## 3-6. OPERATOR'S CHECKS

Description Use the test set-up shown below to verify the front panel controlled functions are being executed by the microprocessor.


Figure 3-3. Basic Functional Checks Test Setup

| Equipment | RF Synthesized Signal Generator (tunable reference) <br> Microwave Synthesized Source <br> (D.U.T.) <br> Computer Controller <br> RF Spectrum Analyzer | HP 8662A <br> (Option 003) <br> HP 8340A <br> HP 85B <br> HP 8566B |
| :---: | :---: | :---: |
| Procedure | Microprocessor Checks |  |

1. Turn on and warm up all instruments for 30 minutes before proceeding.
2. Switch the Carrier Noise Test Set to ON and observe the front panel annunciators. An internal memory check of ROM and RAM is initiated when the Carrier Noise Test Set is switched on. If the memory system is working properly, all front panel annunciators will light for approximately 1.5 seconds. This also provides a quick visual inspection of each front panel annunciator.

If memory failure is detected, no front panel annunciators will light during the 1.5 second time period.

## OPERATOR'S CHECKS

## 3-6. OPERATOR'S CHECKS (cont'd)

Procedure (cont'd)
3. Press the FILTER RANGE buttons and MEASUREMENT MODE button. The clicking sound verifies the switching control of the microprocessor and the switch operation.

IF OUTPUT Check (Using an external source to supply the $\mathbf{6 4 0} \mathbf{~ M H z}$ signal)
4. Set the D.U.T. as follows:

Frequency ......................... 2.32 GHz
Amplitude ......................... +10 dBm
5. Set the Carrier Noise Test Set as follows:

Band center ....................... 1.92 GHz
Measurement Mode ................... $\phi$, CW
6. Adjust the spectrum analyzer to display the 400 MHz IF OUTPUT (D.U.T. frequency minus BAND CENTER frequency).

NOTE
Present at the IF OUTPUT will be the IF signal (signal under test minus the BAND CENTER frequency of the BAND RANGE chosen), IF harmonics and spurious signals. Any IF harmonics or spurious signals can be disregarded. The signal with the highest amplitude is the desired signal.

The harmonics of the IF signal do not affect the phase noise measurement since the NOISE SPECTRUM OUTPUTS are filtered. The spurious signals may appear as sidebands on the IF signal and as spurs at the NOISE SPECTRUM OUTPUTS.
7. Check that the IF OUTPUT level is above the specified limit of +7 dBm minimum. Record the actual value of the IF OUTPUT frequency and level in Table 3-1.
8. If the IF OUTPUT frequency and level did not measure within specified limits check the frequency and power level of the 640 MHz IN signal and the microwave test signal. If a problem still exists refer to the troubleshooting on Service Sheet 1.
9. Change the frequency of the D.U.T to the next microwave test signal frequency listed in Table 3-1. Change the BAND RANGE on the front panel to the nextBAND CENTER listed in Table 3-1.
10. Measure the IF OUTPUT frequency and level with the spectrum analyzer. Record the values and repeat the measurement for each of the BAND CENTER frequencies listed.

## IF OUTPUT Check (Using the 640 MHz oscillator in the Carrier Noise Test Set)

11. Leave the settings on the D.U.T. and Carrier Noise Test Set to those that were used for the last measurement in step 10.

## OPERATOR'S CHECKS

## OPERATOR'S CHECKS (cont'd)

Procedure (cont'd)
12. Disconnect the cable to the 640 MHz IN connector, on the rear panel of the Carrier Noise Test Set.
13. Disconnect the SMA termination from the 640 MHz OUT connector, on the rear panel of the Carrier Noise Test Set.
14. Connect the 640 MHz OUT connector to the 640 MHz IN connector using the cable-attenuator assembly (HP 11729-60096 or HP 11729-60098 [Option 140]) that was shipped with the Carrier Noise Test Set.

NOTE
It is essential that the cable-attenuator assembly that was shipped with the Carrier Nosie Test Set be used to make the connection.
15. Measure the IF OUTPUT frequency and level with the spectrum analyzer. Verify that the typical frequency measured is 400 MHz and the level is greater than +7 dBm .
16. Disconnect the cable between the 640 MHz OUT and 640 MHz IN connectors.
17. Reconnect the 50 Ohm SMA termination to the 640 MHz OUT connector.
18. Reconnect the 640 MHz signal from the tunable reference to the 640 MHz IN connector on the Carrier Noise Test Set.

Table 3-1. IF Output Check

| Microwave Test Signal [GHz] | Band Center [GHz] | IF Output Frequency (MHz) |  | IF Output Level (dBm) |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Actual | Typical | Minimum | Actual |
| 2.32 | 1.92 |  | 400 | +7 |  |
| 4.88 | 4.48 |  | 400 | +7 |  |
| 7.44 | 7.04 |  | 400 | +7 |  |
| 10.00 | 9.60 |  | 400 | +7 |  |
| 12.56 | 12.16 |  | 400 | $+7$ |  |
| 15.12 | 14.72 |  | 400 | +7 |  |
| 17.68 | 17.28 |  | 400 | +7 |  |

## Phase Lock Check

19. Connect the $<10 \mathrm{MHz}$ OUTPUT from the Carrier Noise Test Set to the RF spectrum analyzer.
20. Set the Carrier Noise Test Set as follows:

Lock Bandwidth Factor .................. 100
Measurement Mode .................. $\phi$, CW
Band Range ............. 8.32 to 10.88 GHz

## OPERATOR'S CHECKS

## OPERATOR'S CHECKS (cont'd)

NOTE
If this filter is not included in the Carrier Noise Test Set, select an available BAND RANGE.
21. Set the D.U.T. as follows:

Frequency $\ldots \ldots \ldots \ldots \ldots \ldots \ldots . .10 \mathrm{GHz}$
Amplitude $\ldots \ldots \ldots \ldots \ldots \ldots \ldots+10 \mathrm{dBm}$
NOTE
The test signal is tuned 400 MHz above the center frequency of the BAND RANGE selected on the Carrier Noise Test Set
22. Set the tunable reference as follows:

Frequency ......................... 400 MHz
Amplitude ............................ 0 dBm
23. Press and release CAPTURE, on the Carrier Noise Test Set, to phase lock the D.U.T. to the tunable reference.

If the sources do not phase lock (green bar does not remain illuminated on the front panel phase lock indicator) the tunable reference must be tuned closer in frequency to the IF frequency ( $f_{I F}=f_{\text {D.U.T. }}-f_{\text {band center frequency }}$ ). Press CAPTURE while tuning the tunable reference in 1 kHz steps. Watch the phase lock indicator on the Carrier Noise Test Set. When the LED's on the indicator all light up, reduce the resolution of the tunable reference by a factor of 10 .

NOTE
Connect the spectrum analyzer to the $<10 \mathrm{MHz}$ OUTPUT, on the Carrier Noise Test Set, if difficulties occur in determining the direction to tune the tunable reference to acquire phase lock.

> The signals displayed on the spectrum analyzer represent the frequency difference between the two inputs to an internal mixer/phase detector in the Carrier Noise Test Set. The signals will decrease in frequency to dc when tuning towards phase lock and increase in frequency when tuning away from phase lock.

Press CAPTURE and tune in this reduced resolution. Watch the red LEDS on the Carrier Noise Test Set phase lock indicator step through one side of the display - to the green bar - then to the other side of the display. Again reduce the resolution on the tunable reference by a factor of 10 . Tune in this finer resolution until the green LED is illuminated. When the green LED is illuminated release CAPTURE.

## Display Deviation Check

24. If the Carrier Noise Test Set is not phase locked perform the phase lock check (steps 19-23).
25. Hold CAPTURE in and increase the tunable reference in 10 Hz steps until the loop becomes unlocked. Watch the phase lock indicator, the red LEDs should fully light

## OPERATOR'S CHECKS

## OPERATOR'S CHECKS (cont'd)

Procedure (cont'd)
one at a time and move to the right. When the last LED is illuminated and you tune further the entire indicator should dimly light.

With CAPTURE pressed decrease the tunable reference in 10 Hz steps. The dimly illuminated indicator should change back to the red LEDs one at a time fully illuminated and moving to the left. When the last LED on the left is illuminated and you tune further, the entire indicator will dimly light.
26. When the last LED on the left or right lights and the tunable reference is increased or decreased further, the indicator should immediately dimly light. If the indicator goes blank perform the phase lock indicator adjustments in Section V.

## AM Mode Check

NOTE
Perform this check only when the AM Noise Option is installed.
27. Set the Carrier Noise Test Set as follows:

Measurement Mode ................ AM, CW
All other functions ................ Not used
28. Set the D.U.T. as follows:

Frequency .............................. 1 GHz
Amplitude ........................ +10 dBm
29. AM modulate the microwave test signal at a 1 kHz rate.
30. Adjust the spectrum analyzer to view the 1 GHz signal and the 1 kHz AM sidebands.
31. Adjust the percent of AM modulation so that the 1 kHz AM sidebands are 40 dB below the 1 GHz carrier. (approximately a $2 \%$ depth)
32. Disconnect the microwave test signal from the spectrum analyzer. Connect the microwave test signal to the MICROWAVE TESTSIGNALINPUT on the Carrier Noise Test Set.
33. Connect the $<10 \mathrm{MHz}$ OUTPUT, on the Carrier Noise Test Set, to the spectrum analyzer.
34. Adjust the spectrum analyzer to view the 1 kHz detected signal. AM MODE is operating if the 1 kHz signal level is $-7 \mathrm{dBm} \pm 3 \mathrm{dBm}$.

## HP-IB Address Verification

35. Press and hold the front panel LOCAL key. The LED's on the BAND RANGE select buttons will display the current address in binary.
36. Check the address switch setting on the rear panel of the Carrier Noise Test Set to verify the display on the BAND RANGE select buttons is correct.

## OPERATOR'S CHECKS

## OPERATOR'S CHECKS (cont'd)

## Procedure (cont'd) <br> Local/Remote Operation Check <br> 37. Set the Carrier Noise Test Set to remote using the following:

## Remote 706

38. Press any front panel key except LOCAL to verify that the front panel keys are disabled.
39. Press the LOCAL key. This switches the instrument out of the remote mode.

## NOTE

When the local key is pressed the REMOTE annunciator will turn off, but the LISTEN annunciator will stay illuminated.

Now press any front panel key to verify the front panel keys are enabled.

## Status Byte Check

40. Enter Program 1 into the computer. Insert the correct select code and HP-IB address, for your Carrier Noise Test Set, into the SPOLL function. The HP-IB address of the Carrier Noise Test Set is factory preset to 06 . The user can select the HP-IB address by changing the position of the HP-IB address switches on the rear panel of the Carrier Noise Test Set. (Refer to Section II paragraph 2-7, HP-IB Address Selection, for further information.)

## PROGRAM 1

| 10 A $=$ SPOLL(\#\#\#) | (\#\#\# = Current Carrier Noise Test Set select code |
| :--- | :--- |
| 20 DISP A | and address.) |
| 30 GOTO 10 | Example: 706 |
|  | $7=$ Select code |
|  | $06=$ Address |

This program monitors the status byte of the Carrier Noise Test Set and displays the equivalent decimal value on the computer. The status of the phase lock detector sent out over HP-IB should agree with the phase lock indicator on the front panel. Table 3-2 defines the status bits and their decimal equivalents for the two phase lock conditions.

Table 3-2. Status Bits and Their Decimal Equivalents for Two Phase Lock Conditions

| Phase <br> Condition | Status Bits-Binary |  |  |  |  |  |  |  | Computer Output* |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0108 | 0107 | 0106 | D105 | D104 | D103 | D102 | D101 |  |
| unlocked | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 4 |
| locked (green Bar) | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 2 |
| *If no other bits are logical one. |  |  |  |  |  |  |  |  |  |

## OPERATOR'S CHECKS

## OPERATOR'S CHECKS (cont')

Procedure (cont'd)
41. Set the Carrier Noise Test Set to the phase lock condition (green LED is illuminated on the front panel phase lock display). For help use the phase lock check (steps 19-23).
42. Run Program 1 and compare the number displayed on the computer to the phase condition of the phase lock indicator on the Carrier Noise Test Set. The computer displays a decimal 2 when in the phase lock condition.
43. Increase the frequency of the tunable reference by 1 MHz . Verify that the unlocked condition (red LED adjacent to the left of the green LED) is detected by the microprocessor. A decimal 4 should be displayed on the computer.

If the number ( 2 or 4) displayed on the computer does not correspond to the phase lock condition, displayed on the front panel phase lock indicator, perform the phase lock indicator adjustment procedures in Section V. Run Program 1 again to verify
the adjustments.

## 3-7. GENERAL OPERATING INSTRUCTIONS

## WARNING

Before the Carrier Noise Test Set is switchedon, allprotective earthterminals, extension cords, autotransformers, and devices connected to the instrument should be connected to a protective earth grounded socket. Any interruption of the protective earth grounding will cause a potential shock hazard that could result in personal injury.


Before the Carrier Noise Test Set is switched on, it must be set to the same line voltage as the power source or damage to the instrument may result.

## 3-8. Turn On

Turn-on Procedure. If the Carrier Noise Test Set is already plugged in, set the LINE switch to ON.

If the power cable is not plugged in, follow these instructions.

On the rear panel:

1. Check the line voltage selection card for correct voltage selection.
2. Check the fuse for correct current rating. The current rating is printed on the line power module label.
3. Plug in the power cable.

On the front panel, set the LINE switch to ON.
Turn-on Sequence. The Carrier Noise Test Set performs a quick memory check (ROM and RAM) at turn-on. During this check, all front panel annunciators light for approximately 1.5 seconds to allow a quick visual inspection of each front panel annunciator. If a memory failure is detected the front panel annunciators will not light during the 1.5 second time period.

Following the memory check the Carrier Noise Test Set powers up as follows:

Measurement - $\phi$, CW
Band Range - Band 1 ( $0.010-1.28 \mathrm{GHz}$ )
Lock Bandwidth Factor - 100
NOTE
For the Carrier Noise Test Set to be operational it may require one or both of
the following drive signals when making a phase noise measurement:

- A synthesized 640 MHz signal
- A tunable 5 to 1280 MHz signal

The drive signals can be supplied by an external RF source or the Carrier Noise Test Set can be configured to provide an internally generated 640 MHz signal that can supply the 640 MHz drive signal. The absolute system noise floor will be degraded close-in to the carrier when using the internally generated 640 MHz signal, compared to the 640 MHz signal being supplied by the HP 8662A Synthesized Signal Generator.
When using the Carrier Noise Test Set to make an AM noise measurement none of the drive signals are required.
The number of drive signals required is dependent on the measurement method chosen and the frequency of the signal under test.
The following table lists when the drive signals are required:

| Drive <br> Signal | Phase Detector <br> Method |  | Frequency <br> Discriminator Method |  |
| :--- | :---: | :---: | :---: | :---: |
|  | Frequency Range of <br> Signal Under Test | Frequency Range <br> of Signal Under Test |  |  |
|  | 10 MHz <br> to 1.28 <br> GHz | 1.28 GHz <br> to 18 GHz | 10 MHz <br> to 1.28 <br> GHz | 1.28 GHz <br> to 28 GHz |
|  | Not <br> needed | X | Not <br> needed | X |
| Tunable <br> $5 — 1280$ <br> MHz <br> Source | X | X | Not <br> needed | Not <br> needed |
| $\mathrm{X}=$ Drive signal is needed. |  |  |  |  |

## 3-9. PHASE NOISE MEASUREMENT

## 3-10. Phase Detector Method

 NOTEThe 640 MHz and 5-1280 MHz signals may come from the following sources:

- Two synthesized sources.
- One synthesized source and one cavity tuned source.
- Two cavity tuned sources.

${ }^{1}$ The FREQ-CONT signal can be connected to the source supplying the $5-1280 \mathrm{MHz}$ signal or the device under test.
${ }^{2}$ Two sources can supply the 640 MHz and $5-1280 \mathrm{MHz}$ signals. For important information see the note at the beginning of paragraph 3-10
${ }^{3}$ The NOISE SPECTRUM, ( $<1 \mathrm{MHz}$ or $<10 \mathrm{MHz}$ ) that is connected to the spectrum analyzer, depends on the offset of interest and the input impedance of the spectrum analyzer.

Figure 3-4. Interconnections to the Carrier Noise Test Set when making a Phase Noise Measurement [Using the Phase Detector Method)

## Phase Detector Method (cont'd)

Each configuration will have a different absolute system noise floor. The absolute system noise floor is a function of the noise contributions from the 640 MHz signal, 51280 MHz signal and the HP 11729C.

To calculate the absolute system noise floor use the following formula:

$$
\mathcal{L}_{\text {system }}=10 \log \left(N^{2} \times \frac{\mathcal{L}_{1}}{10^{10}}+\frac{\mathcal{L}_{2}}{10^{10}}+\frac{\mathcal{L}_{3}}{10^{10}}\right)
$$

where

$\mathcal{L}_{1}=$ absolute SSB phase noise of the 640 MHz reference signal ( $\mathrm{dBc} / \mathrm{Hz}$ )
$\mathcal{L}_{2}=$ absolute SSB phase noise of the 51280 MHz tunable signal dBc/Hz
$\AA_{3}=$ residual noise of the HP 11729C (dBc/Hz)

Two synthesized sources with their crystal time bases connected externally will give the lowest close in noise floor performance. When a synthesized source and a cavity tuned source are used the 640 MHz signal should come from the synthesized source. A synthesized source is desired for the 640 MHz signal since the 640 MHz signal multiplied to a microwave frequency is the major contributor to the system noise floor. If the cavity tuned source selected has a wide DC-FM bandwidth and Loop Holding Range this will help to phase lock a drifting source. If two cavity tuned sources are used the absolute system noise floor close-in will be degraded but the noise floor further out will be better.

1. Figure $3-4$ shows the interconnections to the Carrier Noise Test Set when making a phase noise measurement.
2. Be sure the LINE MODULE, on the rear panel, is set to the available line voltage. If it needs to be changed see Figure 2-1 in Section II.

## Phase Detector Method (cont'd)

3. Plug the Carrier Noise Test Set into the available line supply.
4. Turn the Carrier Noise Test Set on and allow a 30 minute warm-up before making any measurements.
5. If the microwave test signal is in the range of $0.010-1.28 \mathrm{GHz}$ go to step 6 . If the microwave test signal is greater than 1.28 GHz follow the instructions for step 5.
Using a coaxial cable connect the synthesized 640 MHz source to the 640 MHz IN connector on the rear panel.

To configure and use the internal 640 MHz oscillator connect the 640 MHz OUT connector to the 640 MHz IN connector with the cable-attenuator assembly (HP 11729-60096 or HP 11729-60098 [Option 140]) provided. Both connectors are on the rear panel. Be sure to make the connection using the cable-attenuator assembly that was shipped with the Carrier Noise Test Set.

## NOTE

The absolute system noise floor will be degraded close-in to the carrier when using the internally generated 640 MHz signal, compared to the 640 MHz signal being supplied by the HP 8662A Synthesized Signal Generator.
6. Using a coaxial cable connect the FREQCONT X-OSC or FREQ-CONT DC-FM, on the rear panel, to an electronic frequency control port on either the tunable $5-1280 \mathrm{MHz}$ source or the device under test.
Either FREQ-CONT X-OSC or FREQ-CONT DC-FM can be used to control the voltage controlled oscillator (VCO) of the phase lock loop. The output chosen will depend on the control voltage required for the VCO. FREQ-CONT X-OSC has an output voltage of -10 volts dc to +10 volts dc. FREQ-CONT DC-FM has an output voltage of -1 volt dc to +1 volt dc. When either output is used the device under test and the tunable $5-1280 \mathrm{MHz}$ source will be maintained in phase quadrature (that is, 90 degrees out of phase).
7. Using a coaxial cable connect the tunable 51280 MHz source to the $5-1280 \mathrm{MHz}$ IN con-
nector on the front panel. Be sure the tunable 5 to 1280 MHz source is set to 0 dBm .
8. Using a coaxial cable connect the device under test to the MICROWAVE TEST SIGNAL INPUT on the front panel.
9. Using a coaxial cable connect one of the NOISE SPECTRUM OUTPUTS $<1 \mathrm{MHz}$ or $<10 \mathrm{MHz}$, on the front panel, to a spectrum analyzer. The $<1 \mathrm{MHz}$ OUTPUT is useful for measuring phase noise at offsets from dc to 1 MHz . The $<10 \mathrm{MHz}$ OUTPUT is useful for measuring phase noise at offsets from 10 Hz to 10 MHz and has 40 dB of gain over the $<1 \mathrm{MHz}$ OUTPUT. The $<1 \mathrm{MHz}$ OUTPUT has an output impedance of $600 \Omega$ and the $<10 \mathrm{MHz}$ OUTPUT has an output impedance of $50 \Omega$.

## NOTE

Do not use the $<10 \mathrm{MHz}$ NOISE SPECTRUM OUTPUT for test signals $\pm 20 \mathrm{MHz}$ around the BAND CENTER frequency. High feedthrough signals (mixer sum products and LO signals) saturate the Low Noise Amplifier in the Carrier Noise Test Set and possibly the spectrum analyzer.
Do not use the $<1 \mathrm{MHz}$ NOISE SPECTRUM OUTPUT for test signals $\pm 5 \mathrm{MHz}$ around the BAND CENTER frequency. LO feedthrough may possibly saturate the spectrum analyzer.
For test signals $\pm 5 \mathrm{MHz}$ to 10 MHz around the BAND CENTER frequency the measured noise level will be 0 dBm to +3 dBm greater than the actual level. The error is caused by an impedance change on the input of the internal Low Noise Amplifier.
For test signals $\pm 10 \mathrm{MHz}$ to 20 MHz around the BAND CENTER frequency the measured noise level will be 0 dBm to +1 $d B m$ greater than the actual level. Again the error is caused by an impedance change on the input of the Low Noise Amplifier.
Therefore, the $<1 \mathrm{MHz}$ OUTPUT can be used for test signals $\pm 5 \mathrm{MHz}$ to 20 MHz around the BAND CENTER frequency by subtracting the maximum error amount from the measured level.
10. To select a PHASE NOISE MEASUREMENT press the MODE button ,on the front panel, until the LED opposite $\phi$, CW is illuminated.

## Phase Detector Method (cont'd)

11. Set the LOCK BANDWIDTH FACTOR to 100.
12. Select the BAND RANGE that includes the frequency of the signal under test. For example, if the frequency of the signal under test is 10 GHz then the BAND RANGE would be $8.32-10.88 \mathrm{GHz}$. Select this filter.
13. Connect the IF OUTPUT, on the front panel, to a spectrum analyzer.

## NOTE

Present at the IF OUTPUT will be the IF signal (signal under test minus the BAND CENTER frequency of the BAND RANGE chosen), IF harmonics and spurious signals. The signal with the highest amplitude is the desired signal.
Adjust the spectrum analyzer to determine the frequency of the IF OUTPUT (signal under test minus the BAND CENTER frequency of the BAND RANGE chosen). Set the tunable $5-1280 \mathrm{MHz}$ source to the frequency read on the spectrum analyzer. Disconnect the IF OUTPUT from the spectrum analyzer.

NOTE
The following applys to those users with an IF signal of 625 MHz to 655 MHz .

IF signals between 625 MHz to 655 MHz cause a high level spur from one or both of the NOISE SPECTRUM OUTPUTS. When setting the reference level on the spectrum analyzer, during calibration, use the beat note and not the high level spur. The high level spur is a mixer product from the 640 MHz rear panel input and the $5-1280 \mathrm{MHz}$ front panel input. The spur is within the passband of the NOISE SPECTRUM OUTPUT, so it does not get filtered out.

For example: with a 635 MHz IF signal you can expect a 5 MHz high level spur from the $<10 \mathrm{MHz}$ OUTPUT.
14. Calibration. At calibration a reference level is being set on the spectrum analyzer. The Carrier Noise Test Set's effect on a given noise input is being used to set the reference level. Below is an example of how to set the reference level on the spectrum analyzer for making a phase noise measurement:
a. Increase the tunable $5-1280 \mathrm{MHz}$ source by 50 kHz . This will produce a 50 kHz beat note at the NOISE SPECTRUM OUTPUTS. This 50 kHz offset is given as an example only. A different offset may be required because of the frequency range of the spectrum analyzer or to make it easier to calibrate with a fast drifting source.
b. Add 40 dB of attenuation to the tunable $5-1280 \mathrm{MHz}$ signal.


Do not set the attenuation any higher than -30 dBm . -30 dBm or lower is necessary for a linear calibration.
c. Adjust the spectrum analyzer so the 50 kHz beat note is on the screen and placed at a convenient reference point. Record the level of the reference point for use later.
d. This reference point represents the power in the carrier minus 40 dB .
e. Remove the 50 kHz offset and 40 dB of attenuation from the tunable $5-1280 \mathrm{MHz}$ signal.
f. The spectrum analyzer is now ready to be used for making a measurement.
15. Phase Locking. The following discussion describes two methods for phase locking the device under test and the tunable 5-1280 MHz source.

When the device under test is a synthesized or very stable source, phase locking can be accomplished using either the FREQ-CONT X-OSC or FREQ-CONT DC-FM connector and the following procedure. The FREQ-CONT X-OSC or FREQ-CONT DC-FM connector is connected to the electronic frequency control input of the tunable $5-1280 \mathrm{MHz}$ source or the device under test.

The connector chosen will depend on the tuning voltage required by the loop VCO (device under test or the $5-1280 \mathrm{MHz}$ source).

## a. Set the LOCK BANDWIDTH FACTOR

 to 100 .b. On the front panel press then release CAPTURE.

## Phase Detector Method (cont'd)

c. If phase lock is acquired, a green LED will be illuminated in the center of the phase lock indicator, on the left side of the front panel.
d. If the two sources did not phase lock proceed as follows. Connect the $<10 \mathrm{MHz}$ OUTPUT, on the front panel, to a spectrum analyzer with a 50 Ohm input impedance and a bandwidth that includes 10 Hz to 10 MHz . Adjust the spectrum analyzer to view the beat note. The beat note is the difference between the tunable $5-1280 \mathrm{MHz}$ signal and the microwave test signal minus the BAND CENTER frequency of the BAND RANGE chosen.

Hold CAPTURE in while tuning the tunable $5-1280 \mathrm{MHz}$ source until a green LED is seen in the center of the phase lock indicator. The frequency resolution of the tunable 5-1280 MHz source should be $<1 / 10$ of the effective tuning range of it's crystal oscillator.

Figure 3-5 shows what the spectrum analyzer display should look like if the tunable 5-1280 MHz source is being tuned in the direction of phase lock (that is, towards dc) or tuned away from phase lock. Figure $3-6$ shows what the phase lock indicator, on the front panel, should be like as the two sources get closer to phase lock. Release CAPTURE and the two sources should now be phase locked.
e. If the device under test and the tunable $5-1280 \mathrm{MHz}$ source are still not phase locked increase the LOCK BANDWIDTH FACTOR to 1 k . Press and release CAPTURE. The two sources should now be phase locked. If phase lock was aquired go to step $g$. If phase lock was not aquired go to step $f$.

## NOTE

If the HP 8662A is used as the tunable $5-1280 \mathrm{MHz}$ source, and the system is locked using the crystal of the HP 8662A, the $1 k$ LOCK BANDWIDTH FACTOR may cause an unstable phase lock loop for microwave test signals greater than 5 GHz . If the loop is unstable lower the LOCK BANDWIDTH FACTOR to 100. If the loop is still unstable try locking using DC-FM.
f. If the two sources are still not phase locked try locking using a loop VCO with a
larger electronic tuning range.
g. Reduce the LOCK BANDWIDTH FACTOR if close-in measurements are desired. Make sure the phase lock indicator remains green or stays within the wide section of the indicator. If lock is broken, hold CAPTURE in while tuning the tunable $5-1280 \mathrm{MHz}$ source until the center green LED is illuminated on the phase lock indicator. When the green LED is illuminated release CAPTURE. If the green LED doesn't stay illuminated increase the LOCK BANDWIDTH FACTOR and press CAPTURE to re-enable lock. For accurate measurements reduce the loop bandwidth to below the lowest offset frequency of interest. Use the following equation to find the maximum loop bandwidth for the offset frequency of interest.

NOTE
Phase noise is suppressed within the phase lock loop bandwidth.

$$
\begin{align*}
& \text { Nominal }  \tag{Hz}\\
& \text { loop bandwidth }=\frac{f_{\text {dut }} \times \operatorname{LBF} \times \mathrm{K}_{0}}{100}(\mathrm{~Hz}) \\
& \mathrm{f}=\text { frequency }(\mathrm{Hz}) \\
& \text { dut }=\text { device under test } \\
& \text { LBF }=\text { LOCK BANDWIDTH FACTOR } \\
& \mathrm{K}_{\mathrm{o}}=\text { The VCO slope in Hz } / \text { volt (For the HP } \\
& \text { 8662A } \mathrm{K}_{0} \text { equals } 10^{\epsilon^{1}} \mathrm{~Hz} / \text { volt) }
\end{align*}
$$

When the device under test is a free-running source and the loop VCO has a DC-FM feature use the following procedure.
h. Connect the FREQ-CONT X-OSC or FREQ-CONT DC-FM connector to the electronic frequency control input of the loop VCO. The connector used will depend on the tuning voltage required for DC-FM.

Set the loop VCO as follows:

- DC-FM
-50 kHz deviation
- Set amplitude to 0 dBm
i. Set the LOCK BANDWIDTH FACTOR to 100 .
j. Connect the $<10 \mathrm{MHz}$ OUTPUT, on the front panel, to a spectrum analyzer with a 50 Ohm input impedance and a bandwidth that


The 5 to 1280 MHz source and device under test are 5 MHz from phase lock (quadrature).


The 5 to 1280 MHz source and device under test are 1.25 MHz from phase lock (quadrature).


The 5 to 1280 MHz source and device under test are 2.5 MHz from phase lock (quadrature).


The 5 to 1280 MHz source and device undee test are close to phase lock (quadrature).

Figure 3-5. Spectrum Analyzer Displays Used for Acquiring Phase Lock (Quadrature)

## Phase Detector Method (cont'd)

includes 10 Hz to 10 MHz . Adjust the spectrum analyzer to view the beat note. The beat note is the difference between the tunable 5-1280 MHz signal and the microwave test signal minus the BAND CENTER frequency of the BAND RANGE chosen.

Hold CAPTURE in while tuning the loop VCO until a green LED is seen in the center of the phase lock indicator. The frequency resolution of the loop VCO should be $<1 / 10$ of the effective tuning range of it's crystal oscillator.

Figure $3-5$ shows what the spectrum analyzer display should look like if the loop VCO is being tuned in the direction of phase lock (that is, towards dc) or tuned away from phase lock. Figure 3-6 shows what the phase lock indicator, on the front panel, should be like as the two sources get closer to phase lock. Release CAPTURE and the two sources should now be phase locked.

If the sources drift out of phase lock repeat the procedure, then after releasing CAPTURE immediately increase the FM deviation to 100 kHz . Again be sure the two sources stay phase locked.
k. If the two sources are still not phase locked repeat the preceeding step, each time increasing the FM deviation until maximum deviation is reached. If maximum deviation is reached and the two sources still will not stay locked, repeat step $j$ but this time increase the LOCK BANDWIDTH FACTOR until the two sources are phase locked. When the two sources are phase locked go to step m .

1. If the two sources are still not locked try making the measurement using the Frequency Discriminator Method.
m. Reduce the LOCK BANDWIDTH FACTOR if close-in measurements are desired. Make sure the phase lock indicator remains green or stays within the wide section of the indicator.


A solid red bar, to the left of the center green bar, indicates the signal under test and the tunable 5-1280 MHz signal are not phase locked and $>100 \mathrm{kHz}$ apart.


The red LEDs, within the display, step one at a time as the signal under test and the tunable 51280 MHz signal approach quadrature.


With the display all illuminated the signal under test and the tunable 51280 MHz signal are $<100$ kHz apart.


A green LED in the center of the display indicates that the signal under test and the tunable 5-1280 MHz signal are in quadrature.

Figure 3-6. Front Panel Phase Lock (Quadrature) Indicator

## Phase Detector Method (cont'd)

If lock is broken, hold CAPTURE in while tuning the tunable $5-1280 \mathrm{MHz}$ source until the center green LED is illuminated on the phase lock indicator. When the green LED is illuminated release CAPTURE. If the green LED doesn't stay illuminated increase the LOCK BANDWIDTH FACTOR and press CAPTURE to re-enable lock. For accurate measurements reduce the loop bandwidth to below the lowest offset frequency of interest. Use the following equation to find the maximum loop bandwidth for the offset frequency of interest.

## NOTE

Phase noise is suppressed within the phase lock loop bandwidth.

$$
\begin{aligned}
& \text { Nominal } \\
& \text { loop bandwidth }=\frac{f_{\text {dut }} \times \operatorname{LBF} \times \mathrm{K}_{\mathrm{o}}}{100} \\
& \mathrm{f}= \text { Frequency (Hz) } \\
& \text { dut }= \text { Device under test } \\
& \mathrm{LBF}= \text { Lock Bandwidth Factor } \\
& \mathrm{K}_{\mathrm{o}}= \text { The VCO slope in Hz } / \mathrm{volt} \text { (For the } \\
&\left.\mathrm{HP} 8662 \mathrm{~A} \mathrm{~K}_{\mathrm{o}} \text { equals } 10^{-1} \mathrm{~Hz} / \mathrm{volt}\right)
\end{aligned}
$$

16. Measurement. With the spectrum analyzer calibrated and phase lock acquired, a phase noise measurement may now be made. When making a phase noise measurement the following items must be taken into consideration:
-Set the spectrum analyzer span to cover the offset frequency of interest.

- Do not change the input sensitivity of the spectrum analyzer. Changing the spectrum analyzer input sensitivity between calibration and measurement decreases the measurement accuracy. For better accuracy recalibrate on a lower level calibration signal. See step 14 of this procedure.
-Select an appropriate resolution bandwidth for the the chosen frequency span (at least $<1 / 10$ frequency span).
- Because phase noise is a random quantity, some sort of averaging or video filtering is desired.
- In general, it is not advisable to take measurements on a portion of the spectrum analyzer display where the noise level is falling
very rapidly ( $>20 \mathrm{~dB}$ per major division). Therefore, increase the frequency span to where the offset frequency of interest is in the center of the spectrum analyzer display.
- It is not recommended to measure noise levels that are in the bottom 10 dB of the display.
- In general, if spurious signals are seen when making a measurement they can be disregarded. Reduce the resolution bandwidth if necessary to determine the noise level near the spur. Be careful not to measure on a spur.
- With the preceeding considerations in mind, a measurement can now be made. Measure down from the reference point (step 14 c .) at the offset of interest.

17. Corrections ${ }^{1}$. Subtract the reference level set during calibration from the level of the noise measured at the offset of interest. Sum this value and the following correction factors.

- Minus 40 dB for the attenuation added during calibration.
- Minus 6 dB for conversion to $£(\mathrm{f})$.
- Minus $10 \log (1.2 \times$ spectrum analyzer resolution bandwidth). This is for normalization to a 1 Hz noise equivalent bandwidth. The result is in dB .
-Plus 2.5 dB is the correction for $\log$ amplifiers and peak detectors used in an analog spectrum analyzer.
- Plus loop noise suppression ${ }^{2}$ at the appropriate offset frequency. Only add loop noise suppression when making a measurement inside the loop bandwidth.
Below is an example of how to calculate the correct amount of phase noise:
$-67 \mathrm{dBm}=$ measured phase noise.
$-10 \mathrm{dBm}=$ reference level set during calibration.
$-40 \mathrm{~dB}=\begin{gathered}\text { attenuation added during } \\ \text { calibration }\end{gathered}$ calibration.

[^0]
## Phase Detector Method (cont'd)

$-6 \mathrm{~dB}=\mathcal{L}(\mathrm{f})$ conversion factor
$-20.8 \mathrm{~dB}=10 \log$ ( 1.2 x spectrum analyzer resolution bandwidth).
$+2.5 \mathrm{~dB}=$ if an analog spectrum analyzer is used.
$+20 \mathrm{~dB}=$ for loop noise suppression if the measurement is made within the loop bandwidth.

$$
\begin{aligned}
& -67 \mathrm{dBm}-(-10 \mathrm{dBm})+(-40 \mathrm{~dB}) \\
& +(-6 \mathrm{~dB})+(-20.8 \mathrm{~dB})+(2.5 \mathrm{~dB}) \\
& +(20 \mathrm{~dB})=-101.3 \mathrm{dBc} / \mathrm{Hz}
\end{aligned}
$$

The actual amount of phase would then be $-101.3 \mathrm{dBc} / \mathrm{Hz}$.

After applying these correction factors the actual amount of phase noise is known for the particular frequency offset.

## 3-11. Frequency Discriminator Method

1. Figure $3-7$ shows interconnections to the Carrier Noise Test Set when making a phase noise measurement.
2. Be sure the LINE MODULE on the rear panel is set to the available line voltage. If it needs to be changed see Figure 2-1 in Section II.
3. Plug the Carrier Noise Test Set into the available line supply.
4. Turn the Carrier Noise Test Set on and allow a 30 minute warm-up before making any measurements.
5. If the microwave test signal is from 0.010 1.28 GHz go to step 6. If the microwave test signal is greater than 1.28 GHz follow the instructions for step 5.
Using a coaxial cable connect a 640 MHz source to the 640 MHz IN connector on the rear panel.
To configure and use the internal 640 MHz oscillator connect the 640 MHz OUT connector to the 640 MHz IN connector with the cable-attenuator assembly (HP 11729-60096 or HP 11729-60098 [Option 140]) provided. Both connectors are on the rear panel. Be sure to make the connection using the cable-attenuator assembly that was shipped with the Carrier Noise Test Set.

## NOTE

The absolute system noise floor will be degraded close-in to the carrier when using the internally generated 640 MHz signal compared to the 640 MHz sig-


Figure 3-7. Interconnections to the Carrier Noise Test Set When Making a Phase Noise Measurement (Using the Frequency Discriminator Method)

## Frequency Discriminator Method (cont'd)

 nal being supplied by the HP 8662A Synthesized Signal Generator.6. Using a coaxial cable connect the device under test to the MICROWAVE TEST SIGNAL INPUT connector on the front panel.
7. Connect the IF OUTPUT, on the front panel, to a spectrum analyzer.
8. To select a PHASE NOISE MEASUREMENT press the MODE button, on the front panel, until the LED opposite $\phi, \mathrm{CW}$ is illuminated.
9. Select the BAND RANGE that includes the frequency of the signal under test. For example, if the frequency of the signal under test is 10 GHz then the BAND RANGE would be $8.32-10.88 \mathrm{GHz}$. Select this filter.
10. The LOCK BANDWIDTH FACTOR can be at any setting.
11. Using a spectrum analyzer determine the frequency at the IF OUTPUT (signal under test minus the BAND CENTER frequency of the BAND RANGE chosen).

## NOTE

A number of signals will be present at the IF OUTPUT. The signals present will include the IF signal (signal under test minus the BAND CENTER frequency of the BAND RANGE chosen), IF harmonics and spurious signals. The signal with the highest amplitude is the desired signal.

Note the frequency for use later. Disconnect the IF OUTPUT from the spectrum analyzer.
12. Connect a suitable delay line (such as a length of flexible RF cable) between the IF OUTPUT and the $5-1280 \mathrm{MHz}$ INPUT, on the front panel. The length of delay line effects the sensitivity of the descriminator. In general, sensitivity increases with cable length. $1.5 \mathrm{~ns} /$ foot is the approximate amount of delay for flexible RF cable when the cable dielectric is Teflon.
13. Set the tunable $5-1280 \mathrm{MHz}$ source to the following conditions:
Frequency: Same as measured in step 11.
Amplitude: -10 dBm
Modulation: FM 1 kHz rate
14. Connect the tunable $5-1280 \mathrm{MHz}$ signal to the input of the spectrum analyzer.
15. Set the FM sidebands on the tunable 5-1280 MHz signal to a convenient carrier to sideband ratio. The ratio should be at least 20 dB at a 0.2 kHz rate. Note the difference between the carrier and sidebands for use later.
16. Disconnect the device under test from the Carrier Noise Test Set and the tunable 5-1280 MHz source from the spectrum analyzer. Connect the tunable 5 to 1280 MHz source to the MICROWAVE TEST SIGNAL INPUT connector on the Carrier Noise Test Set. Enable the $0.010-1.28 \mathrm{GHz}$ BAND RANGE.
17. Connect the $<10 \mathrm{MHz}$ OUTPUT, on the Carrier Noise Test Set front panel, to the spectrum analyzer.

## NOTE

Do not use the $<10 \mathrm{MHz}$ NOISE SPECTRUM OUTPUT for test signals $\pm 20$ MHz around the BAND CENTER frequency. High feedthrough signals (mixer sum products and LO signals) saturate the Low Noise Amplifier in the Carrier Noise Test Set and possibly the spectrum analyzer.
Do not use the $<1 \mathrm{MHz}$ NOISE SPECTRUM OUTPUT for test signals $\pm 5$ MHz around the BAND CENTER frequency. LO feedthrough may possibly saturate the spectrum analyzer.
For test signals $\pm 5 \mathrm{MHz}$ to 10 MHz around the BAND CENTER frequency the measured noise level will be 0 dBm to ${ }^{+3} \mathrm{dBm}$ greater than the actual level. The error is caused by an impedance change on the input of the internal Low Noise Amplifier.
For test signals $\pm 10 \mathrm{MHz}$ to 20 MHz around the BAND CENTER frequency the measured noise level will be 0 dBm to +1 dBm greater than the actual level. Again the error is caused by an impedance change on the input of the Low Noise Amplifier.
Therefore, the $<1 \mathrm{MHz}$ OUTPUT can be used for test signals $\pm 5 \mathrm{MHz}$ to 20 MHz around the BAND CENTER frequency by subtracting the maximum error amount from the measured level.

## Frequency Discriminator Method (cont'd)

18. Increase or decrease the frequency of the tunable $5-1280 \mathrm{MHz}$ source until a green LED is seen in the center of the phase lock indicator on the Carrier Noise Test Set. The frequency resolution of the tunable 5-1280 MHz source should be $<1 / 10$ of $1 / \tau_{\mathrm{d}}$. $\tau_{\mathrm{d}}$ is the time delay caused by the cable connected from the IF OUTPUT to the $5-1280 \mathrm{MHz}$ IN. Once quadrature is established adjust the spectrum analyzer to position the 1 kHz FM sideband at the top line on the spectrum analyzer. Note the level of the 1 kHz sideband for use later.
19. Disconnect the tunable $5-1280 \mathrm{MHz}$ source from the Carrier Noise Test Set. Connect the device under test to the MICROWAVE TEST SIGNAL INPUT connector on the Carrier Noise TestSet. Select the proper BAND RANGE for the frequency of the signal under test.
20. Increase or decrease the length of the delay line or the frequency of the device under test to establish quadrature. The frequency resolution of the device under test should be $<1 / 10$ of $1 / \tau_{\mathrm{d}}$. When quadrature is set a green LED will be illuminated in the center of the phase lock indicator on the Carrier Noise Test Set.
21. Measurement. With calibration completed a measurement can now be made. When making a phase noise measurement the following items must be taken into consideration:

- The operator should be aware that voltage fluctuations caused by frequency fluctuations are being measured. Phase fluctuations are not being measured.
-Set the spectrum analyzer span to cover the offset frequency of interest.
- Do not change the input sensitivity of the spectrum analyzer. Changing the spectrum analyzer input sensitivity between calibration and measurement decreases the measurement accuracy. For better accuracy recalibrate on a lower level calibration signal. See steps 14-18 to recalibrate.
-Select a resolution bandwidth that is appropriate for the chosen frequency span (at least $<1 / 10$ frequency span).
- Because phase noise is a random quantity, some sort of averaging or video filtering is desired.
- In general, it is not advisable to take measurements on a portion of the spectrum analyzer display where the noise level is falling very rapidly ( $>20 \mathrm{~dB}$ per major division). Therefore, increase the frequency span to where the offset frequency of interest is in the center of the spectrum analyzer display.
- It is not recommended to measure noise levels that are in the bottom 10 dB of the display.
- In general, if spurious signals are seen when making a measurement they can be disregarded. If necessary, reduce the resolution bandwidth to determine the noise level close to the spur.
- With the preceding considerations in mind, a measurement can now be made. Measure down from the reference point (step 18) at the offset of interest.

22. Corrections ${ }^{1}$. Subtract the reference level set in step 18 from the measured level. Sum this result with the following correction factors:

- Minus the carrier to sideband ratio set in step 15.
- Minus $20 \log \left(\mathrm{f}_{\text {off }} / 1 \mathrm{kHz}\right) \mathrm{dB}$. This formula will convert frequency fluctuations at any offset to $\mathcal{L}(\mathrm{f}) \mathrm{dBc} . \quad \mathcal{L}(\mathrm{f}) \mathrm{dBc}=10 \log \mathrm{Pssb} / \mathrm{Ps}$ where Pssb is the power density (in one phase modulation sideband) and Ps is the total signal power.
- Minus $10 \log$ ( 1.2 x spectrum analyzer reslution bandwidth). This is for normalization to a 1 Hz noise equivalent bandwidth. The result is in dB .
- Plus 2.5 dB is the correction for $\log$ amplifiers and peak detectors used in an analog spectrum analyzer.
Below is an example of how to calculate the correct amount of phase noise:
$-67 \mathrm{dBm}=$ measured phase noise.
$-10 \mathrm{dBm}=$ reference level set during calibration.
$-20 \mathrm{~dB}=$ carrier to sideband ratio set in step 15.
$-10 \mathrm{~dB}=20 \log \left(\mathrm{f}_{\text {off }} / 1 \mathrm{kHz}\right) \mathrm{db}$. This formula is used to convert frequency fluctuations at any offset to $\mathcal{L}(\mathrm{f}) \mathrm{dBc}$.

[^1]

Figure 3-8. Interconnections to the Carrier Noise Test Set When Making an AM Noise Measurement

## Frequency Discriminator Method (cont'd)

$-20.8 \mathrm{~dB}=10 \log (1.2 \times$ spectrum analyzer resolution bandwidth).
$+2.5 \mathrm{~dB}=$ if an analog spectrum analyzer is used.
$-67 \mathrm{dBm}-(-10 \mathrm{dBm})+(-20 \mathrm{~dB})+(-10 \mathrm{~dB})$ $+(-20.8 \mathrm{~dB})+(2.5 \mathrm{~dB})=-105.3 \mathrm{dBc} / \mathrm{Hz}$
The actual amount of phase would then be $-105.3 \mathrm{dBc} / \mathrm{Hz}$.

After applying these correction factors the actual amount of phase noise will be known at a particular offset, provided the sensitivity, set-up with the delay line, is lower than the phase noise of the device under test.

## 3-12. AM Measurement (Option 130 only)

1. Figure $3-8$ shows interconnections to the Carrier Noise Test Set when making an AM noise measurement.
2. Be sure the LINE MODULE on the rear panel is set to the available line voltage. If it needs to be changed see Figure 2-1 in Section II.
3. Plug the Carrier Noise Test Set into the available line supply.
4. Turn the Carrier Noise Test Set on and allow a 30 minute warm-up before making any measurements.
5. Set the device under test to the frequency of interest. Measure the power out of the device
under test with a power meter. Note the power level for use later.
6. Set the RF source to 1 GHz .
7. Set the power of the RF source to the same power as that measured in step 5 . Use a power meter to measure the power.
8. Connect the RF source to a spectrum analyzer. Set the displayed RF source to a convenient reference point on the spectrum analyzer.
9. Amplitude modulate the RF source at a 1 kHz rate. Adjust the AM level so the AM sidebands are -40 dBc .

## NOTE

If the RF source is a non-synthesized source the modulating rate may have to be increased. This is so the AM sidebands can be seen on the spectrum analyzer display.
10. Press the MODE button, on the front panel of the Carrier Noise Test Set, until the LED next to AM, CW is illuminated. No other Carrier Noise Test Set front panel functions are used.
11. Disconnect the RF source from the spectrum analyzer. Connect the RF source to the MICROWAVE TEST SIGNAL INPUT connector on the front panel of the Carrier Noise Test Set.
12. Connect the $<10 \mathrm{MHz}$ OUTPUT, on the front panel of the Carrier Noise Test Set, to the spectrum analyzer.

## AM Measurements (Option 130 only) (cont'd)

13. Set a reference point with the demodulated 1 kHz signal on the spectrum analyzer. Note the reference level for use later.
14. Disconnect the RF source from the Carrier Noise Test Set. Connect the device under test to the MICROWAVE TEST SIGNAL INPUT connector on the front panel of the Carrier Noise Test Set.
15. Measurement. With calibration completed a measurement can now be made. When making an AM measurement the following items must be taken into consideration:
-Set the spectrum analyzer span to cover the offset frequency of interest.

- Do not change the input sensitivity of the spectrum analyzer. Changing the spectrum analyzer input sensitivity between calibration and measurement decreases the measurement accuracy. For better accuracy recalibrate on a lower level calibration signal. Use steps 5-13 to recalibrate the spectrum analyzer.
-Select a resolution bandwidth that is appropriate for the chosen frequency span (at least $<1 / 10$ frequency span).
- Because AM noise is a random quantity, some sort of averaging or video filtering is desired.
- In general, it is not advisable to take measurements on a portion of the spectrum analyzer display where the noise level is falling very rapidly ( $>20 \mathrm{~dB}$ per major division). Therefore, increase the frequency span to where the offset frequency of interest is in the center of the spectrum analyzer display.
- It is not recommended to measure noise levels that are in the bottom 10 dB of the display.
- In general, if spurious signals are seen when making a measurement they can be disregarded. If necessary, reduce the resolution bandwidth to determine the noise level close to the spur.
- A measurement can now be made. Measure down from the reference point set in step 13 at the offset of interest.

16. Corrections ${ }^{1}$. Subtract the reference level in step 13 from the measured level. Sum this result with the following correction factors:

- Minus 40 dB (The carrier to sideband ratio set in step 9)
- Minus $10 \log$ ( $1.2 \times$ specturm analyzer resolution bandwidth). This is for normalization to a 1 Hz noise equivalent bandwidth. The result is in dB .
- Plus 2.5 dB is the correction for $\log$ amplifiers and peak detectors used in an analog spectrum analyzer.
Below is an example of how to calculate the correct amount of AM noise:
$-67 \mathrm{dBm}=$ measured AM noise.
$-10 \mathrm{dBm}=$ reference level set during calibration.
$-40 \mathrm{~dB}=$ The carrier to sideband ratio set in step 9.
$-20.8 \mathrm{~dB}=10 \log$ ( $1.2 \times$ spectrum analyzer resolution bandwidth).
$+2.5 \mathrm{~dB}=$ if an analog spectrum analyzer is used.
$-67 \mathrm{dBm}-(-10 \mathrm{dBm})+(-40 \mathrm{~dB})$
$+(-20.8 \mathrm{~dB})+(2.5 \mathrm{~dB})=-115.3 \mathrm{dBc} / \mathrm{Hz}$
The actual amount of AM noise would then be $-115.3 \mathrm{dBc} / \mathrm{Hz}$.

[^2]Table 3-3. HP-IB Message Reference Table (1 of 2)

| $\begin{aligned} & \text { HP-IB } \\ & \text { Message } \end{aligned}$ | Applicable | Response | Related Commands \& Controls | Interface Functions |
| :---: | :---: | :---: | :---: | :---: |
| Data | Yes | All Carrier Noise Test Set functions available in local, except the LINE switch, are bus-programmable. |  | $\begin{gathered} \mathrm{AH} 1, \mathrm{SH} 1, \\ \mathrm{~T} 5, \mathrm{TE} 0 \\ \mathrm{~L} 3, \mathrm{LE} 0 \end{gathered}$ |
| Trigger | No | The Carrier Noise Test Set has no trigger capability. |  | DT0 |
| Clear | Yes | The clear message sets the Carrier Noise Test Set to the following conditions: <br> Filter 1 ON <br> Phase Lock Bandwidth <br> 100 Hz <br> Phase noise measurement <br> Capture OFF | $\begin{aligned} & \text { DCL, } \\ & \text { SDC } \end{aligned}$ | DC1 |
| Remote | Yes | Remote mode is enabled when the REN bus control line is true. However, remote mode is not entered until the first time the Carrier Noise Test Set is addressed to listen. The front-panel REMOTE annunciator lights when the instrument is actually in the remote mode. No instrument settings or functions are changed, but all front-panel keys except LOCAL are disabled. | REN | RL1 |
| Local | Yes | The Carrier Noise Test Set returns to local mode (front-panel control). Responds equally to the GTL bus command and the frontpanel LOCAL key. When entering local mode, no instrument settings or functions are changed. | GTL | RL1 |
| Local <br> Lockout | Yes | Disables all front-panel keys including LOCAL. Only the controller can return the Carrier Noise Test Set to local (front-panel control). | LLO | RL1 |
| Clear <br> Lockout <br> Set <br> Local | Yes | The Carrier Noise Test Set returns to local (front-panel control) and local lockout is cleared when the REN bus control line goes false. When entering local mode, no instrument settings or functions are changed. | REN | RL1 |
| Pass <br> Control Take Control | No | The Carrier Noise Test Set has no controller capability. |  | C0 |
| Require <br> Service (SRQ) | Yes | If the SRQ mask is set (see Table 3-4 HP-IB Program Codes for a description of @) and one of the following conditions is valid, then SRQ will be true. <br> 1) Invalid command <br> 2) System in phase lock <br> 3) System out of phase lock | SRQ | SR1 |

Table 3-3. HP-IB Message Reference Table (2 of 2)

| HP-IB Message | Applicable | Response | Related Commands \& Controls | Interiace <br> Functions |
| :---: | :---: | :---: | :---: | :---: |
| Status Byte | Yes | The Carrier Noise Test Set responds to a Serial Poll Enable (SPE) bus command by sending an 8 -bit byte when addressed to talk. If the instrument is holding the SRQ control line true (issuing the Require Service message) bit 7 (RQS bit) in the Status Byte and the bit representing the condition causing the Require Service message to be issued will both be true. The bits in the Status Byte are latched but can be cleared by: <br> 1) Removing the causing condition, and <br> 2) reading the Status Byte. | SPE, | T5, TE0 |
| Status <br> Bit | Yes | The status bit is used in a parallel poll, when enabled, and the SRQ line is true. The status bit position and the sense of the status bit (true high or true low) is set by the computer, with the parallel poll configure message. | PPE, <br> PPD, <br> PPC, <br> PPU | PP1 |
| Abort | Yes | The Carrier Noise Test Set stops talking and listening. | IFC | T5, TE0, <br> L3, LE0 |

Complete HP-IB compatibility as defined in IEEE Standard 488 (and the identical ANSI Standard MC1.1) is: SH1, AH1, T5, TE0, L3, LE0, SR1, RL1, PP1, DC1, DT0, C0.

Table 3-4. HP-IB Program Codes (Alphabetical Order by Code)

| Program Code | Parameter |
| :---: | :---: |
| AM | AM noise measurement (Option 130 only) |
| @ | Causes the Carrier Noise Test Set to accept the next data byte as a binary mask for the status byte. For example: <br> SRQ Mask <br> When position $A$ is set to 1 and the corresponding bit in the status byte becomes 1 , then RQS in the status byte and the SRQ line will be 1 . Under the preceding condition a serial poll of the status byte will indicate that phase lock has been broken. <br> When position $B$ is set to 1 and the corresponding bit in the status byte becomes 1 , then RQS in the status byte and the SRQ line will be 1 . Under the preceding condition a serial poll of the status byte will indicate phase lock. <br> When position C is set to 1 and the corresponding bit in the status byte becomes 1 , then RQS in the status byte and the SRQ line will be 1 . Under the preceding condition a serial poll of the status byte will indicate an invalid command has been received. |
| CA | CA1 = Capture active CA0 $=$ Capture inactive |
| CS | Forces RQS and invalid command bit to zero in the status byte. |
| FT | $\begin{aligned} & \text { Filter Bands } \\ & \begin{aligned} 1 & =\text { FT1 } \quad 7=\text { FT7 } \\ 2 & =\text { FT2 } \quad 8=\text { FT8 } \\ 3 & =\text { FT3 } \quad 9=\text { FT9 } \\ 4 & =\text { FT4 } 10=\text { FT10 } \\ 5 & =\text { FT5 } 11=\text { FT11 } \\ 6 & =\text { FT6 } \end{aligned} \end{aligned}$ |
| LK | Phase Lock Range $\begin{aligned} 1 \mathrm{~Hz}(1) & =\text { LK } 1 \\ 10 \mathrm{~Hz}(2) & =\text { LK } 2 \\ 100 \mathrm{~Hz}(3) & =\text { LK } \\ 1 \mathrm{kHz}(4) & =\text { LK } 4 \\ 10 \mathrm{kHz}(5) & =\text { LK } \end{aligned}$ |
| LP | When addressed to talk the Carrier Noise Test Set will send the current front panel settings in ASCII mnemonic string. |
| PH | Phase noise measurement |
| PU | Pulse measurement |
| ?ID | When addressed to talk the Carrier Noise Test Set will send an ASCII string which contains the model number of the instrument and software revision number. |
| RM | When addressed to talk the Carrier Noise Test Set will send a single byte which is the binary pattern of the SRQ. |
| RO | When addressed to talk the Carrier Noise Test Set will send the ASCII mnemonics of the options installed. |

Table 3-5. Allowable HP-IB Address Codes

| Address Switches ${ }^{1}$ |  |  |  |  | Listen Address Character | Talk Address Character | Decimal EquivaIent ${ }^{1}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A5 | A4 | A3 | A2 | A1 |  |  |  |
| 0 | 0 | 0 | 0 | 0 | SP | @ | 0 |
| 0 | 0 | 0 | 0 | 1 | ! | A | 1 |
| 0 | 0 | 0 | 1 | 0 | " | B | 2 |
| 0 | 0 | 0 | 1 | 1 | \# | C | 3 |
| 0 | 0 | 1 | 0 | 0 | \$ | D | 4 |
| 0 | 0 | 1 | 0 | 1 | \% | E | 5 |
| 0 | 0 | 1 | 1 | 0 | \& | F | 6 |
| 0 | 0 | 1 | 1 | 1 | - | G | 7 |
| 0 | 1 | 0 | 0 | 0 | $($ | H | 8 |
| 0 | 1 | 0 | 0 | 1 | ) | 1 | 9 |
| 0 | 1 | 0 | 1 | 0 | * | J | 10 |
| 0 | 1 | 0 | 1 | 1 | + | K | 11 |
| 0 | 1 | 1 | 0 | 0 | , | L | 12 |
| 0 | 1 | 1 | 0 | 1 | - | M | 13 |
| 0 | 1 | 1 | 1 | 0 | - | N | 14 |
| 0 | 1 | 1 | 1 | 1 | 1 | 0 | 15 |
| 1 | 0 | 0 | 0 | 0 | 0 | P | 16 |
| 1 | 0 | 0 | 0 | 1 | 1 | Q | 17 |
| 1 | 0 | 0 | 1 | 0 | 2 | R | 18 |
| 1 | 0 | 0 | 1 | 1 | 3 | S | 19 |
| 1 | 0 | 1 | 0 | 0 | 4 | T | 20 |
| 1 | 0 | 1 | 0 | 1 | 5 | U | 21 |
| 1 | 0 | 1 | 1 | 0 | 6 | V | 22 |
| 1 | 0 | 1 | 1 | 1 | 7 | W | 23 |
| 1 | 1 | 0 | 0 | 0 | 8 | X | 24 |
| 1 | 1 | 0 | 0 | 1 | 9 | Y | 25 |
| 1 | 1 | 0 | 1 | 0 | : | Z | 26 |
| 1 | 1 | 0 | 1 | 1 | ; | [ | 27 |
| 1 | 1 | 1 | 0 | 0 | < | 1 | 28 |
| 1 | 1 | 1 | 0 | 1 | = | ] | 29 |
| 1 | 1 | 1 | 1 | 0 | > |  | 30 |
| ${ }^{1}$ Decimal characters and the five address switches relate to the last five bits of both talk and listen addresses. <br> ${ }^{2}$ Factory-set address. |  |  |  |  |  |  |  |

## SECTION IV PERFORMANCE TESTS

## 4-1. INTRODUCTION

The procedures in this section test the instrument's electrical performance using the specifications of Table 1-1 as the performance standards. All tests can be performed without access to the interior of the instrument. A simpler operational test is included in Section III under Basic Functional Checks.

NOTE
A 30 minute warm-up period is required before any tests are performed.
Line voltage must be within $+5 \%$ and $-10 \%$ of nominal if the performance tests are to be considered valid.

## 4-2. EQUIPMENT REQUIRED

Equipment required for the performance tests is listed in Table 1-4, Recommended Test Equipment
in Section I. Any equipment that satisfies the critical specifications given in the table may be substituted for the recommended model(s).

## 4-3. TEST RECORD

Results of the performance tests may be tabulated on the Test Record at the end of the procedures. The Test Record lists all of the tested specifications and their acceptable limits. The results, recorded at incoming inspection, can be used for comparison in periodic maintenance and troubleshooting and after repairs or adjustments.

## 4-4. CALIBRATION CYCLE

This instrument requires periodic verification of performance. Depending on the use and environmental conditions, the instrument should be checked using the following performance tests at least once every year.

PERFORMANCE TESTS

## 4-5. MEASUREMENT FREQUENCY RANGE, IF OUTPUT BANDWIDTH AND LEVEL PEFORMANCE TESTS

## Specifications

| Electrical Characteristics | Performance Limits | Conditions |
| :---: | :---: | :---: |
| TEST SIGNAL <br> Frequency Range ${ }^{1}$ | 10 MHz to 18 GHz | External low-pass filtering may be required for test signals $<20 \mathrm{MHz}$ and $\pm 20 \mathrm{MHz}$ around band centers. |
| Band Center Frequencies | $\begin{aligned} & 1.92 \mathrm{GHz} \\ & 4.48 \mathrm{GHz} \\ & 7.04 \mathrm{GHz} \\ & 9.60 \mathrm{GHz} \\ & 12.16 \mathrm{GHz} \\ & 14.72 \mathrm{GHz} \\ & 17.48 \mathrm{GHz} \end{aligned}$ |  |
| IF OUTPUT Bandwidth Level | 5 MHz to 1280 MHz <br> +7 dBm Minimum |  |
| ${ }^{1}$ Frequency range covered in eight bands, excluding $\pm 5 \mathrm{MHz}$ around band center frequencies. |  |  |

## PERFORMANCE TESTS

## MEASUREMENT FREQUENCY RANGE, IF OUTPUT BANDWIDTH AND LEVEL PERFORMANCE TEST (cont'd)

Description This test verifies the frequency range of the Carrier Noise Test Set. A microwave test signal is input to the Carrier Noise Test Set for each BAND RANGE; then the down converted IF OUTPUT is measured on a spectrum analyzer. The IF OUTPUT level is verified to be within specified limits for each band.

Equipment Microwave Synthesized Source ...... HP 8340A
RF Spectrum Analyzer ............... HP 8566B
RF Synthesized
Signal Generator ................... HP 8662A
RF SYNTHESIZED
SIGNAL GENERATOR


Figure 4-1. Measurement Frequency Range, and IF Output Bandwidth and Level Test Set-up

Procedure 1. Connect the test set up shown in Figure 4-1.
2. Set the Carrier Noise Test Set as follows:

Band Center Frequency 1.92 GHz

NOTE
If the unit does not contain a filter with this band center frequency, select the next available band listed in column 2 of Table 4-1.
3. Set the Microwave Synthesized Source (D.U.T.) as follows:

Frequency .......................... 2.32 GHz
Amplitude
$+10 \mathrm{dBm}$
NOTE
The frequency corresponds to the microwave test signal shown in Table 4-1 for the band center frequency selected in step 2.

## MEASUREMENT FREQUENCY RANGE, IF OUTPUT BANDWIDTH AND LEVEL PERFORMANCE TESTS (cont'd)

Procedure (cont'd)
4. Adjust the RF spectrum analyzer to display the 400 MHz IF OUTPUT.

NOTE
The IF OUTPUT will have the following signals:

- The IF signal (the microwave test signal minus the band center of the band range chosen.)
- IF harmonics
- And spurious signals

ALL HARMONICS OF THE IF SIGNAL AND ANY SPURIOUS SIGNALS CAN BE DISREGARDED.
5. Verify the IF OUTPUT level is within the specified limits in Table 4-1 and record the actual value.
6. Adjust the frequency of the D.U.T. to the next microwave test signal frequency listed in column one of Table 4-1. Select the corresponding band center frequency, on the Carrier Noise Test Set, listed in column two. Verify and record the IF OUTPUT power level. Repeat this process for each microwave test signal frequency listed in Table 4-1.
7. If the IF OUTPUT power level did not measure within specified limits, refer to the troubleshooting information on Service Sheet 1.

Table 4-1. IF Output Level

| Microwave Test Signal [GHz] | Band Center Frequency (GHz) | IF Output Frequency (MHz) | IF Output Level (dBm) |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Typical | Minimum | Actual |
| 2.32 | 1.92 | 400 | +7 |  |
| 4.88 | 4.48 | 400 | +7 |  |
| 7.44 | 7.04 | 400 | +7 |  |
| 10.00 | 9.60 | 400 | +7 |  |
| 12.56 | 12.16 | 400 | +7 |  |
| *14.740 | 14.72 | 20 | +7 |  |
| *16.00 | 14.72 | 1280 | +7 |  |
| *17.30 | 17.28 | 20 | +7 |  |
| *18.56 | 17.28 | 1280 | +7 |  |

[^3]
## PERFORMANCE TESTS

## 4-6. RESIDUAL PHASE NOISE PERFORMANCE TEST (Using a test signal less than $1280 \mathbf{M H z}$ )

Specification

| Electrical <br> Characteristics | Performance Limits | Conditions |
| :---: | :---: | :--- |
| Offset From | $\mathrm{dBc} / \mathrm{Hz}$ | With a $<1.28 \mathrm{GHz}$ input |
| Carrier | -115 | signal |
| 10 Hz | -126 |  |
| 100 Hz | -135 |  |
| 1 kHz | -142 |  |
| 10 kHz | -151 |  |
| 100 kHz | -156 |  |
| 1 MHz |  |  |

## Description

NOTE
This test does not check the down converting circuitry in the Carrier Noise Test Set. However, the test requires less equipment than the residual phase noise test using a 10 GHz test signal.

The Carrier Noise Test Set's residual phase noise,for test signals $<1280 \mathrm{MHz}$, is verified by connecting a signal generator's RF output to a power splitter. The output of the power splitter supplies the signals for both the MICROWAVE TEST SIGNAL INPUT and the $5-1280 \mathrm{MHz}$ INPUT. Since the microwave test signal and the 5-1280 MHz signal are identical, the phase noise from the signal generator is canceled by the mixer/phase detector in the Carrier Noise Test Set. During the residual phase noise measurement the microwave test signal and the $5-1280 \mathrm{MHz}$ signal must be in phase quadrature (that is, 90 degrees out of phase). The difference in the lengths of cables $A$ and B provide a time delay,so at a selected frequency on the signal generator the two inputs will have a 90 degree phase difference. The Carrier Noise Test Set's NOISE SPECTRUM OUTPUTS are measured on a low frequency spectrum analyzer and an RF spectrum analyzer. Correction factors are added and the residual phase noise is verified to be below the specified limit.


## PERFORMANCE TESTS

RESIDUAL PHASE NOISE PERFORMANCE TEST (Using a test signal less than $1280 \mathbf{~ M H z ) ~ ( c o n t ' d ) ~}$


Figure 4-2. Residual Phase Noise Test Setup (Using a test signal of less than 1280 MHz )

## Procedure Calibration

1. Connect the instruments as shown in Figure 4-2.
2. Turn on and warm up all instruments in the test setup for 30 minutes.
3. Set the RF synthesized signal generator (tunable reference) as follows:

Frequency .................................... 639.990 MHz
Amplitude ............................................ 0 dBm
4. Set the Carrier Noise Test Set as follows:

Band Range .............................. 0.01 to 1.28 GHz
Measurement Mode ................................... $\phi$, CW
Lock Bandwidth Factor .................... Any setting
5. Measure the power of the tunable reference signal at the end of cable $B$ and adjust the amplitude of the tunable reference until the power meter reads 0 dBm . Connect cable B to the $5-1280 \mathrm{MHz}$ INPUT on the Carrier Noise Test Set.

## PERFORMANCE TESTS

RESIDUAL PHASE NOISE PERFORMANCE TEST (Using a test signal less than $1280 \mathbf{~ M H z}$ ) (cont'd)

Procedure (cont'd)
6. Disconnect cable A from the MICROWAVE TESTSIGNAL INPUT on the Carrier Noise Test Set and terminate cable A with a 50 ohm load. Connect the 640 MHz signal, from the tunable reference rear panel, to the MICROWAVE TEST SIGNAL INPUT, on the front panel, of the Carrier Noise Test Set.
7. Decrease the amplitude of the tunable reference by 50 dB .
8. Adjust the RF spectrum analyzer to display the 10 kHz beat note. (The beat note is the result of mixing the 640 MHz and 639.990 MHz signals). Set the 10 kHz beat note to a convenient reference point.
9. Adjust the low frequency spectrum analyzer to view the 10 kHz beat note. If the spectrum analyzer has selectable filters, select a flat top filter. If RMS averaging is available, select approximately 128 averages. RMS averaging smooths out the noise floor. If RMS averaging is not available the measurement should be made at an average level on the noise floor, not a peak or valley.
10. Set the peak of the 10 kHz beat note to a convenient reference point.
11. Disconnect the 640 MHz signal from the MICROWAVE TEST SIGNAL INPUT on the Carrier Noise Test Set. Disconnect the 50 ohm load from cable A and connect cable A to the MICROWAVE TEST SIGNAL INPUT.

## Residual Phase Noise Measurement

12. Increase the amplitude of the tunable reference by 50 dB . Decrease the frequency of the tunable reference, in 1 MHz steps, until phase lock is acquired (green LED is illuminated on the phase lock display). The green LED should be illuminated when the tunable reference is around 425 MHz . For details on phase locking see Section III.
13. Adjust the RF spectrum analyzer to view the noise level at a 10 kHz offset. For the most accurate measurement use the smallest possible resolution bandwidth. Use some averaging to smooth out the noise level. Measure the noise level down from the reference point at 10 kHz . Measure an average noise level, do not measure on a peak or minimum noise level. Record this noise level (A) along with the spectrum analyzer's resolution bandwidth setting (B) below. Repeat the measurement and record for offsets of 100 kHz and 1 MHz .

| Offset from <br> carrier | Noise level (A) <br> (relative to reference level) (dB) | Resolution Bandwidth (B) <br> [Hz] |
| :---: | :---: | :---: |
| 10 kHz | - | - |
| 100 kHz <br> 1 MHz | - | - |

## PERFORMANCE TESTS

## RESIDUAL PHASE NOISE PERFORMANCE TEST (Using a test signal less than 1280 MHz ) (cont'd)

Procedure (cont'd)
14. On the low frequency spectrum analyzer, select a Hanning filter and the normalization to 1 Hz bandwidth (if the spectrum analyzer has these features available). If the spectrum analyzer does not have the normalization to a 1 Hz bandwidth this figure will have to be calculated later using the formula at the end of the test.

## NOTE

Power line spurs are not specified for the Carrier Noise Test Set. Power line spurs will appear at power line frequencies and multiples of power line frequencies. Do not make a noise measurement on a spur; make the measurement on an average noise level.
15. Adjust the low frequency spectrum analyzer to view the noise level at a 10 Hz offset. For the most accurate measurement use the smallest possible resolution bandwidth. Use some averaging if required. Measure the noise level down from the reference point at 10 Hz . Measure an average noise level, do not measure on a peak or minimum noise level. Record this noise level (C) in the table below. If the measurement was not made in a 1 Hz resolution bandwidth, also record the spectrum analyzer's resolution bandwidth setting (D) below. Repeat the measurement and record for offsets of 100 Hz and 1 kHz .

| Offiset from <br> carrier | Noise level (C) <br> (relative to reference level) (dB) | Resolution Bandwidth (D) <br> [Hz) |
| :---: | :---: | :---: |
| 10 Hz | - | - |
| 100 Hz | - | - |
| 1 kHz | - |  |

16. Calculate the Carrier Noise Test Set's residual phase noise at $10 \mathrm{kHz}, 100 \mathrm{kHz}$ and 1 MHz offsets from the carrier. Sum the measured noise level (A) and the 4 correction factors as shown below. The normalization bandwidth factor is determined by putting the resolution bandwidth (B) into the equation below. Verify the residual phase noise level did not exceed the specified limit, as shown at the bottom of each column.
[^4]
## PERFORMANCE TESTS

RESIDUAL PHASE NOISE PERFORMANCE TEST (Using a test signal less than $1280 \mathbf{~ M H z ) ~ ( c o n t ' d ) ~}$

## Procedure (cont'd)


${ }^{1}$ Refer to Application Note 150-4, HP 5952-1147, if additional information on calibration of spectrum analyzers for noise measurements is needed.
17. Calculate the Carrier Noise Test Set's residual phase noise at $10 \mathrm{~Hz}, 100 \mathrm{~Hz}$ and 1 kHz offsets from the carrier. Sum the measured noise level (C) and the 3 correction factors ${ }^{2}$ as shown below. Do not add the normalization to 1 Hz equivalent noise bandwidth factor, when using a spectrum analyzer with normalization to a 1 Hz bandwidth. This correction factor is accounted for automatically. Verify the residual phase noise level did not exceed the specified limit as shown at the bottom of each column.

|  | 10 Hz | 100 Hz | 1 kHz |
| :---: | :---: | :---: | :---: |
| Noise level = C (relative to reference level) <br> Normalization to 1 Hz equivalent noise bandwidth ${ }^{1}$ $-10 \log \left({ }^{\prime} B " \times 1.2\right)=$ <br> Calibration Attenuation (Step 7) <br> $\mathcal{L}(f)$ conversion factor <br> Total (dBc/Hz) | $\begin{gathered} \\ \\ \hline-50 \mathrm{~dB} \\ -6 \mathrm{~dB} \\ -<-115 \end{gathered}$ | $\qquad$ dB $\qquad$ dB <br> $-50 \mathrm{~dB}$ <br> $-6 \mathrm{~dB}$ $\qquad$ | $\begin{gathered} \\ \\ \hline-50 \mathrm{~dB} \\ \mathrm{~dB} \\ -6 \mathrm{~dB} \\ <-135 \end{gathered}$ |

${ }^{1}$ Refer to Application Note 150-4, HP 5952-1147, if additional information on calibration of spectrum analyzers for noise measurements is needed.

## NOTE

If an analog spectrum analyzer was used to measure the noise floor at $10 \mathrm{~Hz}, 100 \mathrm{~Hz}$, and 1 kHz , add +2.5 dB to the totals above as a correction for the log amplifiers and peak detectors in the analog spectrum analyzer.

[^5]
## PERFORMANCE TESTS

## 4-7. RESIDUAL PHASE NOISE PERFORMANCE TEST (Using a test signal of $10 \mathbf{G H z}$ )

 Specification| Electrical <br> Characteristics | Performance Limits | Conditions |
| :---: | :---: | :--- |
| Offset From | $\mathrm{dBc} / \mathrm{Hz}$ | With a 10 GHz input |
| Carrier | -90 | signal |
| 10 Hz | -105 |  |
| 100 Hz | -115 |  |
| 1 kHz | -127 |  |
| 10 kHz | -137 |  |
| 100 kHz | -142 |  |
| 1 MHz |  |  |

## Description

## NOTE

This performance test is only necessary when the residual phase noise of the Carrier Noise Test Set is in question.

This test verifies the Carrier Noise Test Set's residual phase noise specifications using a 10 GHz test signal. A second Carrier Noise Test Set is required as a reference unit in this test. Since this test requires a second Carrier Noise Test Set, we recommend that the phase noise of the other instruments in the phase noise measuring system be checked before this test is performed.

During the residual phase noise measurement the microwave test signal and the $5-1280 \mathrm{MHz}$ signal must be in phase quadrature (that is 90 degrees out of phase). One microwave synthesized source supplies the MICROWAVE TEST SIGNAL INPUT to both of the Carrier Noise Test Sets (device under test and reference). The IF OUTPUT of the reference Carrier Noise Test Set then supplies the $5-1280 \mathrm{MHz}$ INPUT of the Carrier Noise Test Set device under test. The Carrier Noise Test Set's residual phase noise is measured on a low frequency spectrum analyzer and an RF spectrum analyzer. Correction factors are added and the residual phase noise is verified to be below the specified limit.

## Equipment

Carrier Noise Test Set
HP 11729C
(used as reference)
RF Synthesized Signal Generator ........ HP 8662A (Option 003)
Microwave Synthesized Source ............ HP 8340A
Low Frequency Spectrum Analyzer ....... HP 3582A
RF Spectrum Analyzer ..................... HP 8566B
Power Meter ................................. HP 436A
Power Sensor . .............................. HP 8482A
Power Splitter (quantity 2) ................. HP 11667A
Amplifier ................................... HP 8447E/F
1 dB Step Attenuator (quantity 2) ......... HP 355C
Procedure Initial Instrument Settings

1. Connect the instruments as shown in Figure 4-3.
2. Turn on and warm-up the instruments for 30 minutes.
3. Set both step attenuators to maximum attenuation.

## PERFORMANCE TESTS

RESIDUAL PHASE NOISE PERFORMANCE TEST (Using a test signal of $10 \mathbf{G H z}$ ) (cont'd)
Procedure
(cont'd)


Figure 4-3. Residual Phase Noise Test Setup (Using a Test Signal of 10 GHz )
4. Set the Microwave Synthesized Soruce as follows:

Frequency $\qquad$ 10 GHz
Output Level $\ldots \ldots . .+10 \mathrm{dBm}$ to +20 dBm
5. Set the RF Synthesized Signal Generator (tunable reference) as follows:

Frequency 399.990 MHz

Output Level ......................... 0 dBm
6. Set both Carrier Noise Test Sets as follows:

Band Center Frequency $\qquad$ 9.6 GHz

Lock Bandwidth Factor ..................... . 1
Measurement Mode .................... $\phi$, CW

## PERFORMANCE TESTS

## RESIDUAL PHASE NOISE PERFORMANCE TEST (Using a test signal of 10 GHz ) (cont'd)

## Procedure Power Level Checks

7. Disconnect the cable which goes to the 640 MHz IN connector on the rear panel of the Carrier Noise Test Set device under test. Connect the power sensor to this cable. Adjust the step attenuator that is located before the power splitter, supplying the 640 MHz signal, such that the power meter reads between 0 dBm and +3 dBm . Reconnect the cable to the 640 MHz INPUT, on the rear panel, of Carrier Noise Test Set device under test.
8. Disconnect the end of cable $A$ which is connected to the $5-1280 \mathrm{MHz}$ INPUT on the Carrier Noise Test Set device under test. Connect the cable to a power sensor. Measure the IF OUTPUT power. Adjust the 1 dB step attenuator located after the IF OUTPUT of the reference Carrier Noise Test Set until the power meter reads -1 dBm to 0 dBm . Record the exact power meter reading below.

> Reference Carrier Noise Test Set IF OUTPUT power =
$\qquad$ dBm

## Spectrum Analyzer Calibration

9. Disconnect cable A from the power sensor. Connect the cable from the tunable reference output to the power sensor. Adjust the amplitude of the tunable reference until the power meter reads the power level recorded in step 8 . Connect the tunable reference to the $5-1280 \mathrm{MHz}$ INPUT on the Carrier Noise Test Set device under test.
10. Decrease the amplitude of the tunable reference by 50 dB . Adjust the RF spectrum analyzer to display the approximately 10 kHz beat note. (The beat note is the result of mixing the 400 MHz IF (MICROWAVE TEST SIGNAL INPUT minus the band center of the BAND RANGE chosen) and the 399.990 MHz tunable reference signal). Set the peak of the 10 kHz beat note to a convenient reference point.
11. Adjust the low frequency spectrum analyzer to view the approximately 10 kHz beat note. If the spectrum analyzer has selectable filters, select a flat top filter. If RMS averaging is available, select approximately 128 averages. RMS averaging smooths out the noise floor. If RMS averaging is not available the measurement should be made at an average level on the noise floor, not on a peak or valley.
12. Set the peak of the beat note to a convenient reference point.

## Residual Phase Noise Measurement

13. Disconnect the tunable reference from the 5 to 1280 MHz INPUT on the Carrier Noise Test Set device under test. Reconnect cable A to the $5-1280 \mathrm{MHz}$ INPUT on the Carrier Noise Test Set device under test.
14. Decrease the frequency of the Microwave Synthesized Source in 1 MHz steps, until the Carrier Noise Test Set device under test indicates phase quadrature (green LED is illuminated on the phase lock display.) Details of phase locking are found in Section III.

## PERFORMANCE TESTS

## RESIDUAL PHASE NOISE PERFORMANCE TEST (Using a test signal of $10 \mathbf{G H z}$ (cont'd)

Procedure (cont'd)
15. Adjust the RF spectrum analyzer to view the residual phase noise level at a 10 kHz offset from the carrier. For the most accurate measurement, use the smallest possible resolution bandwidth. Use averaging if required. Measure the residual phase noise level down from the reference point. Measure on an average phase noise level, do not measure on a peak or minimum phase noise level. Record the phase noise level (A) along with the measurement resolution bandwidth (B) below. Repeat this measurement for offsets of 100 kHz and 1 MHz .

| Offiset from <br> carrier | Noise level (A) <br> (relative to reference level) (dB) | Resolution Bandwidth (B) <br> (Hz) |
| :---: | :---: | :---: |
| 10 kHz | - | - |
| 100 kHz | - | - |
| 1 MHz | - |  |

16. On the low frequency spectrum analyzer, select a Hanning filter and the normalization to a 1 Hz bandwidth (if these features are available). If the spectrum analyzer does not have the feature for normalization to a 1 Hz bandwidth this figure will have to be calculated later using the formula at the end of the test.
17. Adjust the low frequency spectrum analyzer to view the residual phase noise level at 10 Hz . Measure the residual phase noise level down from the reference point. Measure on an average phase noise level; do not measure on a peak or minimum level.

NOTE
Power line spurs are not specified for the Carrier Noise Test Set. Power line spurs will appear at power line frequencies and multiples of power line frequencies. Do not make a phase noise measurement on a spur, make the measurement on an average noise level.
18. Record the phase noise level (C) below. If the measurement was not made in a 1 Hz resolution bandwidth, also record the measurement resolution bandwidth (D). Repeat this measurement at 100 Hz and 1 kHz offsets.

| Ofiset from <br> carrier | Noise level (C) <br> (relative to reference level) (dB) | Resolution Bandwidth (D) <br> (Hz) |
| :---: | :---: | :---: |
| 10 Hz |  |  |
| 100 Hz |  |  |
| 1 kHz | - |  |

19. Calculate the residual phase noise of the Carrier Noise Test Set at $10 \mathrm{kHz}, 100 \mathrm{kHz}$ and 1 MHz offsets from the carrier. Sum the measured phase noise level (A) and the 4 correction factors ${ }^{2}$ listed below. The normalization bandwidth factor is determined by putting the resolution bandwidth (B) into the equation below. Verify the residual phase noise level did not exceed the specified limit as shown at the bottom of each column.
[^6]
## PERFORMANCE TESTS

## RESIDUAL PHASE NOISE PERFORMANCE TEST (Using a test signal of 10 GHz ) (cont'd)

## Procedure (cont'd)

|  | 10 kHz | 100 kHz | 1 MHz |
| :---: | :---: | :---: | :---: |
| Noise level = A (relative to reference level) <br> Normalization to 1 Hz equivalent noise bandwidth ${ }^{1}$ $-10 \log (\text { " } \mathrm{B} " \mathrm{x} 1.2)=$ <br> Calibration Attenuation (Step 10) $\mathcal{L}(f)$ conversion factor <br> Correction for log amplifiers and peak detectors in analog spectrum analyzer | $\begin{gathered} \\ \hline-50 \mathrm{~dB} \\ -6 \mathrm{~dB} \\ \\ +2.5 \mathrm{~dB} \\ <-127 \end{gathered}$ | $\qquad$ dB $\qquad$ dB <br> $-50 \mathrm{~dB}$ <br> $-6 \mathrm{~dB}$ <br> $+2.5 \mathrm{~dB}$ $\qquad$ $<-137$ | $\qquad$ dB $\qquad$ dB <br> $-50 \mathrm{~dB}$ <br> $-6 \mathrm{~dB}$ $+2.5 \mathrm{~dB}$ $\qquad$ $<-142$ |
| ${ }^{1}$ Refer to Application Note 150-4, HP 5952-1147, if additional information on calibration of spectrum analyzers for noise measurements is needed. |  |  |  |

20. Calculate the residual phase noise level of the Carrier Noise Test Set at $10 \mathrm{~Hz}, 100$ Hz and 1 kHz offsets from the carrier. Sum the measured phase noise level (C) and the 3 correction factors ${ }^{2}$ below. Do not add the normalization to a 1 Hz equivalent noise bandwidth factor, when the spectrum analyzer accounts for this factor automatically. Verify the residual phase noise level does not exceed the specified limit shown at the bottom of each column.

|  | 10 Hz | 100 Hz | 1 kHz |
| :---: | :---: | :---: | :---: |
| Noise level = C (relative to reference level) | $\square \mathrm{dB}$ | $\longrightarrow$ dB | [ dB |
| Normalization to 1 Hz equivalent noise bandwidth ${ }^{1}$ $-10 \log (\text { " } \mathrm{D} \text { " } \times 1.2)=$ | dB |  | dB |
| Calibration Attenuation (Step 10) | $-50 \mathrm{~dB}$ | $-50 \mathrm{~dB}$ | $-50 \mathrm{~dB}$ |
| $\mathcal{L}(\mathrm{f})$ conversion factor | $-6 \mathrm{~dB}$ | $-6 \mathrm{~dB}$ | -6 dB |
| Total ( $\mathrm{dBc} / \mathrm{Hz}$ ) | - <-90 | -_<-105 | - <-115 |

${ }^{1}$ Refer to Application Note 150-4, HP 5952-1147, if additional information on calibration of spectrum analyzers for noise measurements is needed.

## NOTE

If an analog spectrum analyzer was used to measure the noise floor at $10 \mathrm{~Hz}, 100 \mathrm{~Hz}$ and 1 kHz add +2.5 dB to the totals above. This is the correction factor for the log amplifiers and peak detectors in the analog spectrum analyzer.

[^7]
## PERFORMANCE TESTS

## 4-8. AM NOISE FLOOR PERFORMANCE TEST

Specification

| Electrical <br> Characteristics | Performance Limits | Conditions |
| :---: | :---: | :---: |
| AM Noise Floor |  | At +10 dBm input level |
| Offset from | AM Noise |  |
| Carrier | $(\mathrm{dBc} / \mathrm{Hz})$ |  |
| 1 kHz | -138 |  |
| 10 kHz | -145 |  |
| 100 kHz | -155 |  |
| 1 MHz | -160 |  |

Description

Equipment Microwave Synthesized Source ............ HP 8340A
(with AM modulation)
Spectrum Analyzer ........................ HP 8566B
Function Generator ....................... HP 3312A
Coaxial to waveguide adapter ............. HP X281A
*Isolator . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . HP 0955-0178
Power Supply ................................ . HP 6214B
Power Meter .................................. HP 436A
Power Sensor . ............................... HP 8481A
Low Noise Oscillator ....................... . MA 86651A
*The isolator stabilizes load effects on the AM noise floor. When an isolator is not available an attenuator pad may be used. The attenuator pad may be used only if the output power of the oscillator is +10 dBm with the attenuator pad in place. If the measured power is +10 dBm or lower an isolator will have to be used. (See step 5 of the test procedure)

## Procedure Calibration

1. Connect the equipment as shown in Figure 4-4.
2. Connect +10 Vdc from the power supply to the low noise oscillator. Warm up the oscillator for 30 minutes.

## PERFORMANCE TESTS

## AM NOISE FLOOR PERFORMANCE TEST (cont'd)

Procedure (cont'd)


Figure 4-4. AM Noise Floor Test Set-up
3. Set the Microwave Synthesized Source as follows:

Frequency
AM modulation ........................... $50 \%$
4. Set the function generator as follows:

Function $\qquad$ sinewave
Frequency ............................ 100 kHz
5. Set the Carrier Noise Test Set as follows:

Measurement Mode AM, CW
All other controls .............. Any setting
6. Measure the power level of the low noise oscillator at the end of cable A (the end that connects to the MICROWAVE TEST SIGNAL INPUT). The level should be approximately +10 dBm . Connect an attenuator pad at the oscillator's output if the power level is above +10 dBm . The value of the attenuator pad selected should bring the measured power level to +10 dBm . Disconnect cable A from the power sensor.

Record the power level below.
$\qquad$ dBm

## PERFORMANCE TESTS

## AM NOISE FLOOR PERFORMANCE TEST (cont'd)

## Procedure (cont'd)

## NOTE

The AM noise floor of the Carrier Noise Test Set is specified for a +10 $d B m$ input level. Using an input signal lower than +10 dBm will increase the AM noise floor. The noise floor will increase by the amount in dB that the input signal was lowered from +10 dBm . As an example: a $+7 d B m$ input will raise the $A M$ noise floor by $+3 d B$.
Because our specifications are higher than typical measured values, an input signal of +5 dBm minimum will typically still measure within specifications.
7. Connect the end of the cable from the Microwave Synthesized Source to the power sensor. Adjust the amplitude of the Microwave Synthesized Source until the power meter reads the power level recorded in step 6.
8. Turn the Microwave Synthesized Source to external AM modulation. Connect the Microwave Synthesized Source to the spectrum analyzer. Be sure the input to the spectrum analyzer is 50 ohms .
9. Adjust the amplitude on the function generator so the sidebands displayed on the spectrum analyzer are -40 dBc . Disconnect the Microwave Synthesized Source from the spectrum analyzer and connect it to the Carrier Noise Test Set MICROWAVE TEST SIGNAL INPUT.
10. Connect the $<10 \mathrm{MHz}$ OUTPUT from the Carrier Noise Test Set to the spectrum analyzer. Adjust the spectrum analyzer to view the 100 kHz sidebands on the 1 GHz signal. Set the peak of the 100 kHz signal to a convenient reference point.

## AM Noise Floor Measurement

11. Disconnect the Microwave Synthesized Source from the MICROWAVE TEST SIGNAL INPUT. Connect the output of the low noise oscillator to the MICROWAVE TEST SIGNAL INPUT.

NOTE
The oscillator signal should come directly from the resonator with no amplification stage in between. Under this condition, it is likely that the AM noise coming from the oscillator is less than or equal to $-155 \mathrm{dBc} / \mathrm{Hz}$ at a 100 kHz offset.
12. Measure the noise level down from the reference point at a 100 kHz offset. Record the AM noise level (A) and resolution bandwidth (B) below. Measure the AM noise floor at a 1 MHz offset. Record this level with the corresponding resolution bandwidth below.

| Offset from <br> carrier | Noise level (A) <br> (relative to reference level) (dB) | Resolution Bandwidth (B) <br> [Hz) |
| :---: | :---: | :---: |
| 100 kHz | - | - |
| 1 MHz | - |  |

## PERFORMANCE TESTS

## AM NOISE FLOOR PERFORMANCE TEST (cont'd)

Procedure (cont'd)
13. Calculate the AM noise floor by summing the measured AM noise level (A) and the 3 correction factors ${ }^{2}$ shown below. The normalization bandwidth factor is determined by putting the resolution bandwidth (B) into the equation below. Verify the AM noise floor did not exceed the specified limit as shown at the bottom of each column.

|  | 100 kHz | 1 MHz |
| :---: | :---: | :---: |
| Noise level = A (relative to reference level) <br> Normalization to 1 Hz equivalent noise bandwidth ${ }^{1}$ $-10 \log (" B " \times 1.2)=$ <br> Calibration Attenuation (Step 8) <br> Correction for $\log$ amplifiers and peak detectors in analog spectrum analyzer Total (dBc/Hz) | $\begin{gathered} \\ \hline-40 \mathrm{~dB} \\ \\ \\ +2.5 \mathrm{~dB} \\ <-155 \end{gathered}$ | $\begin{gathered} \\ \hline-40 \mathrm{~dB} \\ \mathrm{~dB} \\ +2.5 \mathrm{~dB} \\ <-160 \end{gathered}$ |
| ${ }^{1}$ Refer to Application Note 150-4, HP 5952-1147, if additional information on calibration of spectrum analyzers for noise measurements is needed. |  |  |

[^8]Table 4-2. Performance Test Record


## SECTION V ADJUSTMENTS

## 5-1. INTRODUCTION

This section contains adjustments and checks that ensure peak performance of the Carrier Noise Test Set. The instrument should be readjusted after repair or after failure to pass a performance test. Allow a 30 minute warm-up period prior to performing the adjustments unless noted otherwise.

To determine which performance tests and adjustments to perform after a repair, refer to the paragraph entitled Related Adjustments. After the repair and/or adjustment, performance tests are usually required to verify performance.

## 5-2. SAFETY CONSIDERATIONS

This section contains information, cautions, and warnings which must be followed for your protection and to avoid damage to the equipment.

## WARNINGS

Adjustments described in this section are performed with power supplied to the instrument and with protective covers removed. Maintenance should be performed only by service trained personnel who are aware of the hazard involved (for example, fire and electrical shock). Where maintenance can be performed without power applied, the power should be removed.

Before the instrument is switched on, all protective earth terminals, extension cords, autotransformers and devices connected to it should be connected to a protective earth grounded socket. Any interruption of the protective earth grounding will cause a potential shock hazard that could result in personal injury.

> Whenever it is likely that the protection has been impaired, the instrument must be made inoperative and be secured against any unintended operation.

Only 250 V normal blow fuses with the required rated current should be used. Do not use repaired fuses or short circuited fuseholders. To do so could cause a shock or fire hazard.

## 5-3. EQUIPMENT REQUIRED

Each adjustment procedure contains a list of required test equipment. The test equipment is identified by callouts in the test setup diagrams where included.

If substitutions must be made for the specified test equipment, refer to Table 1-4 in Section I for the minimum specifications. It is important that the test equipment meet the critical specifications listed in the table if the Carrier Noise Test Set is to meet its performance requirements.

## 5-4. FACTORY-SELECTED COMPONENTS

Factory selected components are identified on the schematics and parts list by an asterisk (*) which follows the reference designator. The normal value or range of the components is shown. The manual change sheets may provide updated information pertaining to the selected components.

## 5-5. RELATED ADJUSTMENTS

The procedures in this section can be performed in any order. However, it is advisable to check the power supply voltages first.

NOTE
The steps within a procedure must be performed in the order listed.

## ADJUSTMENTS

## 5-6. POWER SUPPLY ADJUSTMENT

Reference $\quad$ Service Sheet 7
Description The +5.0 Vdc power supply is adjusted for $+5.000 \mathrm{Vdc} \pm 0.025 \mathrm{Vdc}$ at the 5 V Test Point A7TP3 using a digital multimeter.


Figure 5-1. +5.0 Vdc Power Supply Adjustment Setup
Digital Multimeter .............................. HP 3465A

## Equipment Procedure

1. Take off the top cover of the Carrier Noise Test Set. Locate the 5V Test Point A7TP3 on the power supply board. Turn on the Carrier Noise Test Set.
2. Connect the digital multimeter to the 5V Test Point A7TP3. Adjust A7R10 (+5V ADJ) for a reading of $+5.000 \mathrm{Vdc} \pm 0.025 \mathrm{Vdc}$ on the digital multimeter.

## ADJUSTMENTS

## 5-7. PHASE LOCK INDICATOR ADJUSTMENT

## Reference Service Sheet 3

## Description The Phase Lock Board is adjusted to calibrate the lock and unlock positions on the

 Phase Lock Indicator. If the Phase Lock Indicator does not agree with the status byte, sent out over HP-IB, the Phase Lock Board may need adjustment. The adjustments for the Phase Lock Indicator only need to be made in one BAND RANGE. The Phase Lock Board is also adjusted to compensate for dc offsets in the switchable gain amplifier and integrator.

Figure 5-2. Phase Lock Indicator Adjustment Setup
Equipment RF Synthesized Signal Generator .......... HP 8662A (Option 003)
Microwave Synthesized Source ..............HP 8340A
Computer Controller........................... HP 85B
Digital Multimeter . . . . . . . . . . . . . . . . . . . . . . HP 3465A
SMC to BNC adapter . . . . . . . . . . . . . . . . . . . . . . HP 1250-0831
BNC to alligator clips . . . . . . . . . . . . . . . . . . . HP 8120-1292
Procedure 1. Connect the equipment as shown in Figure 5-2.
2. Turn on and warm up all instruments for 30 minutes before doing the following adjustments.
3. Set the Carrier Noise Test Set as follows:

Lock Bandwidth Factor ...................... . 100
Measurement Mode................................ . . CW
Band Range..................................... 8.32 to 10.88 GHz
NOTE
If this BAND RANGE is not included in the Carrier Noise Test Set, select an available range.

## ADJUSTMENTS

## PHASE LOCK INDICATOR ADJUSTMENT (cont'd)

Procedure (cont'd)
4. Set the Microwave Synthesized Source (D.U.T.) as follows:

Amplitude .................................... +10 dBm
NOTE
The test signal is tuned 400 MHz above the BAND CENTER frequency of the BAND RANGE chosen.
5. Set the RF synthesized signal generator (tunable reference) as follows:

Frequency .................................... 400.001 MHz
Amplitude .................................... 0 dBm
NOTE
The difference in frequency between the IF signal (D.U.T. frequency minus the BAND CENTER frequency of the BAND RANGE chosen) and the tunable reference is called a beat note. By connecting the $<1$ MHz or $<10 \mathrm{MHz}$ NOISE SPECTRUM OUTPUT to a spectrum analyzer the approximately 1 kHz beat note can be viewed.
6. Remove the top cover of the Carrier Noise Test Set. Disconnect the cable to PHASE LOCK IN (A7J9) on the Power Supply Board. Connect an SMC to BNC adapter (HP 1250-0831) to PHASE LOCK IN (A7J9). Attach a BNC to alligator clip (HP 8120-1292) to the adapter that you just connected to PHASE LOCK IN (A7J9). Short the alligator clips to simulate a perfect phase lock.
7. Adjust DSP CNTR (A5R37), on the Phase Lock Board, to center the Phase Lock Indicator. A green LED should be displayed in the center of the indicator.

8. Connect the AUX NOISE OUTPUT, on the front panel, to LOOP TEST PORT IN on the rear panel. Two red LEDs should appear, one on either side of the center green LED. If the red LEDs are not illuminated adjust DSP DEV (A5R35) on the Phase Lock Board until the two red LEDs are visible. For optimum resolution no more than two red LEDs should be illuminated.
Fine adjust DSP CNTR (A5R37) until the red LEDs have equal intensity on both sides of the center green LED.
9. Remove the cable to the LOOP TEST PORT IN connector. Remove the short from the PHASE LOCK IN connector on the Power Supply Board and reconnect the original cable (W6) to the PHASE LOCK IN connector.
10. Set the LOCK BANDWIDTH FACTOR, on the front panel, to 1 .
11. Adjust DSP DEV (A5R35), on the Phase Lock Board, until the Phase Lock Indicator displays four (4) red LEDs to either side of center. The indicator may have to be

## ADJUSTMENTS

## PHASE LOCK INDICATOR ADJUSTMENT (cont'd)

Procedure (cont'd)

## M\& $\Leftrightarrow$

shaded to view the LEDs. The Phase Lock Indicator now displays maximum display deviation. The D.U.T. and the tunable reference must not phase lock during the adjustment. If they phase lock while making the adjustment, disconnect the FREQ-CONT X-OSC cable, on the rear panel of the Carrier Noise Test Set, then reconnect.
12. Increase the frequency of the tunable reference by 5 MHz to unlock the display. A red LED should be illuminated to the left of the center green LED. If the red LED is not illuminated adjust UNLK DSP (A5R5) until the red LED lights.

13. Decrease the frequency of the tunable reference by 5.001 MHz .
14. Be sure the LOCK BANDWIDTH FACTOR is set to 1 .
15. Press then release CAPTURE to enable phase lock. If phase lock is aquired go to step 16. If phase lock was not aquired proceed as follows:
The tunable reference must be tuned closer in frequency to the IF frequency ( $\mathrm{f}_{\mathrm{IF}}=$ $f_{\text {d.u.t }}-f_{\text {band center frequency }}$ ). Press CAPTURE while tuning the tunable reference in 1 kHz steps. Watch the phase lock indicator on the Carrier Noise TestSet. When the LED's on the indicator all light up, reduce the resolution of the tunable reference by a factor of 10 .

## NOTE

Connect the spectrum analyzer to the $<10 \mathrm{MHz}$ OUTPUT, on the Carrier Noise Test Set, if difficulties occur in determining the direction to tune the tunable reference to acquire phase lock.
The signals displayed on the spectrum analyzer represent the frequency difference between the two inputs to an internal mixer/phase detector in the Carrier Noise Test Set. The signals will decrease in frequency to dc when tuning towards phase lock and increase in frequency when tuning away from phase lock.

Press CAPTURE and tune in this reduced resolution. Watch the red LEDS on the Carrier Noise TestSet phase lock indicator step through one side of the display - to the green bar - then to the other side of the display. Again reduce the resolution on the tunable reference by a factor of 10 . Tune in this finer resolution until the green LED is illuminated. When the green LED is illuminated release CAPTURE.
16. Hold CAPTURE in and increase the tunable reference in 10 Hz steps until the loop becomes unlocked. Watch the phase lock indicator. The red LEDs should fully light one at a time and move to the right. When the last LED is illuminated and you tune further the entire indicator should dimly light. 39.9 \& 58
With CAPTURE pressed decrease the tunable reference in 10 Hz steps. The dimly illuminated indicator should change back to the red LEDs one at a time fully illuminated and moving to the left. When the last LED on the left is illuminated and you tune further, the entire indicator will dimly light.

$$
399897664
$$

## ADJUSTMENTS

## PHASE LOCK INDICATOR ADJUSTMENT (cont'd)

## Procedure (cont'd)

17. When the last LED on the left or right lights and the tunable reference is increased or decreased further, the indicator should immediately dimly light. If the indicator goes blank adjust DSP DEV (A5R35), on the Phase Lock Board, so the last LED on the right or left is illuminated. Tune further and the entire indicator should dimly light.
18. If DSP DEV did not need adjustment go to step 19. If DSP DEV was adjusted repeat steps $12-17$ because the adjustments UNLK DSP and DSP DEV are interactive.
19. Set the LOCK BANDWIDTH FACTOR, on the front panel, to 100.
20. Press and hold CAPTURE while tuning the tunable reference using a 100 Hz resolution. Tune until the tunable reference and D.U.T. are phase locked (green LED). Release CAPTURE. If the display changes to a red LED adjust OFF AD (A5R34), on the Phase Lock Board, to center the.display (green LED). If the display remains centered do not adjust OFF AD.
21. Set the LOCK BANDWIDTH FACTOR to 10. If the center green LED stays illuminated go to step 22. If the center green LED doesn't stay illuminated repeat step 20 with a 10 Hz resolution.
22. Set the LOCK BANDWIDTH FACTOR to 1 . The center green LED should stay illuminated. If the center green LED doesn't stay illuminated repeat step 20 with a 1 Hz resolution.
23. Use the following procedure to verify if the adjustment for UNLK DSP is calibrated correctly:

Enter Program 1 into a computer or controller that runs basic. Insert the correct select code and HP-IB address, for your Carrier Noise Test Set, into the SPOLL function. The HP-IB address of the Carrier Noise Test Set is factory preset to 06. The user can select the HP-IB address by changing the position of the HP-IB address switches on the rear panel of the Carrier Noise TestSet. (Refer to Section II paragraph 2-7, HP-IB Address Selection, for further information.)

## PROGRAM 1

```
10 A = SPOLL(###)
20 DISP A
30 GOTO 10
```

(\#\#\# = Current Carrier Noise Test Set select code and address.)
Example: 706
$7=$ Select code $06=$ Address

This program monitors the status byte of the Carrier Noise Test Set and displays the equivalent decimal value. The status of the phase lock detector sent out over HP-IB should agree with the phase lock indicator on the front panel. Table 5-1 defines the status bits and their decimal equivalents for the two phase lock conditions.

## ADJUSTMENTS

## PHASE LOCK INDICATOR ADJUSTMENT (cont'd)

Procedure (cont'd)

Table 5-1. Phase Lock and Unlock Status Bits

| Phase <br> Condition |  |  |  |  |  |  |  | Output <br> Decimal* $^{*}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | D108 | D107 | D106 | D105 | D104 | D103 | D102 |  |  |
| unlocked | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 4 |
| locked <br> (green bar) | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 2 |

*If no other bits are logical one.
24. Set the Carrier Noise Test Set to the phase lock condition (green LED is illuminated on the front panel phase lock indicator).
25. Run Program 1 and compare the number displayed on the computer to the phase condition of the phase lock indicator on the Carrier Noise Test Set. A decimal 2 is displayed when in the phase lock condition.
26. Increase the frequency of the tunable reference by 1 MHz . Verify that the unlocked condition (red LED adjacent to the left of the green LED) is detected by the microprocessor. A decimal 4 should be displayed on the computer.

If the number ( 2 or 4) displayed on the computer does not correspond to the phase lock condition, displayed on the front panel phase lock indicator, perform steps 12-18 again. Perform steps $23-26$ to verify the adjustments.

## ADJUSTMENTS

## 5-8. OPTION SWITCH ADJUSTMENT

## Reference <br> Service Sheet 6

## NOTE

If a filter is added to the Carrier Noise Test Set the inputs to the Option Switch (S1), on the microprocessor board, need to be changed.

Description The five (5) input switch (S1), on the microprocessor board, defines the options installed in the Carrier Noise Test Set. The switch should only be adjusted when the options are changed or the switch is being replaced.

## Procedure

1. Take off the bottom cover of the Carrier Noise Test Set
2. Unscrew the three Pozidriv screws, on microprocessor board (A9), to access the component side of the board.
3. Locate the five (5) input switch (S1) near the front panel. Table 5-2 defines the switch positions. The 0 and 1 logic levels are etched on the board on either side of the switch.

Table 5-2. Definition of Option Switch S1

| Switch Input Logic Levels |  |  |  |  | Total Number of Bands in the Carrier Noise Test Set |
| :---: | :---: | :---: | :---: | :---: | :---: |
| \#5 | \#4 | \#3 | \#2 | \#1 |  |
| X | 0 | 0 | 0 | 0 | 1 |
| X | 0 | 0 | 0 | 1 | 1 |
| X | 0 | 0 | 1 | 0 | 2 |
| X | 0 | 0 | 1 | 1 | 3 |
| X | 0 | 1 | 0 | 0 | 4 |
| X | 0 | 1 | 0 | 1 | 5 |
| X | 0 | 1 | 1 | 0 | 6 |
| X | 0 | 1 | 1 | 1 | 7 |
| X | 1 | 0 | 0 | 0 | 8 |
| X | 1 | 0 | 0 | 1 | 9 (exceeds capacity) |
| X | 1 | 0 | 1 | 0 | 10 (exceeds capacity) |
| X | 1 | 0 | 1 | 1 | 11 (exceeds capacity) |
| X | 1 | 1 | 0 | 0 | 1 |
| X | 1 | 1 | 0 | 1 | 1 |
| X | 1 | 1 | 1 | 0 | 1 |
| X | 1 | 1 | 1 | 1 | 1 |
| 0 | X | X | X | X | AM is not installed |
| 1 | X | X | X | X | AM is installed |
| X = Don't care |  |  |  |  |  |

4. If a filter is added to the instrument, switch S 1 to the corresponding logic levels for the total number of filters in the Carrier Noise Test Set.

## OPTION SWITCH ADJUSTMENT (cont'd)

Procedure (cont'd)
4. If a filter is added to the instrument, switch S1 to the corresponding logic levels for the total number of filters in the Carrier Noise Test Set.
5. Verify that the microprocessor recognizes the change by pressing the BAND RANGE button of the newly installed filter. The filter switch will click on and the LED on the BAND RANGE button will light if the microprocessor has acknowledged the new filter.
6. Reinstall the screws on the microprocessor board and replace the bottom cover.

## ADJUSTMENTS

## 5-9. PULSE BALANCE ADJUSTMENT

Reference Service Sheet 2
Description The COARSE BAL adjustment, on the rear of the front panel, is adjusted to center the tuning range of the front panel BAL control.

Procedure 1. Turn the Carrier Noise Test Set off.
2. Remove the top cover of the Carrier Noise Test Set.
3. Disconnect A3W11 from the IF port on the Low Pass Filter.
4. Turn the Carrier Noise Test Set on.
5. Press the MODE button, on the front panel, until the annunciator next to $\phi$, PULSED is illuminated.
6. Center the rotational swing of the front panel BAL control. .
7. Adjust the COARSE BAL potentiometer, on the rear of the front panel, until the front panel Phase Lock Indicator displays the center green LED.
8. Turn the Carrier Noise Test Set off.
9. Reconnect A3W11 to the IF port on the Low Pass Filter.
10. Replace the top cover of the Carrier Noise Test Set.

## SECTION VI REPLACEABLE PARTS

## 6-1. INTRODUCTION

This section contains information for ordering parts. Table 6-1 lists abbreviations used in the parts list and throughout the manual. Table 6-2 lists all replaceable parts in reference designator order. Table 6-3 contains the names and addresses that correspond to the manufacturers' code numbers.

## 6-2. ABBREVIATIONS

Table 6-1 lists abbreviations used in the parts list, schematics, and throughout the manual. In some cases, two forms of the abbreviation are used; one all in capital letters, and one partial or no capitals. This occurs because the abbreviations in the parts list are always all capitals. However, in the schematics and other parts of the manual, other abbreviation forms are used with both lower case and upper case letters.

## 6-3. REPLACEABLE PARTS LIST

Table 6-2 is the list of replaceable parts and is organized as follows:
a. Electrical assemblies and their components in alpha-numerical order by reference designation.
b. Chassis-mounted parts in alpha-numerical order by reference designation.
c. Miscellaneous parts.

The information given for each part consists of the following:
a. The Hewlett-Packard part number.
b. Part number check digit (CD).
c. The total quantity (Qty) in the instrument, which appears only at the first listing of a particular part number.
d. The description of the part.
e. A typical manufacturer of the part in a fivedigit code.
f. The manufacturer's number for the part.

## 6-4. FACTORY SELECTED PARTS (*)

Parts marked with an asterisk (*) are factory selected parts. The value listed in the parts list is the nominal value. Refer to Section V for information on determining what value to use for replacement.

## 6-5. PARTS LIST BACKDATING ( $\dagger$ )

Parts marked with a dagger ( $\dagger$ ) are different in instruments with serial number prefixes lower than the one that this manual applies to directly. Table 7-1 lists the backdating changes by serial number prefix. The backdating changes are contained in Section VII.

## 6-6. PARTS LIST UPDATING (Change Sheet)

Production changes to instruments made after the publication of this manual are accompanied by a change in the serial number prefix. Changes to the parts list are recorded by serial number prefix on a MANUAL CHANGES supplement. Also, parts list errors are noted in the ERRATA portion of the MANUAL CHANGES supplement.

## 6-7. ILLUSTRATED PARTS BREAKDOWN

Most mechanical parts are identified in Figures 6-1 through 6-7. These figures are located near the end of the Replaceable Parts table.

## 6-8. HARDWARE

Both metric and nonmetric screws are used in the Carrier Noise Test Set.

## 6-9. ORDERING INFORMATION

To order a part listed in the replaceable parts table, quote the Hewlett-Packard part number (with the check digit), indicate the quantity required and address the order to the nearest Hewlett-Packard office (see note). The check digit will ensure accurate and timely processing of your order.

To order a part that is not listed in the replaceable parts table, include the instrument model number, instrument serial number, description and function of the part, and the number of parts required. Address the order to the nearest Hewlett-Packard office.

## ORDERING INFORMATION (cont'd)

NOTE
Within the USA, it is better to order directly from the HP Parts Center in Mountain View, California. Ask your nearest HP office for information and forms for the "Direct Mail Order System."

## 6-10. RECOMMENDED SPARES LIST

Stocking spare parts for an instrument is often done to ensure quick return to service after a malfunction occurs. Hewlett-Packard prepares a "Recommended Spares" list for this instrument. The
contents of the list are based on failure reports and repair data. Quantities given are for one year of parts support. A complimentary copy of the "Recommended Spares" list may be requested from your nearest Hewlett-Packard office.

When stocking parts to support more than one instrument or to support a variety of HewlettPackard instruments, it may be more economical to work from one consolidated list rather than simply adding together stocking quantities from the individual instrument lists. Hewlett-Packard will prepare consolidated "Recommended Spares" lists for any number or combination of instruments. Contact your nearest Hewlett-Packard office for details.

Table 6-1. Reference Designations and Abbreviations (1 of 2)


Table 6-1. Reference Designations and Abbreviations (2 of 2)


NOTE
All abbreviations in the parts list will be in upper-case.

## MULTIPLIERS

| Abbreviation | Prefix | Multiple |
| :---: | :--- | :---: |
| T | tera | $10^{12}$ |
| G | giga | $10^{9}$ |
| M | mega | $10^{6}$ |
| k | kilo | $10^{3}$ |
| da | deka | 10 |
| d | deci | $10^{-1}$ |
| c | centi | $10^{-2}$ |
| m | milli | $10^{-3}$ |
| $\mu$ | micro | $10^{-6}$ |
| n | nano | $10^{-9}$ |
| p | pico | $10^{-12}$ |
| f | femto | $10^{-15}$ |
| a | atto | $10^{-18}$ |

Table 6-2. Replaceable Parts

| Reference Designation | HP Part Number | $\left\lvert\, \begin{aligned} & C \\ & D \end{aligned}\right.$ | Qty | Description | Mfr Code | Mir Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A1 | 11729-60011 | 8 | 1 | INDICATOR BOARD ASSEMBLY | 28480 | 11729-60011 |
| A1C1 | 0180-2617 | 1 | 4 | CAPACITOR-FXD 6.8UF+-10\% 35VDC TA | 25088 | D6R8GSIB35K |
| A1DS1 A1DS2 | $1990-0759$ $1990-0759$ | 6 | 2 | LED-LIGHT BAR MODULE LUM-INT $=3$ MCD LEC IGHT BAR MODULE | 28480 | HLMP-2620 |
| A1DS3 | 1990-0698 | 2 | 1 | LED-LIGHT BAR MODULE LUM-INT $=2$ MCD | 28480 28480 | HLMP-2620 1LMI-2500 |
| A1J1 | 1200-0508 | 0 | 3 | SOCKET-IC 14-CONT DIP-SLDR | 28480 | 1200-0508 |
| A1MP1 | 5041-0377 | 7 |  | KEY CAP FULL SMK | 28480 | 5041-0377 |
| A1MP2 | 1251-4459 | 5 | 3 | CLIP-CABLE PLUG RTNG-DUAL INLINE 14 CONT | 28480 | $1251-4459$ |
| A1R1 | 0698-7231 | 2 | 1 | RESISTOR 619 1\% . 056 d F TC=0+-100 | 24546 | C3-1/8-T0-619R-F |
| A1R2 A1R3 | 0698-7235 | 6 | 1 | RESISTOR 909 1\%.05W F TC $=0+-100$ | 24546 | C3-1/8-T0-909R-F |
| A1R3 A1R4 Al | $0698-7220$ $0698-7220$ | 9 9 | 8 | RESISTOR 215 RESISTOR 215 $1 \%$ | 24546 24546 | C3-1/8-T0-215R-F C3-1/8-T0-215R-F |
| A1R5 | 0698-7220 | 9 |  | RESISTOR 215 1\% . 05 W F TC=0+-100 | 24546 24546 | C3-1/8-T0-215R-F $\mathrm{C} 3-1 / 8-\mathrm{TO}-215 \mathrm{~F}-\mathrm{F}$ |
| A1R6 | 0698-7220 | 9 |  | RESISTOR $2151 \%$. 05 W F TC $=0+-100$ | 24546 | C3-1/8-T0-215R-F |
| A1R7 | 0698-7220 | 9 |  | RESISTOR 215 1\% .05w F TC $=0+-100$ | 24546 | C3-1/8-T0-215R-F |
| A1R8 A1R9 | 0698-7220 | 9 |  | RESISTOR 215 1\% .05w F TC=0+-100 | 24546 | C3-1/8-TO-215R-F |
| A1R9 AlR10 | $0698-7220$ $0698-7220$ | 9 9 |  | RESISTOR 215 RESISTOR 215 $1 \%$ | 24546 24546 | C3-1/8-TO-215R-F |
| Airio | 0698-7220 | 9 |  | RESISTOR 215 1\% .05W F TC=0+-100 | 24546 | C3-1/8-T0-215R-F |
| AlSi | 5060-9436 | 7 | 16 | PUSHBUTTON SWITCH P.C. MOUNT | 28480 | 5060-9436 |
| Alu1 | 1826-0655 | 4 | 1 | IC 18-DIP-P PKG | 27014 |  |
| A1U2 | 1826-0276 | 5 | 2 | IC 78L05A V RGLTR T0-92 | 04713 | MC78L05ACP |
| A1 XDS 1 | 1200-0507 | 9 | 2 | SOCKET-IC 16-CONT DIP-SLDR | 28480 | 1200-0507 |
| A1 XDS2 | 1200-0507 | 9 |  | SOCKET-IC 16-CONT DIP-SLDR | 28480 | 1200-0507 |
| A1 XDS3 | 11729-80004 | 1 | 1 | SKT, STRP 4 CONT | 28480 | 11729-80004 |
| A2 | 11729-60088 | 9 | 1 | FRONT PANEL KEY AND DISPLAY BOARD ASSY | 28480 | 11729-60088 |
| A2C1 | 0180-0116 | 1 | 5 | CAPACITOR-FXD 6.8UF+-10\% 35VDC TA | 56289 |  |
| A2C2 | 0180-0116 | 1 |  | CAPACITOR-FXD 6.8UF+-10\% 35VDC TA | 56289 | $1500685 \times 9035 B 2$ |
| A2DS 1 | 1990-0665 | 3 | 21 | LED-LAMP LUM-INT=1MCD IF=20MA-MAX BVR=5V | 28480 | 1990-0665 |
| A2DS2 | 1990-0665 | 3 |  | LED-LAMP LUM-INT $=1$ MCD $\quad$ IF $=20 \mathrm{MA}-\mathrm{MAX} \quad \mathrm{BVR}=5 \mathrm{~V}$ | 28480 | 1990-0665 |
| A2DS3 | 1990-0665 | 3 |  | LED-LAMP LUM-INT $=1 \mathrm{MCD} \quad \mathrm{IF}=20 \mathrm{MA}-\mathrm{MAX} \quad \mathrm{BVR}=5 \mathrm{~V}$ | 28480 | 1990-0665 |
| A2DS4 | 1990-0665 | 3 |  | LED-LAMP LUM-INT $=1 \mathrm{MCD} \quad \mathrm{IF}=20 \mathrm{MA}-\mathrm{MAX} \quad \mathrm{BVR}=5 \mathrm{~V}$ | 28480 | 1990-0665 |
| A2DS5 | 1990-0665 | 3 |  | LED-LAMP LUM-INT $=1$ MCD IF $=20 \mathrm{MA}-$ MAX $\quad \mathrm{BVR}=5 \mathrm{~V}$ | 28480 | 1990-0665 |
| A2DS6 | 1990-0665 |  |  | LED-LAMP LUM-INT=1MCD IF $=20 \mathrm{MA}-\mathrm{MAX}$ BVR $=5 \mathrm{~V}$ | 28480 | 1990-0665 |
| A2DS7 | 1990-0665 | 3 |  | LED-LAMP LUM-INT $=1 \mathrm{MCD}$ IF $=20 \mathrm{MA}-\mathrm{MAX} \quad \mathrm{BVR}=5 \mathrm{~V}$ | 28480 | 1990-0665 |
| A2DS8 | 1990-0665 | 3 |  | LED-LAMP LUM-INT $=1 \mathrm{MCD}$ IF $=20 \mathrm{MA}-\mathrm{MAX} \quad \mathrm{BVR}=5 \mathrm{~V}$ | 28480 | 1990-0665 |
| A2DS9 | 1990-0665 | 3 |  | LED-LAMP LUM-INT $=1 \mathrm{MCD}$ IF $=20 \mathrm{MA}-\mathrm{MAX} \quad \mathrm{BVR}=5 \mathrm{~V}$ | 28480 | 1990-0665 |
| A2DS10 | 1990-0665 | 3 |  | LED-LAMP LUM-INT $=1$ MCD $\quad$ IF $=20 \mathrm{MA}-\mathrm{MAX} \quad \mathrm{BVR}=5 \mathrm{~V}$ | 28480 | 1990-0665 |
| A2DS 11 | 1990-0665 | 3 |  | LED-LAMP LUM-INT=1MCD IF $=20 \mathrm{MA}-\mathrm{MAX}$ BVR $=5 \mathrm{~V}$ | 28480 | 1990-0665 |
| A2DS 12 | 1990-0665 | 3 |  | LED-LAMP LUM-INT $=1$ MCD $\quad$ IF $=20 \mathrm{MA}-\mathrm{MAX} \quad \mathrm{BVR}=5 \mathrm{~V}$ | 28480 | 1990-0665 |
| A2DS 13 | 1990-0665 | 3 |  | LED-LAMP LUM-INT $=1 \mathrm{MCD}$ IF $=20 \mathrm{MA}-\mathrm{MAX} \quad \mathrm{BVR}=5 \mathrm{~V}$ | 28480 | 1990-0665 |
| A2DS 14 | 1990-0665 | 3 |  | LED-LAMP LUM-INT $=1$ MCD $\quad$ IF $=20 \mathrm{MA}-\mathrm{MAX} \quad \mathrm{BVR}=5 \mathrm{~V}$ | 28480 | 1990-0665 |
| A2DS 15 | 1990-0665 | 3 |  | LED-LAMP LUM-INT $=1 \mathrm{MCD}$ IF $=20 \mathrm{MA}-\mathrm{MAX} \quad \mathrm{BVR}=5 \mathrm{~V}$ | 28480 | 1990-0665 |
| $\text { A2DS } 16$ | $1990-0665$ |  |  | LED-LAMP LUM-INT $=1$ MCD IF $=20 \mathrm{MA}-\mathrm{MAX}$ BVR $=5 \mathrm{~V}$ | 28480 |  |
| $\text { A2DS } 17$ | 1990-0665 | 3 |  | LED-LAMP LUM-INT $=1$ MCD $\quad$ IF $=20 \mathrm{MA}-$ MAX $\quad \mathrm{BVR}=5 \mathrm{~V}$ | 28480 | 1990-0665 |
| A2DS 18 A2DS 19 | $1990-0665$ $1990-0665$ | 3 3 3 |  | LED-LAMP LUM-INT $=1 \mathrm{MCD}$ IF $=20 \mathrm{MA}-\mathrm{MAX} \quad \mathrm{BVR}=5 V$ | 28480 | 1990-0665 |
| A2dS20 | $1990-0665$ $1990-0665$ | 3 3 |  |  | 28480 28480 | $1990-0665$ $1990-0665$ |
| A2DS21 | 1990-0665 | 3 |  | LED-LAMP LUM-INT $=1$ MCD IF $=20 \mathrm{MA}-$ MAX $\quad \mathrm{BVR}=5 \mathrm{~V}$ | 28480 | 1990-0665 |
| A2J 1 | 1251-5722 | 7 | 1 | CONNECTOR 50 -PIN M POST TYPE | 28480 | 1251-5722 |
| A2J2 | 1251-8391 | 2 | 1 | CONN-POST TYPE . 100-PIN-SPCG 4 -CONT | 28480 | 1251-8391 |
| A2MP 1 | 5041-0252 | 7 | 5 | KEY CAP 1/4 FOR LOCK BANDWIDTH SWIT HES | 28480 | 5041-0252 |
| A2MP2 | 5041-0252 | 7 |  | KEY CAP 1/4 FOR LOCK BANDWIDTH SWITCHES | 28480 | 5041-0252 |
| A2MP3 | 5041-0252 | 7 |  | KEY CAP 1/4 FOR LOCK BANDWIDTH SWITCHES | 28480 | 5041-0252 |
| A2MP4 | 5041-0252 | 7 |  | KEY CAP 1/4 FOR LOCK BANDWIDTH SWITCHES | 28480 | 5041-0252 |
| A2MP5 | 5041-0252 | 7 |  | KEY CAP 1/4 FOR LOCK BANDWIDTH SWITCHES | 28480 | 5041-0252 |
| A2MP6 | 5041-0352 |  | 8 | KEY CAP FOR FILTER SWITCHES |  |  |
| A2MP7 | $5041-0352$ | 8 |  | KEY CAP FOR FILTER SWITCHES | 28480 | $5041-0352$ |
| A2MP8 | 5041-0352 | 8 |  | KEY CAP FOR FILTER SWITCHES | 28480 | 5041-0352 |
| A2MP9 | $5041-0352$ | 8 |  | KEY CAP FOR FILTER SUITCHES | 28480 | 5041-0352 |
| A2MP10 | 5041-0352 | 8 |  | KEY CAP FOR FILTER SWITCHES | 28480 | 5041-0352 |

Table 6-2. Replaceable Parts

| Reference Designation | HP Part Number | $\left\lvert\, \begin{aligned} & C \\ & D \end{aligned}\right.$ | Qty | Description | Mir Code | Mir Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A2MP 11 | 5041-0352 | 8 |  | KEY CAP FOR FILTER SWITCHES | 28480 | 5041-0352 |
| A2MP12 | 5041-0352 | 8 |  | KEY CAP FOR FILTER SWITCHES | 28480 | 5041-0352 |
| A2MP13 | 5041-0352 | 8 |  | KEY CAP FOR FILTER SWITCHES | 28480 | 5041-0352 |
| A2MP14 | 5041-2811 | 8 | 1 | KEY CAP (MODE) | 28480 | 5041-2811 |
| A2MP15 | 5041-2812 | 9 | 1 | KEY CAP (LOCAL) | 28480 | 5041-2812 |
| A2MP16 | 5040-8823 | 2 | 1 | KNOB JADE GRAY | 28480 | 5040-8823 |
| A201 | 1853-0264 | 8 | 4 | TRANSISTOR PNP SI PD $=310 \mathrm{ML} \mathrm{FT}=100 \mathrm{MHZ}$ | 04713 | 2N5401 |
| A202 | 1853-0264 | 8 |  | TRANSISTOR PNP SI PD $=310 \mathrm{ML} \mathrm{FT}=100 \mathrm{MHZ}$ | 04713 | 2N5401 |
| A2Q3 | 1853-0264 | 8 |  | TRANSISTOR PNP SI PD $=310 \mathrm{ML} \mathrm{FT}=100 \mathrm{MHZ}$ | 04713 | 2N5401 |
| A204 | 1853-0264 | 8 |  | TRANSISTOR PNP SI PD $=310 \mathrm{ML}$ FT $=100 \mathrm{MHZ}$ | 04713 | 2N5401 |
| A205 | 1855-0082 | 2 | 1 | TRANSISTOR J-FET P-CHAN D-MODE SI | 28480 | 1855-0082 |
| A2R1 | 1810-0397 | 8 | 3 | NETWORK-RES 10-SIP68.0 OHM X 9 | 01121 | 2104680 |
| A2R2 | 1810-0397 | 8 |  | NETWORK-RES $10-$ SIP68.0 OHM X 9 | 01121 | 2104680 |
| A2R3 | 1810-0397 | 8 |  | NETWORK-RES 10-SIP68.0 OHM $\times 9$ | 01121 | 2104680 |
| A2R4 | 0757-0280 | 3 | 19 | RESISTOR $1 \mathrm{~K} 1 \% .125 \mathrm{~W}$ F TC $=0+-100$ | 24546 | C4-1/8-T0-1001-F |
| A2R5 | 0757-0280 | 3 |  | RESISTOR 1K 1\%.125W F TC $=0+-100$ | 24546 | C4-1/8-T0-1001-F |
| A2R6 | 0757-0280 | 3 |  | RESISTOR 1K 1\%. 125 W F TC=0+-100 | 24546 | C4-1/8-T0-1001-F |
| A2R7 | 0757-0421 | 4 | 4 | RESISTOR 825 1\% .125w F TC $=0+-100$ | 24546 | C4-1/8-T0-825R-F |
| A2R8 | 0757-0421 | 4 |  | RESISTOR 825 1\% .125W F TC $=0+100$ | 24546 | C4-1/8-T0-825R-F |
| A2R9 | 0698-3447 | 4 | 6 | RESISTOR 422 1\%. 125 W F TC $=0+-100$ | 24546 | C4-1/8-T0-422R-F |
| A2R10 | 0698-3162 | 0 | 3 | RESISTOR 46.4K 1\% .125U F TC=0+-100 | 24546 | C4-1/8-T0-4642-F |
| A2R11 | 0698-3157 |  |  | RESISTOR 19.6K 1\% . 125 W F TC=0+-100 | 24546 | C4-1/8-T0-1962-F |
| A2R12 | 2100-0558 | 9 | 1 | RESISTOR-TRMR 20K $10 \%$ C TOP-ADJ 1 -TRN | 28480 | $2100-0558$ |
| A2R13 | 2100-4109 | 4 | 1 | RESISTOR-VAR CONTROL C 2K 5\% LIN | 28480 | 2100-4109 |
| A2S1 | 5060-9436 | 7 |  | PUSHBUTTON SWITCH P.C. MOUNT | 28480 | 5060-9436 |
| A2S2 | 5060-9436 | 7 |  | PUSHBUTTON SWITCH P.C. MOUNT | 28480 | 5060-9436 |
| A2S3 | 5060-9436 | 7 |  | PUSHBUTTON SWITCH P.C. MOUNT | 28480 | 5060-9436 |
| A2S4 | 5060-9436 | 7 |  | PUSHBUTTON SWITCH P.C. MOUNT | 28480 | 5060-9436 |
| A2S5 | 5060-9436 | 7 |  | PUSHBUTTON SWITCH P.C. MOUNT | 28480 | 5060-9436 |
| A2S6 | 5060-9436 | 7 |  | PUSHBUTTON SWITCH P.C. MOUNT | 28480 | 5060-9436 |
| A2S7 | 5060-9436 | 7 |  | PUSHBUTTON SWITCH P.C. MOUNT | 28480 | 5060-9436 |
| A258 | 5060-9436 | 7 |  | PUSHBUTTON SWITCH P.C. MOUNT | 28480 | 5060-9436 |
| A259 | 5060-9436 | 7 |  | PUSHBUTTON SWITCH P.C. MOUNT | 28480 | 5060-9436 |
| A2S10 | 5060-9436 | 7 |  | PUSHBUTTON SWITCH P.C. MOUNT | 28480 | 5060-9436 |
| A2511 | 5060-9436 | 7 |  | PUSHBUTTON SWITCH P.C. MOUNT | 28480 | 5060-9436 |
| A2S12 | 5060-9436 | 7 |  | PUSHBUTTON SWITCH P.C. MOUNT | 28480 | 5060-9436 |
| A2S13 | 5060-9436 | 7 |  | PUSHBUTTON SWITCH P.C. MOUNT | 28480 | 5060-9436 |
| A2S14 | 5060-9436 | 7 |  | PUSHBUTTON SWITCH P.C. MOUNT | 28480 | 5060-9436 |
| A2S 15 | 5060-9436 | 7 |  | PUSHBUTTON SWITCH P.C. MOUNT | 28480 | 5060-9436 |
| A2TP1 | 0360-0535 | 0 | 26 | TERMINAL TEST POINT PCB | 00000 | ORDER BY DESCRIPTION |
| A2U1 | 1820-1208 | 3 | 5 | IC GATE TTL LS OR QUAD 2-INP | 01295 | SN74LS32N |
| A2U2 | 1820-2973 | 1 | 15 | IC DRVR TTL PRPHL HV DUAL | 28480 | 1820-2973 |
| A2W1 | 8159-0005 | 0 | 3 | Resistor-zero ohms 22 awg lead dia | 28480 | 8159-0005 |
| A3 | 11729-60087 | 8 | 1 | LOW PASS FILTER BOARD ASSEMBLY | 28480 | 11729-60087 |
| A3C1 | 0160-4767 | 4 | 1 | CAPACITOR-FXD 20PF +-5\% 200VDC CER 0+-30 | 28480 | 0160-4767 |
| A3C2 | 0160-2208 | 4 | 2 | CAPACITOR-FXD 330PF +-5\% 300VDC MICA | 28480 | 0160-2208 |
| АЗС3 | 0160-2208 | 4 |  | CAPACITOR-FXD 330PF +-5\% 300VDC MICA | 28480 | 0160-2208 |
| A3C4 | 0140-0210 | 2 | 2 | CAPACITOR-FXD 270PF +-5\% 300VDC MICA | 72136 | DM15F271J0300UVICR |
| АЗС5 | 0140-0210 | 2 |  | CAPACITOR-FXD 270PF +-5\% 300VDC MICA | 72136 | DM15F271J0300WVICR |
| $\begin{aligned} & \text { A3FL1- } \\ & \text { A3FL4 } \end{aligned}$ | 9135-0174 | 5 | 4 | FILTER-LOW PASS LEADS-TERMS | 28480 | 9135-0174 |
| A3J1 | 1250-1220 | 0 | 6 | CONNECTOR-RF SMC M PC 50-0HM | 28480 | 1250-1220 |
| A3J2 | 1250-1220 | 0 |  | CONNECTOR-RF SMC M PC 50-OHM | 28480 | 1250-1220 |
| A3J3 | 1250-1220 | 0 |  | CONNECTOR-RF SMC M PC 50-OHM | 28480 | 1250-1220 |
| A3J4 | 1250-1220 | 0 |  | CONNECTOR-RF SMC M PC 50-0HM | 28480 | 1250-1220 |
| A3J5 | 1250-1220 | 0 |  | CONNECTOR-RF SMC M PC 50-OHM | 28480 | 1250-1220 |
| АЗJ6 | 1250-1220 | 0 |  | CONNECTOR-RF SMC M PC 50-OHM | 28480 | 1250-1220 |
| $\begin{aligned} & \text { A3K1 } \\ & \text { A3K2 } \end{aligned}$ | $\begin{aligned} & 0490-1013 \\ & 0490-1013 \end{aligned}$ | 6 6 | 2 | RELAY-REED 1 C 250MA 28VDC 5VDC-COIL 3VA RELAY-REED 1C 250MA 28VDC 5VDC-COIL 3VA | $\begin{aligned} & 28480 \\ & 28480 \end{aligned}$ | $\begin{aligned} & 0490-1013 \\ & 0490-1013 \end{aligned}$ |

Table 6-2. Replaceable Parts

| Reference Designation | HP Part Number | $\left\lvert\, \begin{aligned} & \mathrm{C} \\ & \mathrm{D} \end{aligned}\right.$ | Qty | Description | Mfr Code | Mir Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A3Li | 9140-0094 | 9 | 2 | INDUCTOR RF-CH-MLD 680NH $10 \%$ | 28480 | 9140-0094 |
| A3L2 | 9100-1615 | 8 | 1 | INDUCTOR RF-CH-MLD 1.2UH 10\% | 28480 | 9100-1615 |
| A3L3 | 9140-0094 | 9 |  | INDUCTOR RF-CH-MLD 680NH 10\% | 28480 | 9140-0094 |
| A3L4 | 9140-0238 | 3 | 2 | INDUCTOR RF-CH-MLD 82UH 5\% . 166DX.385LG | 28480 | 9140-0238 |
| A3L5 | 9140-0178 | 0 | 1 | INDUCTOR RF-CH-MLD 12UH 10\% . 166DX.385LG | 28480 | 9140-0178 |
| A3L6 | 9100-1638 | 5 | 1 | INDUCTOR RF-CH-MLD 130UH 5\% .166DX.385LG | 28480 | 9100-1638 |
| A3L7 | 9140-0238 | 3 |  | INDUCTOR RF-CH-MLD 82UH 5\% .1660X.385LG | 28480 | 9140-0238 |
| A3MP1 | 2190-0124 | 4 | 18 | WASHER-LK INTL T NO. 10.195-IN-ID | 28480 | 2190-0124 |
| A3MP2 | 2190-0124 | 4 |  | WASHER-LK INTL T NO. $10.195-\mathrm{IN}$-ID | 28480 | 2190-0124 |
| A3MP3 | 2190-0124 | 4 |  | WASHER-LK INTL T NO. $10.195-\mathrm{IN}$-ID | 28480 | 2190-0124 |
| A3MP4 | 2190-0124 | 4 |  | WASHER-LK INTL T NO. $10.195-\mathrm{IN}$-ID | 28480 | 2190-0124 |
| A3MP5 | 2190-0124 | 4 |  | WASHER-LK INTL T NO. $10.195-\mathrm{IN}$-ID | 28480 | 2190-0124 |
| A3MP6 | 2190-0124 | 4 |  | WASHER-LK INTL T NO. $10.195-\mathrm{IN}$-ID | 28480 | 2190-0124 |
| A3MP7 | 2190-0124 | 4 |  | WASHER-LK INTL T NO. $10.195-\mathrm{IN}$-ID | 28480 | 2190-0124 |
| A3MP8 | 2190-0124 | 4 |  | UASHER-LK INTL T NO. $10.195-\mathrm{IN}$-ID | 28480 | 2190-0124 |
| A3MP9 | 2190-0124 | 4 |  | WASHER-LK INTL T NO. $10 \cdot 195-\mathrm{IN}$-ID | 28480 | 2190-0124 |
| A3MP10 | 2190-0124 | 4 |  | WASHER-LK INTL T NO. $10.195-\mathrm{IN}$-ID | 28480 | 2190-0124 |
| A3MP11 | 2190-0124 | 4 |  | WASHER-LK INTL T NO. $10.195-\mathrm{IN}$-ID | 28480 | 2190-0124 |
| A3MP12 | 2190-0124 | 4 |  | WASHER-LK INTL T NO. 10.195-IN-ID | 28480 | 2190-0124 |
| A3MP13 | 2950-0078 | 9 | 18 | NUT-HEX-DBL-CHAM 10-32-THD .067-IN-THK | 28480 | 2950-0078 |
| A3MP14 | 2950-0078 | 9 |  | NUT-HEX-DBL-CHAM 10-32-THD . 067 -IN-THK | 28480 | 2950-0078 |
| A3MP15 | 2950-0078 | 9 |  | NUT-HEX-DBL-CHAM 10-32-THD .067-IN-THK | 28480 | 2950-0078 |
| A3MP16 | 2950-0078 | 9 |  | NUT-HEX-DBL-CHAM 10-32-THD .067-IN-THK | 28480 | 2950-0078 |
| A3MP17 | 2950-0078 | 9 |  | NUT-HEX-DEL-CHAM 10-32-THD .067-IN-THK | 28480 | 2950-0078 |
| A3MP18 | 2950-0078 | 9 |  | NUT-HEX-DBL-CHAM 10-32-THD . 067 -IN-THK | 28480 | 2950-0078 |
| A3MP19 A3MP20 | 2950-0078 | 9 |  | NUT-HEX-DBL-CHAM 10-32-THD . 067-IN-THK | 28480 | 2950-0078 |
| A3MP20 | 2950-0078 | 9 |  | NUT-HEX-DEL-CHAM 10-32-THD .067-IN-THK | 28480 | 2950-0078 |
| A3MP21 | 2950-0078 | 9 |  | NUT-HEX-DEL-CHAM 10-32-THD .067-IN-THK | 28480 | 2950-0078 |
| A3MP22 | 2950-0078 | 9 |  | NUT-HEX-DBL-CHAM 10-32-THD .067-IN-THK | 28480 | 2950-0078 |
| A3MP23 | 2950-0078 | 9 |  | NUT-HEX-DBL-CHAM 10-32-THD .067-IN-THK | 28480 | 2950-0078 |
| A3MP24 | 2950-0078 | 9 |  | NUT-HEX-DEL-CHAM 10-32-THD .067-IN-THK | 28480 | 2950-0078 |
| A3MP25 | 11729-20091 | 0 | 1 | LOW PASS FILTER CAN | 28480 | 11729-20091 |
| A3MP26 | 3050-0079 | $3$ | 8 | WASHER-FL NM NO. 2 . 094-IN-ID . 188-IN-OD | 28480 | 3050-0079 |
| A3MP27 | 3050-0079 | 3 |  | WASHER-FL NM NO. 2 .094-IN-ID . 188-IN-OD | 28480 | 3050-0079 |
| A3MP28 | 3050-0079 | 3 |  | WASHER-FL NM NO. 2 . 094 -IN-ID 188 -IN-OD | 28480 | 3050-0079 |
| A3MP29 | 3050-0079 | 3 |  | UASHER-FL NM NO. $2.094-I N-I D .188-I N-O D$ | 28480 | 3050-0079 |
| АЗМР30. | 3050-0079 | 3 |  | WASHER-FL NM NO. 2 . $094-I N-I D .188-I N-O D$ | 28480 | 3050-0079 |
| A3MP31 | 3050-0079 | 3 |  | WASHER-FL NM NO. 2 .094-IN-ID . 188-IN-OD | 28480 | 3050-0079 |
| A3MP32 | 2190-0009 | 4 | 5 | WASHER-LK INTL T NO. 8 .168-IN-ID | 28480 | 2190-0009 |
| A3MP33 | 2190-0009 | 4 |  | WASHER-LK INTL T NO. 8.168-IN-ID | 28480 | 2190-0009 |
| A3MP34 | 2580-0002 | 4 | 5 | NUT-HEX-DBL-CHAM 8-32-THD .085-IN-THK | 28480 | 2580-0002 |
| A3MP35 | 2580-0002 | 4 |  | NUT-HEX-DEL-CHAM 8-32-THD .085-IN-THK | 28480 | 2580-0002 |
| A3MP36 | 2580-0002 |  |  | NUT-HEX-DBL-CHAM 8-32-THD .085-IN-THK | 28480 | 2580-0002 |
| A3MP37 | 2580-0002 | 4 |  | NUT-HEX-DBL-CHAM 8-32-THD . 085 -IN-THK | 28480 | 2580-0002 |
| A3MP38 | 2190-0009 | 4 |  | WASHER-LK INTL T NO. 8 .168-IN-ID | 28480 | 2190-0009 |
| A3MP39 | 2190-0009 | 4 |  | WASHER-LK INTL T NO. 8 . 168-IN-ID | 28480 | 2190-0009 |
| A3MP40 | 2950-0078 | 9 |  | NUT-HEX-DEL-CHAM 10-32-THD .067-IN-THK | 28480 | 2950-0078 |
| A3MP41 | 2950-0078 | 9 |  | NUT-HEX-DBL-CHAM 10-32-THD .067-IN-THK | 28480 | 2950-0078 |
| A3MP42 | 2950-0078 | 9 |  | NUT-HEX-DBL-CHAM 10-32-THD . 067 -IN-THK | 28480 | 2950-0078 |
| A3MP43 | 2950-0078 | 9 |  | NUT-HEX-DBL-CHAM 10-32-THD .067-IN-THK | 28480 | 2950-0078 |
| A3MP44 | 3050-0079 | 3 |  | WASHER-FL NM NO. 2 . 094 -IN-ID . 188-IN-OD | 28480 | 3050-0079 |
| A3MP45 | 3050-0079 | 3 |  | WASHER-FL NM NO. 2 .094-IN-ID .188-IN-OD | 28480 | 3050-0079 |
| A3MP46 | $2190-0124$ | 4 |  | WASHER-LK INTL T No. $10.195-\mathrm{IN}$-ID | 28480 | 2190-0124 |
| A3MP47 | 2190-0124 | 4 |  | WASHER-LK INTL T NO. $10.195-\mathrm{IN}$-ID | 28480 | 2190-0124 |
| A3MP48 | 2190-0124 | 4 |  | WASHER-LK INTL T NO. $10.195-\mathrm{IN}$-ID | 28480 | 2190-0124 |
| A3MF49 | 2190-0124 | 4 |  | WASHER-LK INTL T NO. $10.195-\mathrm{IN}$-ID | 28480 | 2190-0124 |
| A3R1 | 0698-7205 | 0 |  | RESISTOR 51.1 1\% . O5W F TC $=0+-100$ | $24546$ |  |
| A3R2 | 0757-0417 | 8 | 2 | RESISTOR 562 1\% .125W F TC $=0+-100$ | $24546$ | $C 4-1 / 8-T 0-562 R-F$ |
| A3R3 | 0757-0417 | 8 |  | RESISTOR 562 1\% . 125 W F TC=0+-100 | $24546$ | C4-1/8-T0-562R-F |
| A3R4 | 0698-0083 | 8 | $1$ | RESISTIOR 1.96K $1 \% .125 \mathrm{~W}$ F TC $=0+-100$ | $24546$ | $\mathrm{C}-1 / 8-\mathrm{TO}-1961-\mathrm{F}$ |
| A3R5 | 0698-0089 | 4 | $i$ | RESISTOR 1.78K $1 \%$. 5 W F TC $=0+-100$ | $28480$ | 0699-0089 |
|  | 0515-0208 | 3 | 8 | SCREW-MACH M3 $\times 0.5$ 14MM-LG PAN-HD (USED TO MOUNT The A3 acsembly to THE DECK) | 28480 | 0515-0208 |
|  | 2190-0584 | 0 | 112 | WASHER-LK HLCL 3.0 MM 3.1-MM-ID (USED TO MOUNT THE A3 ASSEMBLY TO THE DECK) | 28480 | 2190-0584 |

Table 6-2. Replaceable Parts

| Reference Designation | HP Part Number |  | Qty | Description | Mfr Code | Mir Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A4 |  |  |  | NOT ASSIGNED |  |  |
| A5 | 11729-60002 | 7 | 1 | PHASELOCK BOARD ASSEMBLY | 28480 | 11729-60002 |
| A5C1 | 0180-2617 | 1 |  | CAPACITOR-FXD 6.8UF+-10\% 35VDC TA | 25088 | D6R8GS1B35K |
| A5C2 | 0180-2617 | 1 |  | CAPACITOR-FXD 6.8UF+-10\% 35VDC TA | 25088 | D6R8GS1835K |
| A5C3 | 0160-0576 | 5 | 3 | CAPACITOR-FXD . $1 \mathrm{UF}+$ +-20\% SOVDC CER | 28480 | 0160-0576 |
| A5C4 | 0160-3830 | 0 | 2 | CAPACITOR-FXD SUF +-10\% 50VDC MET-POLYC | 28480 | 0160-3830 |
| A5C5 | 0160-3830 | 0 |  | CAPACITOR-FXD SUF +-10\% SOVDC MET-POLYC | 28480 | 0160-3830 |
| A5C6 | 0160-0571 | 0 | 2 | CAPACITOR-FXD 470PF +-20\% 100VDC CER | 28480 | 0160-0571 |
| A5C7 | 0160-0576 | 5 |  | CAPACITOR-FXD . $1 \mathrm{UF}+-20 \% 50 \mathrm{VDC}$ CER | 28480 | 0160-0576 |
| A5CR1 | 1901-0050 | 3 | 13 | DIODE-SWITCHING 80V 200MA 2NS D0-35 | 28480 | 1901-0050 |
| A5CR2 | 1901-0050 | 3 |  | DIODE-SWITCHING 80V 200MA 2NS DO-35 | 28480 | $1901-0050$ |
| ASCR3 | 1901-0050 | 3 |  | DIODE-SWITCHING 80V 200MA 2NS DO-35 | 28480 | 1901-0050 |
| A5CR4 | 1901-0050 | 3 |  | DIODE-SWITCHING 80V 200MA 2NS DO-35 | 28480 | 1901-0050 |
| ASCR5 | 1901-0050 | 3 |  | DIODE-SWITCHING 80V 200MA 2NS DO-35 | 28480 | 1901-0050 |
| A5CR6 | 1901-0050 | 3 |  | DIODE-SWITCHING 80V 200MA 2NS DO-35 | 28480 | 1901-0050 |
| A5CR7 | 1901-0050 | 3 |  | DIODE-SWITCHING 8OV 200MA 2NS DO-35 | 28480 | $1901-0050$ |
| ASK1 | 0490-0916 | 6 | 2 | RELAY-REED 1A 500MA 100VDC SVDC-COIL | 28480 |  |
| ASK2 | 0490-0916 | 6 |  | RELAY-REED 1A 500MA 100VDC SVDC-COIL | 28480 | 0490-0916 |
| ASL 1 | 9100-1626 | 1 | 3 | INDUCTOR RF-CH-MLD 36UH 5\% . 166 DX .385 LG | 28480 | 9100-1626 |
| A5L2 | 9100-1626 | 1 |  | INDUCTOR RF-CH-MLD 36UH 5\% . 166DX.385LG | 28480 | 9100-1626 |
| A5MP1 | 5040-6852 | 3 | 1 | EXTRACTOR, ORANGE | 28480 | $5040-6852$ |
| A5MP2 | 5000-9043 | 6 | 1 | PIN:P.C. BOARD EXTRACTOR | 28480 | $5000-9043$ |
| A5R1 | 0757-0442 | 9 | 8 | RESISTOR 10K 1\%.125w F TC $=0+-100$ | 24546 | C4-1/8-T0-1002-F |
| A5R2 | 0757-0442 | 9 |  | RESISTOR 10K 1\% .125W F TC $=0+-100$ | 24546 | C4-1/8-70-1002-F |
| A5R3 | 0757-0442 | 9 |  | RESISTOR 10K 1\%. 125 W F TC $=0+-100$ | 24546 | C4-1/8-T0-1002-F |
| A5R4 | 0757-0465 | 6 | 9 | RESISTOR 100K 1\% . 125 W F TC $=0+-100$ | 24546 | $\mathrm{C} 4-1 / 8-\mathrm{TO}-1003-\mathrm{F}$ |
| A5R5 | 2100-2514 | 1 | 2 | RESISTOR-TRMR 20K 10\% C SIDE-ADJ 1-TRN | 30983 | ET50W203 |
| A5R6 | 0757-0438 | 3 | 3 | RESISTOR 5.11K 1\% . 125 W F TC $=0+-100$ | 24546 | C4-1/8-70-5111-F |
| A5R7 | 0757-0458 | 7 | 3 | RESISTOR 51.1K 1\% .125W F TC $=0+-100$ | 24546 | $\mathrm{C} 4-1 / 8-\mathrm{TO}-5112-\mathrm{F}$ |
| A5R8 | 0757-0280 | 3 |  | RESISTOR 1K 1\%. 125 W F TC $=0+-100$ | 24546 | C4-1/8-T0-1001-F |
| ASR9 | 0757-0442 | 9 |  | RESISTOR 10K $1 \%$. 125 W F TC $=0+-100$ | 24546 | C4-1/8-T0-1002-F |
| ASR10 | 0757-0280 | 3 |  | RESISTOR 1K $1 \% .125 \mathrm{~W}$ F TC $=0+-100$ | 24546 | C4-1/8-T0-1001-F |
| A5R11 | 0757-0442 | 9 |  | RESISTOR 10K 1\%.125 W F TC $=0+-100$ | 24546 | C4-1/8-70-1002-F |
| A5R12 | 0757-0465 | 6 |  | RESISTOR 100K $1 \% .125 \mathrm{~W}$ F TC $=0+-100$ | 24546 | C4-1/8-T0-1003-F |
| A5R13 | 0757-0444 | 1 | 1 | RESISTOR 12.1K 1\%.125W F TC $=0+-100$ | 24546 | C4-1/8-T0-1212-F |
| ASR14 | 0698-3162 | 0 |  | RESISTOR 46.4K 1\% . 125 W F TC $=0+-100$ | 24546 | C4-1/8- 0 - $4642-\mathrm{F}$ |
| ASR15 | 0757-0200 | 7 | 1 | RESISTOR 5.62K 1\% . 125 W F TC $=0+-100$ | 24546 | C4-1/8-T0-5621-F |
| ASR16 |  |  |  | RESISTOR 46.4K 1\% .125W F TC=0+-100 | 24546 | C4-1/8-T0-4642-F |
| A5R17 | 0757-0421 | 4 |  | RESISTOR 825 1\% .125W F TC $=0+-100$ | 24546 | $\mathrm{C} 4-1 / 8-\mathrm{TO}-825 \mathrm{R}-\mathrm{F}$ |
| A5R18 | 0757-0443 | 0 | 3 | RESISTOR $11 \mathrm{~K} 1 \%$. 125 W F TC $=0+-100$ | 24546 | C4-1/8-T0-1102-F |
| A5R19 | 0757-0465 | 6 |  | RESISTOR 100K 1\%. 125 W F TC $=0+-100$ | 24546 | $\mathrm{C} 4-1 / 8-\mathrm{TO}-1003-\mathrm{F}$ |
| A5R20 | 0698-3154 | 0 | 3 | RESISTOR 4.22K 1\% . 125 W F T C $=0+-100$ | 24546 | C4-1/8-T0-4221-F |
| ASR21 | 0757-0465 | 6 |  | RESISTOR 100K 1\% . 125 W F TC=0+-100 | 24546 | C4-1/8-T0-1003-F |
| A5R22 | 0757-0438 | 3 |  | RESISTOR $5.11 \mathrm{~K} 1 \% .125 \mathrm{~W}$ F TC $=0+-100$ | 24546 | C4-1/8-T0-5111-F |
| A5R23 | 0757-0461 | 2 | 1 |  | 24546 | $\mathrm{C} 4-1 / 8-\mathrm{T0}-6812 \cdot \mathrm{~F}$ |
| A5R24 | 0757-0438 | 3 |  | RESISTOR 5.11K 1\% . 125 W F TC $=0+-100$ | 24546 | $\mathrm{C} 4-1 / 8-\mathrm{TO}-5111-\mathrm{F}$ |
| A5R25 | 0757-0439 | 4 | 1 | RESISTOR $6.81 \mathrm{~K} 1 \% .125 \mathrm{~W}$ F TC $=0+-100$ | 24546 | C4-1/8-T0-6811-F |
| A5R26 | 0757-0280 | 3 |  | RESISTOR 1K 1\% . 125 W F TC=0+-100 | 24546 | C4-1/8-70-1001-F |
| A5R27 | 0757-0421 | 4 |  | RESISTOR 825 1\%.125W F TC $=0+-100$ | 24546 | C4-1/8-T0-825R-F |
| A5R28 | 0757-0443 | 0 |  | RESISTOR $11 \mathrm{~K} 1 \%$. 125 W F TC $=0+-100$ | 24546 | $\mathrm{C} 4-1 / 8-\mathrm{TO}-1102-\mathrm{F}$ |
| A5R29 | 0757-0465 | 6 |  | RESISTOR 100K $1 \% .125 \mathrm{~W}$ F TC $=0+-100$ | 24546 | C4-1/8-T0-1003-F |
| A5R30 | 0757-0465 | 6 |  | RESISTOR 100K 1\% . 125 W F TC $=0+-100$ | 24546 | C4-1/8-T0-1003-F |
| A5R31 | 0757-0465 | 6 |  | RESISTOR 100K 1\% . 125 W F TC= $0+-100$ | 24546 | C4-1/8-70-1003-F |
| A5R32 | 0757-0443 | 0 |  | RESISTOR 11K $1 \% .125 \mathrm{~W}$ F TC $=0+-100$ | 24546 | $\mathrm{C} 4-1 / 8-\mathrm{TO}-1102-\mathrm{F}$ |
| A5R33 | 0757-0442 | 9 |  | RESISTOR 10K 1\%. 125 W F TC $=0+-100$ | 24546 | C4-1/8-T0-1002-F |
| A5R34 | 2100-2516 | 3 | 2 | RESISTOR-TRMR 100K 10\% C SIDE-ADJ 1-TRN | 32997 | 3329W-1-104 |
| A5R35 | 2100-2516 | 3 |  | RESISTOR-TRMR 100K 10\% C SIDE-ADJ 1-TRN | 32997 | 3329w-1-104 |
| A5R36 | $0698-3450$ | $9$ | 1 | RESISTOR 42.2K 1\% .125W F TC=0+-100 | $24546$ |  |
| A5R37 | $2100-2514$ | 1 |  | RESISTOR-TRMR 20K 10\% C SIDE-ADJ 1-TRN | $30983$ | ETSOW203 |
| A5R38 | 0757-0465 | 6 |  | RESISTOR 100K $1 \% .125 \mathrm{~W}$ F TC $=0+-100$ | 24546 | C4-1/8-T0-1003-F |
| A5R39 | 0698-3160 | 8 | 2 | RESISTOR 31.6K 1\% . 125 W F $\mathrm{T} C=0+-100$ | 24546 | C4-1/8-T0-3162-F |
| A5R40 | 0698-3160 | 8 |  | RESISTOR 31.6K 1\% .125W F TC $=0+-100$ | 24546 | C4-1/8-70-3162-F |

Table 6-2. Replaceable Parts

| Reference Designation | HP Part Number | $\mathrm{C}$ | Qty | Description | Mfr Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A5R41 | 0757-0442 | 9 |  | RESISTOR 10K 1\% . 125 W F TC $=0+100$ | 24546 |  |
| A5R42 | 0698-3440 | 7 | 1 | RESISTOR $1961 \% .125 \mathrm{~W}$ F TC $=0+-100$ | 24546 | C4-1/8-T0-196R-F |
| A5R43 | 0757-0465 | 6 |  | RESISTOR 100K $1 \% .125 \mathrm{~W}$ F TC $=0+-100$ | 24546 | C4-1/8-T0-1003-F |
| A5R44 | 0757-0280 | 3 |  | RESISTOR $1 \mathrm{~K} 1 \% .125 \mathrm{~W}$ F TC $=0+-100$ | 24546 | C4-1/8-T0-1001-F |
| A5R45 | 0757-0401 | - | 7 | RESISTOR 100 1\%.125w F TC $=0+-100$ | 24546 | C4-1/8-T0-101-F |
| ASR4E | 0698-0082 | 7 | 1 | RESISTOR 464 1\% . 125 w F TC $=0+-100$ | 24546 | C4-1/8-T0-4640-F |
| A5R47 | 0757-0401 | 0 |  | RESISTOR 100 1\% .125w F TC $=0+-100$ | 24546 | $\mathrm{C} 4-1 / 8-\mathrm{T} 0-101-\mathrm{F}$ |
| A5R48 | 0757-0280 | 3 |  | RESISTOR 1K $1 \% .125 \mathrm{~W}$ F TC $=0+-100$ | 24546 | C4-1/8-T0-1001-F |
| A5R49 | 0757-0394 | 0 | 1 | RESISTOR 51.1 $1 \%$. 125 W F TC $=0+-100$ | 24546 | C4-1/8-T0-51R1-F |
| ASTP1 | 0360-0535 | 0 |  | terminal test point pce | 00000 | ORDER BY DESCRIPTION |
| ASTP2 | 0360-0535 | 0 |  | TERMINAL TEST POINT PCB | 00000 | ORDER BY DESCRIPTION |
| A5TP3 | 0360-0535 | 0 |  | TERMINAL TEST POINT PCB | 00000 | ORDER BY DESCRIPIION |
| ASTP4 | 0360-0535 | 0 |  | TERMINAL TEST POINT PCB | 00000 | ORDER BY DESCRIPIION |
| A5TP5 | 0360-0535 | 0 |  | terminal test point pce | 00000 | ORDER BY DESCRIPTION |
| A5TP6 | 0360-0535 | 0 |  | TERMINAL TEST POINT PCB | 00000 |  |
| ASTP7 A5TP8 | 0360-0535 | 0 |  | TERMINAL TEST POINT PCB | 00000 | ORDER BY DESCRIPTION |
| ASTP8 | 0360-0535 | 0 |  | terminal test point pce | 00000 | ORDER BY DESCRIPTION |
| A5U1 | 1826-0600 | 9 | 2 | IC OP AMP LOW-EIAS-H-IMPD QUAD 14-DIP-P | 01295 | TL074ACN |
| A5U2 | 1826-0600 | 9 |  | IC OP AMP LOW-BIAS-H-IMPD QUAD 14-DIP-P | 01295 | tL074ACN |
| ASU3 | 1820-1374 | 4 | 4 | IC SWITCH ANLG QUAD 16-DIP-P PKG | 24355 | AD7510DIJN |
| A5U4 | 1820-1374 | 4 |  | IC SWITCH ANLG QUAD 16-DIP-P PKG | 24355 | AD7510DIJN |
| A5U5 | 1820-1374 | 4 |  | IC SWITCH ANLG QUAD 16-DIP-P PKG | 24355 | AD7510DIJN |
| A5U6 | 1820-1374 | 4 |  | IC SWITCH ANLG QuAd 16-DIP-P PKG | 24355 | AD7510DIJN |
| A5U7 | 1820-1962 | 6 | 1 | IC DCDR CMOS BCD-TO-DEC | 3 L 585 | CD4028BE |
| ASU8 A5U9 | $1826-0276$ $1826-0547$ | 5 |  | IC 78L05A V RGLTR TO-92 | 04713 | MC78L05ACP |
| A5U9 | 1826-0547 | 3 | 1 | IC OP AMP LOW-BIAS-H-IMPD DUAL 8-DIP-P | 01295 | TL072ACP |
| ASVR1 | 1902-0958 | 2 | 4 | DIODE-ZNR 10V $5 \%$ DO-35 $\mathrm{PD}=.4 \mathrm{~W} T \mathrm{~T}=+.075 \%$ | 28480 | 1902-0958 |
| A5VR2 | 1902-0951 | 5 | 2 | DIODE-ZNR 5.1V 5\% DO-35 PD=.4W TC=+.035\% | 28480 | 1902-0951 |
| A6 | 11729-60014 | 1 | 1 | LOW NOISE AMPLIFIER ASSEMBLY | 28480 | 11729-60014 |
| A6A1 | 11729-60009 | 4 | 1 | LOU NOISE AMPLIFIER BOARD ASSEMBLY | 28480 | 11729-60009 |
| A6A1C1 |  |  |  | NOT ASSIGNED |  |  |
| A6A1C2 | 0180-3348 | $7$ |  | CAPACITOR-FXD 100UF | 28480 | 0180-3348 |
| A6A1C3 | 0180-3384 | 1 | 1 | CAPACITOR-FXD 100UF | 28480 | $0180-3384$ |
| A6A1C4 | 0180-3345 | 4 | 1 | CAPACITOR-FXD 1500uF | 28480 | $0180-3345$ |
| A6A1C5 | 0180-3341 | 0 | 1 | CAPACITOR-FXD 330UF | 28480 | 0180-3341 |
| A6A1c6 | 0180-3383 | 0 | 1 | CAPACITOR-FXD 2700UF | 28480 | 0180-3383 |
| A6A1C7 | 0160-3875 | 3 | 2 | CAPACITOR-FXD 22PF +-5\% 200VDC CER 0+-30 | 28480 | 0160-3875 |
| A6A1C8 | 0160-3875 | 3 |  | CAPACITOR-FXD 22PF +-5\% 200VDC CER $0+-30$ | 28480 | 0160-3875 |
| A6A1C9 | 0180-3346 | 5 | 1 | CAPACITOR-FXD 680UF | 28480 | 0180-3346 |
| A6A1C10 | 0180-3228 | 2 | 1 | CAPACITOR-FXD 100UF +-20\% 10VDC AL | 28480 | 0180-3228 |
| A6A1C11 | 0180-3347 | $6$ | 1 | CAPACITOR-FXD 330UF | 28480 | 0180-3347 |
| A6A1C12 | 0160-2437 | 1 | 1 | CAPACITOR-FDTHRU 5000PF $+80-20 \% 200 \mathrm{~V}$ | 28480 | 0160-2437 |
| A6A1CR1 | 1901-0050 | 3 |  | DIODE-SWITCHING 80V 200MA 2NS DO-35 | 28480 | 1901-0050 |
| A6A1CR2 | 1901-0050 | 3 |  | DIODE-SUITCHING 80V 200MA 2NS DO-35 | 28480 | 1901-0050 |
| A6A1CR3 A6A1CR4 | 1901-0050 | 3 |  | DIODE-SUITCHING 80V 200MA 2NS DO-35 | 28480 | 1901-0050 |
| A6A1CR4 A6A1CRS | $1901-0050$ $1901-0050$ | 3 3 |  | DIODE-SWITCHING 80V 200MA 2NS DO-35 DIODE-SWITCHING 80V 200MA 2NS DO-35 | 28480 | $1901-0050$ $1901-0050$ |
| A6A1CR6 | 1901-0050 | 3 |  | DIODE-SUITCHING 80V 200MA 2NS DO-35 |  | 1901-0050 |
| A6A1CR7 | 1901-0028 | 5 | 1 | DIODE-PWR RECT 400V 750MA D0-29 | 28480 | 1901-0028 |
| A6A1DS1 | 1990-0944 | 1 | 1 | LED-RED | 28480 | 1990-0944 |
| A6A1E1 A6A1E2 | $9170-0847$ $9170-0847$ | 3 3 | 2 | CORE-SHIELDING BEAD | 02114 | 56-590-65/3B PARYLENE COATED |
| A6A1E2 A6A1E3 | $9170-0847$ $9170-0962$ | 3 3 | 1 | CORE-SHIELDING BEAD CORE-SHIELDING BEAD | 02114 28480 | 56-590-65/3B PARYLENE COATED 9170-0962 |
| A6A1J1 | 1250-1425 | 7 | 2 | CONNECTOR-RF SMC M SGL-HOLE-RR 50-OHM | 28480 | 1250-1425 |
| A6A1J2 | 1250-1425 | 7 |  | CONNECTOR-RF SMC M SGL-HOLE-RR 50-OHM | 28480 | $1250-1425$ |
| A6A1MP1 | 1205-0011 | 0 | 3 | HEAT SINK T0-5/T0-39-CS | 28480 | 1205-0011 |
| A6A1MP2 | 1205-0011 | 0 |  | HEAT SINK TO-5/T0-39-CS | 28480 | 1205-0011 |
| A6A1MP3 | 1205-0011 | 0 |  | HEAT SINK T0-5/T0-39-CS | 28480 | 1205-0011 |
| A6A1MP4 | 1205-0037 | 0 | 1 | HEAT SINK TO-18-CS | 28480 | 1205-0037 |
| A6AIMPS | 0360-0005 | 9 | 1 | TERMINAL-SLDR LUG PL-MTG FOR-\#8-SCR | 28480 | 0360-0005 |

Table 6-2. Replaceable Parts

| Reference Designation | HP Part Number | $\left\lvert\, \begin{aligned} & C \\ & D \end{aligned}\right.$ | Qty | Description | Mfr Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A6AIMP6 | 2190-0584 | 0 |  | WASHER-LK HLCL 3.0 MM 3.1-MM-ID | 28480 |  |
| A6A1MP7 | 2190-0584 | 0 |  | WASHER-LK HLCL 3.0 MM 3.1-MM-ID | 28480 | $2190-0584$ $2190-0584$ |
| A6A1MP8 | 2190-0584 | 0 |  | WASHER-LK HLCL 3.0 MM 3.1-MM-ID | 28480 | 2190-0584 |
| A6A1MP9 | 2190-0009 | 4 |  | WASHER-LK INTL T NO. 8 -168-IN-ID | 28480 | 2190-0009 |
| A6AIMP10 | 2190-0124 | 4 |  | WASHER-LK INTL T NO. $10.195-\mathrm{IN}$-ID | 28480 | $2190-0124$ |
| A6A1MP11 | 2190-0124 | 4 |  | WASHER-LK INTL T NO. $10.195-\mathrm{IN}$-ID | 28480 | 2190-0124 |
| A6A1MP12 | 2200-0139 | 4 | 5 | SCREW-MACH 4-40 .25-IN-LG PAN-HD-POZI | 28480 | 2200-0139 |
| A6A1MP13 | 2200-0139 | 4 |  | SCREL-MACH 4-40 .25-IN-LG PAN-HD-POZI | 28480 | 2200-0139 |
| A6A1MP14 | 2200-0139 | 4 |  | SCREU-MACH 4-40.25-IN-LG PAN-HD-POZI | 28480 | 2200-0139 |
| A6A1MP15 | 2580-0002 | 4 |  | NUT-HEX-DBL-CHAM 8-32-THD .085-IN-THK | 28480 | 2580-0002 |
| A6A1MP16 | 2950-0078 | 9 |  | NUT-HEX-DBL-CHAM 10-32-THD .067-IN-THK | 28480 | 2950-0078 |
| A6A1MP17 | 2950-0078 | 9 |  | NUT-HEX-DBL-CHAM 10-32-THD .067-IN-THK | 28480 | 2950-0078 |
| A6A1MP18 | 11729-20015 | 8 | 1 | COVER LOW NOISE AMPLIFIER | 28480 | 11729-20015 |
| A6A1Q1 | 1854-0597 | 2 | 6 | TRANSISTOR NPN 2 N5943 SI T0-39 PD=1w | 04713 | 2N5943 |
| A6A1Q2 | 1854-0597 | 2 |  | TRANSISTOR NPN 2N5943 SI TO-39 PD=1 ${ }^{\text {d }}$ | 04713 | 2N5943 |
| A6A103 A6A1Q4 | 1854-0597 | 2 |  | TRANSISTOR NPN 2N5943 SI TO-39 PD=1W NOT ASSIGNED | 04713 | 2N5943 |
| a6alas | 1853-0430 | 0 | 1 | TRANSISTOR PNP 2 N4959 SI $10-72$ PD $=200 \mathrm{MW}$ | 04713 | 2N4959 |
| A6A106 | 1854-0597 | 2 |  | TRANSISTOR NPN 2 N5943 SI TO-39 PD $=1 \mathrm{~W}$ | 04713 | 2N5943 |
| A6A107 | 1854-0597 | 2 |  | TRANSISTOR NPN 2N5943 SI T0-39 PD=1 ${ }^{\text {d }}$ | 04713 | 2N5943 |
| A6A108 | 1854-0597 | 2 |  | TRANSISTOR NPN 2N5943 SI T0-39 PD= 1 w | 04713 | 2N5943 |
| A6A199 | 1853-0405 | 9 | 1 | TRANSISTOR PNP SI PD $=300 \mathrm{MU}$ FT $=850 \mathrm{MHZ}$ | 04713 | 2N4209 |
| A6A1Q10 | 1853-0314 | 9 | 1 | 1RANSISTOR PNP 2N2905A SI TO-39 PD=600MU | 04713 | 2N2905A |
| A6A1R1 |  |  |  | NOT ASSIGNED |  |  |
| A6A1R2 | 0757-0280 | 3 |  | RESISTOR 1K 1\% .125U F TC=0 + - 100 | 24546 | C4-1/8-T0-1001-F |
| A6A1R3 | 0757-0441 | 8 | 1 | RESISTOR 8.25K $1 \% .125 \mathrm{~W}$ F TC $=0+-100$ | 24546 | C4-1/8-70-8251-F |
| A6A1R4 | 0757-0458 | 7 |  | RESISTOR $51.1 \mathrm{~K} 1 \% .125 \mathrm{~W}$ F TC $=0+-100$ | 24546 | $\mathrm{C} 4-1 / 8-\mathrm{TO} 0-5112-\mathrm{F}$ |
| A6A1R5 | 0698-3153 | 9 | 2 | RESISTOR 3.83K 1\% .125W F TC $=0+-100$ | 24546 | C4-1/8- ${ }^{\text {C0-3831-F }}$ |
| A6A1R6 | 0698-3150 |  |  | RESISTOR $2.37 \mathrm{~K} 1 \% .125 \mathrm{~W}$ F TC= $0+-100$ | 24546 | C4-1/8-T0-2371-F |
| A6A1R7 | 0757-0428 | $1$ | 1 | RESISTOR 1.62K 1\%.125W F TC $=0+-100$ | 24546 | C4-1/8-T0-1621-F |
| A6A1R8 | 0698-3446 | 3 | 1 | RESISTOR $3831 \%$. $125 \omega$ F TC $=0+-100$ | 24546 | C4-1/8-T0-383R-F |
| A6A1R9 | 0757-0422 | 5 | 3 | RESISTOR $9091 \% .125 \mathrm{~W}$ F TC $=0+-100$ | 24546 | C4-1/8-T0-909R-F |
| A6A1R10 | 0757-0416 | 7 | 1 | RESISTOR 511 1\% .125w F TC $=0+100$ | 24546 | C4-1/8-T0-511R-F |
| A6A1R11 | 0698-3154 | 0 |  | RESISTOR 4.22K $1 \% .125 \mathrm{~W}$ F TC $=0+-100$ | 24546 | C4-1/8-T0-4221-F |
| A6A1R12 | 0698-0085 | 0 | 1 | RESISTOR $2.61 \mathrm{~K} 1 \% .125 \mathrm{~W}$ F TC $=0+-100$ | 24546 | C4-1/8-T0-2611-F |
| A6A1R13 | 0757-0420 | 3 | 2 | RESISTOR 750 1\% .125W F TC=0 $0+100$ | 24546 | C4-1/8-70-751-F |
| A6A1R14 | 0757-0405 | 4 | , | RESISTOR 162 1\% .125 W F TC $=0+100$ | 24546 | C4-1/8-T0-162R-F |
| A6A1R15 | 0757-0401 | 0 |  | RESISTOR 100 1\% .125U F TC $=0+-100$ | 24546 | C4-1/8-T0-101-F |
|  | $0757-0420$ |  |  | RESISTOR 750 1\% .125 W F TC $=0+100$ | 24546 | C4-1/8-70-751-F |
| A6A1R17 | 0757-0814 | 9 | 1 | RESISTOR 511 1\% . 5 L F F TC $=0+-100$ | 28480 | 0757-0814 |
| A6AIR18 | 0698-3153 | 9 |  | RESISTOR 3.83K $1 \% .1254 \mathrm{~F}$ T $C=0+-100$ | 24546 | C4-1/8-T0-3831-F |
| A6A1R19 | 0757-0346 | 2 | 2 | RESISTOR $101 \% .125 \omega$ F TC $=0+-100$ | 24546 | C4-1/8-T0-10R0-F |
| A6A1R20 | 0757-0346 | 2 |  | RESISTOR $10 \quad 1 \%$. 125 W F TC $=0+-100$ | 24546 | C4-1/8-T0-10R0-F |
| A6A1R21 | 0757-1094 | 9 | 1 | RESISTOR 1.47K 1\% .125 W F TC=0+-100 | 24546 | C4-1/8-T0-1471-F |
| A6A1R22 | 0757-1002 | 9 | 2 | RESISTOR 61.9 1\% . 5 L F TC=0 +-100 | 28480 | 0757-1002 |
| A6A1R23 | 0698-8822 | 9 | 2 | RESISTOR 6.81 1\% . 125 W F TC $=0+-100$ | 28480 | 0698-8822 |
| A6A1R24 | 0698-8822 | 9 |  | RESISTOR 6.81 1\% . 125 W F TC $=0+-100$ | 28480 | 0698-8822 |
| A6A1R25 | 0757-1002 | 9 |  | RESISTOR 61.9 1\% .5W F TC=0 $0+100$ | 28480 | 0757-1002 |
| A6A1R26 | $0698-3435$ | 0 | 1 | RESISTOR 38.3 1\% . 125 W F TC $=0+-100$ | 24546 | C4-1/8-T0-38R3-F |
| A6A1R27 | 0757-0458 | 7 |  | RESISTOR $51.1 \mathrm{~K} 1 \% .125 \mathrm{~W}$ F TC $=0+-100$ | 24546 | C4-1/8-T0-5112-F |
| A6A1TP1 | 0360-0535 | 0 |  | TERMINAL TEST POINT PCB | 00000 |  |
| A6A1TP2 | 0360-0535 | 0 |  | TERMINAL TEST POINT PCB | 00000 | ORDER BY DESCRIPTION |
| A6A1TP3 | 0360-0535 | 0 |  | TERMINAL TEST POINT PCB | 00000 | ORDER BY DESCRIPTION |
| A6A1 TP4 | 0360-0535 | 0 |  | terminal test point pch | 00000 | ORDER BY DESCRIPTION |
| A6MP1 | 11729-20097 | 6 | 1 | AMPLIFIER HOUSING | $28480$ | 11729-20097 |
| A6MP2 | 0624-0077 | 5 | 6 | SCREL-TPG 4-40.312-IN-LG PAN-HD-POZI | $28480$ | 0624-0077 |
| A6MP3 | 0624-0077 | 5 |  | SCREW-TPG 4-40 .312-IN-LG PAN-HD-POZI | 28480 | 0624-0077 |
| A6MP4 | 0624-0077 | 5 |  | SCREW-TPG 4-40 .312-IN-LG PAN-HD-POZI | 28480 | $0624-0077$ |
| A6MP5 | 0624-0077 | 5 |  | SCREW-TPG 4-40 .312-IN-LG PAN-HD-POZI | 28480 | 0624-0077 |
| A6MP6 | 0624-0077 | 5 |  | SCREU-TPG 4-40 .312-IN-LG PAN-HD-POZI | 28480 | 0624-0077 |
| A6MP 7 | 0624-0077 | 5 |  | SCREW-TPG 4-40 .312-IN-LG PAN-HD-POZI | 28480 | 0624-0077 |

See introduction to this section for ordering information

Table 6-2. Replaceable Parts

| Reference Designation | HP Part Number | $\begin{aligned} & C \\ & D \end{aligned}$ | Qty | Description | Mfr Code | Mir Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A7 | 11729-60092 | 5 | 1 | POWER SUPPLY BOARD ASSEMBLY | 28480 | 11729-60092 |
| A7C1 | 0180-3285 | 7 | 1 | CAPACITOR-FXD ELEC 1200UF SOVDC | 28480 |  |
| A 7 Cl A A | $0180-3281$ $0180-3284$ | 7 | 1 | CAPACITOR-FXD 6500UF $+75-10 \% 30 \mathrm{VDC}$ AL | 28480 | 0180-3281 |
| A7C4 | $0180-3284$ $0180-3280$ | 6 | 1 | CAPACITOR-FXD CAPACITOR-FXD 1 1 | 28480 | 0180-3284 |
| A7C5 | 0160-5652 | 8 | 2 | CAPACITOR-FXD $1800 \mathrm{UF}+100-10 \%$ 30VDC AL CAPACITOR-FXD $2.2 \mathrm{~F}+-20 \%$ 50VDC CER | 28480 28480 | $0180-3280$ $0160-5652$ |
| A7C6 | 0180-2205 | 3 | 1 | CAPACITOR-FXD .33UF+-10\% 35VDC TA | 56289 | 150D334×9035A2 |
| A7C7 A7C8 | 0180-1743 | 2 | 2 | CAPACITOR-FXD. $14 \mathrm{~F}+-10 \% 35 \mathrm{VDC}$ TA | 56289 | 150D104×9035A2 |
| A7C8 | 0160-5652 | 8 1 |  | CAPACITOR-FXD $2.2 \mathrm{UF}+-20 \% 50 \mathrm{VDC}$ CER CAPACITOR-FXD $6.8 \mathrm{UF}+-10 \%$ 35VDC | 28480 | 0160-5652 |
| A7C10 | 0180-0374 | 3 | 3 | CAPACITOR-FXD CAPACITOR-FXD 1 10UF+-10\% 20 | 56289 56289 | 1500685×9035日2 1500106x9020B2 |
| ${ }^{\text {A }}$ A ${ }^{\text {A }} 111$ | 0180-0291 |  | 3 | CAPACITOR-FXD 1UF+-10\% 35VDC TA |  |  |
|  | 0180-1743 | 2 |  | CAPACITOR-FXD . 1 UF+-10\% 35VDC TA | 56289 | 150D104×9035A2 |
| A 7 C13 A 714 | $0180-0291$ $0180-0291$ | 3 3 |  | CAPACITOR-FXD 1 1UF+-10\% 35VDC TA CAPACITOR-FXD 1UF+-10\% 35VC | 56289 | 150D105X9035A2 |
| A7C15 | 0180-0423 | 3 3 3 | 2 | CAPACITOR-FXD CAPACITOR-FXD 1 100 | 56289 28480 | 1500105×9035A2 $0180-0423$ |
| ${ }_{\text {A }}{ }^{\text {A7 }} 1617$ | 0180-0491 | 5 | 1 | CAPACITOR-FXD 10UF+-20\% 25VDC TA | 28480 |  |
| A $7 \mathrm{Cl17}$ A 718 | 0160-4005 | 3 | , | CAPACITOR-FXD 1UF +-20\% 100VDC CER | 28480 | 0160-4005 |
| A A 7 C18 18 A | $0160-3876$ $0180-0423$ | 4 3 3 | 1 | CAPACITOR-FXD 47PF +-20\% 200VDC CER | 28480 | 0160-3876 |
| A 7 C 20 | 0180-2617 | 1 |  | CAPACITOR-FXD 100UF+50-10\% 25 VDC AL CAPACITOR-FXD $6.8 \mathrm{UF}+-10 \% 35 \mathrm{VDC} \mathrm{TA}$ | 28480 25088 | 0180-0423 D6R8GS1B35K |
| A 7 C21 | 0160-0576 | 5 |  | CAPACITOR-FXD . $1 \mathrm{UF}+$-20\% 50VDC CER |  |  |
| A7C22 | 0160-4387 | 4 | 1 | CAPACITOR-FXD 47PF +-5\% 200VDC CER 0+-30 | 28480 | 0160-0576 |
| A7C23 | 0180-3644 | 6 | 1 | CAPACITOR-FXD 1500UF +-20\% 10UDC THERMO | 28480 | 0180-3644 |
| A7CR1 | 1901-0159 | 3 | 17 | DIODE-PWR RECT 400V 750MA D0-41 | 28480 |  |
| A7CR2 | 1901-0159 | 3 |  | DIODE-PWR RECT 400 V 750 MA DO-41 | 28480 | 1901-0159 |
| A7CR3 A7CR4 | $1901-0159$ $1901-0159$ | 3 3 3 |  | DIODE-PWR RECT 400V 750MA DO-41 | 28480 | 1901-0159 |
| A7CR5 | $1901-0159$ $1901-0159$ | 3 3 |  | DIODE-PWR RECT 400V 750MA DO-41 | 28480 | 1901-0159 |
| AJCRS | 1901-0159 | 3 |  | DIODE-PWR RECT 400V 750MA D0-41 | 28480 | 1901-0159 |
| A7CR6 | 1901-0159 | 3 |  | DIODE-PUR RECT 400V 750MA DO-41 | 28480 | 1901-0159 |
| A7CR7 A 7 CR8 | $1901-0159$ $1901-0159$ | 3 |  | DIODE-PUR RECT 400V 750MA D0-41 | 28480 | 1901-0159 |
| A7CR9 | 1901-0159 | 3 3 3 |  | DIODE-PWR RECT 400 V 750MA DO-41 DIODE-PUR RECT 400V 750 MA DO-41 | 28480 28480 | 1901-0159 |
| A7CR10 | 1901-0159 | 3 |  | DIODE-PWR RECT 400V 750MA DO-41 | 28480 28480 | 1901-0159 |
| A 7 CR11 A 7 CR12 | 1901-0159 |  |  | DIODE-PWR RECT 400 V 750 MA DO-41 | 28480 |  |
| A 7 CR12 A A | $1901-0159$ $1901-0159$ | 3 3 3 |  | DIODE-PWR RECT 400V 750MA DO-41 | 28480 | 1901-0159 |
| A 7 CR13 A 7 CR14 | $1901-0159$ $1901-0159$ | 3 3 3 |  | DIODE-PWR RECT 400V 750MA DO-41 | 28480 | 1901-0159 |
| A7CR15 | 1901-0159 | 3 3 |  | DIODE-PLR RECT 400 V 750MA DO-41 DIODE-PUR RECT 400 V 750 MA DO-41 | 28480 | 1901-0159 |
|  |  |  |  | - Rect | 28480 | 1901-0159 |
| A7CR16 | 1901-0159 | 3 |  | DIODE-PWR RECT 400V 750MA DO-41 | 28480 | 1901-0159 |
| A7CR17 | 1901-0159 | 3 |  | DIODE-PWR RECT 400V 750MA DO-41 | 28480 | 1901-0159 |
| A7DS1 | 1990-0678 | 8 | 5 | LED-LAMP LUM-INT $=8000$ CD IF $=30 \mathrm{MA}-\mathrm{MAX}$ | 28480 | 1990-0678 |
| A 70 S2 | 1990-0678 | 8 |  | LED-LAMP LUM-INT $=800 \cup C D$ IF $=30 \mathrm{MA}-\mathrm{MAX}$ | 28480 | 1990-0678 |
| A7DS3 | 1990-0678 | 8 |  | LED-LAMP LUM-INT $=800 \cup C D$ IF $=30 \mathrm{MA}-$ MAX | 28480 | 1990-0678 |
| A7DS A | 1990-0678 | 8 |  | LED-LAMP LUM-INT $=800$ UCD IF $=30 \mathrm{MA}-\mathrm{MAX}$ | 28480 | 1990-0678 |
| A 7 DS5 | 1990-0678 | 8 |  | LED-LAMP LUM-INT $=800$ UCD IF $=30 \mathrm{MA}-\mathrm{MAX}$ | 28480 | 1990-0678 |
|  | 2110-0202 |  |  | FUSE .5A 250 V TD 1.25x. 25 UL | 75915 | 313.500 |
| A7F2 A7F3 | $2110-0002$ $2110-0055$ | 9 | 1 | FUSE 2A 250V NTD 1.25X. 25 UL | 75915 | 312002 |
| A7F4 | $2110-0055$ $2110-0012$ | 2 | 1 | FUSE 4A 250V NTD 1.25X. 25 UL | 75915 | 312004 |
| A7F4 | 2110-0012 | 1 | 2 | FUSE . 5 A 250 V NTD 1.25x. 25 UL | 28480 | 2110-0012 |
| A7J 11 A 73 | 1200-0508 | 0 |  | SOCKET-IC 14-CONT DIP-SLDR | 28480 | 1200-0508 |
| A 7 a 23 A7J | $1251-3475$ $1251-7165$ | 3 | 1 | CONNECTOR 10 -PIN M POST TYPE CONNECTOR 26 -PIN M POST TYPE | 28480 | 1251-3475 |
| A7J4 | 1251-7727 | 6 | 1 | CONNECTOR- 7 PIN | 28480 28480 | $1251-7165$ $1251-7727$ |
| A7J5 | 1250-0836 | 2 | 3 | CONNECTOR-RF SMC M PC 50-OHM | 28480 | 1250-0836 |
| A7J 6 A7J A | $1250-0836$ $1250-0836$ | 2 |  | CONNECTOR-RF SMC M PC $50-\mathrm{OHM}$ CONNECTOR-RF SMC M PC $50-0 \mathrm{HM}$ | 28480 | 1250-0836 |
| A7J8 | $1250-0836$ $1250-0835$ | 2 | 2 | CONNECTOR-RF SMC M PC $50-\mathrm{HM}$ CONNECTOR-RF SMC M PC $50-\mathrm{OHM}$ | 28480 28480 | 1250-0836 |
| A7J9 | 1250-0835 | , |  | CONNECTOR-RF SMC M PC 50-OHM | 28480 | $1250-0835$ $1250-0835$ |
| $\begin{aligned} & \text { A7L1 } \\ & \text { A } 7 \mathrm{~L} 2 \end{aligned}$ | $\begin{aligned} & 9100-1641 \\ & 9100-2<47 \end{aligned}$ | 4 | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | INDUCTOR RF-CH-MLD 240UH 5\% . 166DX.385LG INDUCTOR RF-CH-MLD 100NH 10\% .105DX.26LG | $\begin{aligned} & 28480 \\ & 28480 \end{aligned}$ | $\begin{aligned} & 9100-1641 \\ & 9100-2247 \end{aligned}$ |

Table 6-2. Replaceable Parts

| Reference Designation | HP Part Number | $\left\lvert\, \begin{aligned} & C \\ & D \end{aligned}\right.$ | Qty | Description | Mfr Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A7MP1 | 1251-4459 | 5 |  | CLIP-CABLE PLUG RTNG-DUAL INLINE 14 CONT | 28480 | 1251-4459 |
| A 7 MP 2 | 2110-0269 | 0 | 8 | FUSEHOLDER-CLIP TYPE.25D-FUSE | 28480 | 2110-0269 |
| A7MP3 | 2110-0269 | 0 |  | FUSEHOLDER-CLIP TYPE.25D-FUSE | 28480 | 2110-0269 |
| A7MP4 | 2110-0269 | 0 |  | FUSEHOLDER-CLIP TYPE. 25D-FUSE | 28480 | 2110-0269 |
| A7MPS | 2110-0269 | 0 |  | FUSEHOLDER-CLIP TYPE.25D-FUSE | 28480 | 2110-0269 |
| A7MP6 | 2110-0269 | 0 |  | FUSEHOLDER-CLIP TYPE. 25D-FUSE | 28480 | 2110-0269 |
| A7MP7 | 2110-0269 | 0 |  | FUSEHOLDER-CLIP TYPE. 25D-FUSE | 28480 | 2110-0269 |
| A7MP8 | 2110-0269 | 0 |  | FUSEHOLDER-CLIP TYPE.25D-FUSE | 28480 | 2110-0269 |
| A7MP9 | 2110-0269 | 0 |  | FUSEHOLDER-CLIP TYPE.25D-FUSE | 28480 | 2110-0269 |
| A 701 A 702 |  |  |  | NOT ASSIGNED THYRISTOR-SCR VRRM $=400$ | 3 L 585 | S2600D |
| A702 | $1884-0244$ $1884-0244$ | 9 | 3 | THYRISTOR-SCR $\quad$ VRRM $=400$ THYRISTOR-SCR VRRM $=400$ | $3 L 585$ $3 L 585$ | S26000 |
| A 704 | 1884-0244 | 9 |  | THYRISTOR-SCR VRRM $=400$ | 3L585 | S26000 |
| A 7 R1 |  |  |  | NOT ASSIGNED |  |  |
| A7R2 | 0757-0280 | 3 |  | RESISTOR 1K 1\%.125 W F TC=0+-100 | 24546 | C4-1/8-T0-1001-F |
| A7R3 | 0698-3447 | 4 |  | RESISTOR 422 1\%.1256 F TC=0+-100 | 24546 | C4-1/8-T0-422R-F |
| A7R4 | 0757-0401 | 0 |  | RESISTOR 100 1\% . 125 W F TC $=0+-100$ | 24546 | C4-1/8-T0-101-F |
| A7R5 | 0757-0288 | 1 | 1 | RESISTOR 9.09K 1\% .125W F TC=0+-100 | 19701 | MF4C1/8-T0-9091-F |
| A7R6 | 0698-3155 | 1 | 2 | RESISTOR 4.64K $1 \%$. 125U F TC $=0+-100$ | 24546 | C4-1/8-T0-4641-F |
| A7R7 | 0757-0422 | 5 |  | RESISTOR 909 1\%. 125 W F TC=0+-100 | 24546 | C4-1/8-T0-909R-F |
| A7R8 | 0698-3155 | 1 |  | RESISTOR 4.64K 1\% . 125 W F TC $=0+100$ | 24546 | C4-1/8-T0-4641-F |
| A7R9 | 0757-0403 | 2 | 1 | RESISTOR $1211 \% .125 \mathrm{~W}$ F TC $=0+-100$ | 24546 | C4-1/8-T0-121R-F |
| A7R10 | 2100-3288 | 8 | 1 | RESISTOR-TRMR $5020 \%$ C TOP-ADJ 17-TRN | 28480 | 2100-3288 |
| A7R11 | 0698-3442 | 9 | 1 | RESISTOR 237 1\% .125w F TC $=0+-100$ | 24546 | C4-1/8-T0-237R-F |
| A7R12 | 0698-3154 | 0 |  | RESISTOR 4.22K 1\%.125W F TC $=0+100$ | 24546 | C4-1/8-T0-4221-F |
| A7R13 | 0698-3445 | 2 | 1 | RESISTOR 348 1\% . 125 W F TC $=0+-100$ | 24546 | C4-1/8-T0-348R-F |
| A7R14 | 0757-0401 | 0 |  | RESISTOR 100 1\% .125U F TC $=0+-100$ | 24546 | C4-1/8-T0-101-F |
| A7R15 | 0757-0280 | 3 |  | RESISTOR 1K 1\%.125 F F TC $=0+-100$ | 24546 | C4-1/8-T0-1001-F |
| A7R16 | 0757-0401 | 0 |  | RESISTOR 100 1\% . 125 W F TC $=0+-100$ | 24546 | C4-1/8-T0-101-F |
| A 7 R17 | 0757-0280 | 3 |  | RESISTOR 1K 1\%. 125 W F TC $=0+-100$ | 24546 | C4-1/8-T0-1001-F |
| A7R18 | 0698-3443 | 0 | 1 | RESISTOR 287 1\% .125W F TC $=0+-100$ | 24546 | C4-1/8-T0-287R-F |
| A7R19 | 0698-3447 | 4 |  | RESISTOR 422 1\% . 125 W F TC $=0+-100$ | 24546 | C4-1/8-T0-422R-F |
| A7R20 | 0698-3447 | 4 |  | RESISTOR 422 1\% .125W F TC $=0+-100$ | 24546 | C4-1/8-T0-422R-F |
| A7R21 | 0698-3447 | 4 |  | RESISTOR 422 1\% .125w F TC=0 +-100 | 24546 | C4-1/8-T0-422R-F |
| A7R22 | 0757-0280 | 3 |  | RESISTOR $1 \mathrm{~K} 1 \% .125 \mathrm{~W}$ F TC $=0+-100$ | 24546 | C4-1/8-T0-1001-F |
| A 7 R23 | 0757-0280 | 3 |  | RESISTOR $1 \mathrm{~K} 1 \%$. 125 W F TC $=0+-100$ | 24546 | C4-1/8-T0-1001-F |
| A 7 R24 | 0757-0280 | 3 |  | RESISTOR $1 \mathrm{~K} 1 \% .125 \mathrm{~W}$ F TC $=0+-100$ | 24546 | C4-1/8-T0-1001-F |
| A 7825 | 0757-0280 | 3 |  | RESISTOR 1K 1\% .125 W F TC=0+-100 | 24546 | C4-1/8-T0-1001-F |
| A7R26 | 0698-3390 | 6 | 2 | RESISTOR 19.6 1\% . 5 W F TC $=0+-100$ | 28480 | 0698-3390 |
| A7R27 | 8159-0005 | 0 |  | RESISTOR-ZERO OHMS 22 All LEAD DIA | 28480 | 8159-0005 |
| A 7 R28 | 0698-3390 | 6 |  | RESISTOR 19.6 1\%. 5 Ll F TC=0+-100 | 28480 | 0698-3390 |
| A7R29 | 8159-0005 | 0 |  | RESISTOR-ZERO OHMS 22 AWG LEAD DIA | 28480 | 8159-0005 |
| A7R31 | 0698-3447 | 4 |  | RESISTOR 422 1\% .125W F TC=0+-100 | 24546 | C4-1/8-T0-422R-F |
| A7R32 | 0698-6360 |  | 1 | RESISTOR 10K . $1 \%$. 125 W F TC $=0+-25$ | 28480 | 0698-6360 |
| A7R33 | 0698-3156 | 2 | 1 | RESISTOR 14.7K $1 \% .125 \mathrm{~W}$ F TC $=0+100$ | 24546 | C4-1/8-T0-1472-F |
| A7R34 | 0757-0280 | 3 |  | RESISTOR 1K 1\%. 125 W F TC $=0+-100$ | 24546 | C4-1/8-T0-1001-F |
| A7R35 | 0757-0422 | 5 |  | RESISTOR $9091 \% .125 \mathrm{~W}$ F TC $=0+100$ | 24546 | C4-1/8-T0-909R-F |
| A7R36 | 0757-0280 | 3 |  | RESISTOR 1K 1\% . 125 W F TC=0+-100 | 24546 | C4-1/8-T0-1001-F |
| A7TP1 | 0360-0535 | 0 |  | TERMINAL TEST POINT PCB | 00000 | ORDER BY DESCRIPTION |
| A7TP2 | 0360-0535 | 0 |  | TERMINAL TEST POINT PCB | 00000 | ORDER BY DESCRIPTION |
| A7TP3 | 0360-0535 | 0 |  | TERMINAL TEST POINT PCB | 00000 | ORDER BY DESCRIPTION |
| A7TP4 | 0360-0535 | 0 |  | TERMINAL TEST POINT PCB | 00000 | ORDER BY DESCRIPTION |
| A7TP5 | 0360-0535 | 0 |  | TERMINAL TEST POINT PCB | 00000 | ORDER BY DESCRIPTION |
| A7TP6 | 0360-0535 | 0 |  | TERMINAL TEST POINT PCB | 00000 | ORDER BY DESCRIPTION |
| A7U1- <br> A7U4 <br> A7U5 |  | 9 |  | NOT ASSIGNED IC OP AMP LOW-NOISE 8-DIP-C PKG |  |  |
| A7U5 | 1826-0783 | 9 | 1 | IC OP AMP LOW-NOISE 8-DIP-C PKG | 52063 | XR5534ACN |
| A7VR1 | 1902-0969 |  | 1 | DIODE-ZNR 30V 5\% DO-35 PD=.4W TC $=+.095 \%$ | 28480 | 1902-0969 |
| A7VR2 | 1902-0644 | 3 | 1 | DIODE-ZNR 1 N5363B 30V 5\% PD $=5 \mathrm{~W}$ TC $\mathrm{T}=+29 \mathrm{MV}$ | 28480 | 1902-0644 |
| A7VR3 | 1902-0963 | 9 | 1 | DIDDE-ZNR 16V 5\% DO-35 PD=.44 TC=+.088\% | 28480 | 1902-0963 |
| A7VR4 | 1302-0951 | 5 |  | DIODE-ZNR 5.1V $5 \%$ DO-35 PD=.4W TC=+.035\% | 28480 | 1902-0951 |
| A7VR5 | 1902-1340 | 8 | 1 | DIODE-ZNR 1 N5355B 18V 5\% PD=5W IR $=500 \mathrm{NA}$ | 04713 | 1 N5355B |

See introduction to this section for ordering information

Table 6-2. Replaceable Parts

| Reference Designation | HP Part Number | C | Qty | Description | Mfr Code | - Mir Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A7VR6 | 1902-0965 | 1 | 1 | DIODE-ZNR 20V 5\% DO-35 PD=.4W TC=+.092\% |  |  |
| A7VR7 | 1902-0958 | 2 |  | DIODE-2NR 10V 5\% DO-35 PD =.4W TC $=+.075 \%$ | 28480 28480 | $\begin{aligned} & 1902-0965 \\ & 1902-0958 \end{aligned}$ |
| A7VR8 | 1902-0958 | 2 |  | DIODE-ZNR 10V 5\% DO-35 PD=.4W TC=+.075\% | 28480 | 1902-0958 |
| A7VR9 A7VR10 | $1902-0958$ $1902-0630$ | 2 |  | DIODE-ZNR $10 \mathrm{~V} 5 \%$ D0-35 $\mathrm{PD}=.4 \mathrm{~W} \quad \mathrm{TC}=+.075 \%$ DIODE-ZNR 1 N5 | 28480 | 1902-0958 |
| ATVR10 | 1902-0630 | 7 | 1 | DIODE-ZNR 1N5236日 7.5V 5\% D0-7 PD=.5U | 04713 | 1 N 5236 B |
| A7XA5 | 1251-1365 | 6 | 1 | CONNECTOR-PC EDGE 22-CONT/ROW 2-ROWS | 28480 | 1251-1365 |
| A8 | 11729-60012 | 9 | 1 | HP-IE INTERCONNECT BOARD ASSEMBLY | 28480 | 11729-60012 |
| A8J1 A8J2 | 1251-5615 | 7 | 2 | CONNECTOR 34-PIN M POST TYPE | 28480 | 1251-5615 |
| A8JJ3 | $1251-3283$ $1200-0508$ | 1 | 1 | CONNECTOR 24-PIN F MICRORIBBON | 28480 | 1251-3283 |
|  | 1200-0508 | 0 |  | SOCKET-IC 14-CONT DIP-SLDR | 28480 | 1200-0508 |
| A8MP1 | 0380-0643 | 3 | 2 | STANDOFF-HEX .255-IN-LG 6-32THD | 00000 | ORDER BY DESCRIPTION |
| A8MP2 | 0380-0643 | 3 |  | STANDOFF-HEX . 255 -IN-LG 6-32THD | 00000 | ORDER BY DESCRIPTION |
| A8MP3 | 0515-0054 | 7 |  | SCREW-MACH M3 $\times 0.510 \mathrm{MM}$-LG PAN-HD | 28480 | 0515-0054 |
| A8MP4 | 0515-0054 | 7 |  | SCREL-MACH M3 $\times 0.510 \mathrm{MM}$-LG PAN-HD | 28480 | 0515-0054 |
| A8MP5 | 0535-0004 | 9 |  | NUT-HEX DBL-CHAM M3 $\times 0.5$ 2.4MM-THK | 00000 | ORDER BY DESCRIPTION |
| A8MP6 | 0535-0004 | 9 |  | NUT-HEX DBL-CHAM $13 \times 0.5$ 2.4MM-THK | 00000 |  |
| A8MP7 | 1251-4459 | 5 |  | CLIP-CABLE PLUG RTNG-DUAL INLINE 14 CONT | 28480 | $1251-4459$ |
| A8MP8 A8MP9 | $1530-1098$ $1530-1098$ | 4 | 2 | CLEVIS 0.070-IN WSLT: $0.454-$ IN PIN CTR | 00000 | ORDER BY DESCRIPIION |
| A8MP9 A8MP10 | $1530-1098$ $2190-0017$ | 4 |  | CLEVIS 0.070-IN W SLT: 0.454 -IN PIN CTR | 00000 | ORDER BY DESCRIPIION |
|  | 2190-0017 | 4 |  | WASHER-LK HLCL NO. 8 .168-IN-ID | 28480 | 2190-0017 |
| A8MP 11 | 2190-0017 | 4 |  | WASHER-LK HLCL NO. 8 .168-IN-ID | 28480 | 2190-0017 |
| A8MP12 | 2190-0019 | 6 | 2 | WASHER-LK HLCL NO. 4.115-IN-ID | 28480 | 2190-0019 |
| A8MP13 | 2190-0019 | 6 |  | WASHER-LK HLCL NO. 4 .115-IN-ID | 28480 | 2190-0019 |
| A9 | 11729-60109 | 5 | 1 | MICROPROCESSOR BOARD ASSEMBLY | 28480 | 11729-60109 |
| A9C1 | 0180-2207 |  | 1 | CAPACITOR-FXD 100UF+-10\% 10VDC TA | 56289 | 150D107X9010R2 |
| A9C2 | 0180-2620 | 6 | 4 | CAPACITOR-FXD 2.2UF+-10\% 50VDC TA | 25088 | D2R2GS1B50K |
| A9C3 | $0180-2620$ $0160-4835$ | 6 |  | CAPACITOR-FXD $2.2 \mathrm{UF}+-10 \%$ 50VDC TA | 25088 | D2R2GS1B50K |
| A9C4 A9C5 | 0160-4835 | 7 | 28 | CAPACITOR-FXD . 1UF +-10\% 50VDC CER | 28480 | 0160-4835 |
| A9C5 | 0160-4835 | 7 |  | CAPACITOR-FXD. $1 \mathrm{UF}+-10 \%$ SOVDC CER | 28480 | 0160-4835 |
| A9C6 | 0160-4835 | 7 |  | CAPACITOR-FXD . $1 \mathrm{UF}+\mathrm{-10} \mathrm{\%}$ SOVDC CER | 28480 | 0160-4835 |
| A9C7 | 0160-4835 | 7 |  | CAPACITOR-FXD. $14 \mathrm{~F}+-10 \% 50 \mathrm{VDC}$ CER | 28480 | 0160-4835 |
| A9C8 | 0160-4835 | 7 |  | CAPACITOR-FXD. $1 \mathrm{UF}+-10 \%$ SOVDC CER | 28480 | 0160-4835 |
| A9C9 | 0160-4835 | 7 |  | CAPACITOR-FXD. $1 \mathrm{UF}+$ +-10\% 50VDC CER | 28480 | 0160-4835 |
| A9C10 | 0180-0374 | 3 |  | CAPACITOR-FXD 10UF+-10\% 20VDC TA | 56289 | 150D106×902082 |
| A9C11 |  |  |  | CAPACITOR-FXD 10UF+-10\% 20VDC TA |  |  |
| ${ }_{\text {AsC12 }}$ | 0160-0127 | $2$ | 1 | CAPACITOR-FXD 1UF +-20\% 25VDC CER | 56289 28480 | $\begin{aligned} & 1500106 \times 9020 \mathrm{~B} 2 \\ & 0160-0127 \end{aligned}$ |
| ${ }_{\text {A A Cl }}$ | 0160-4835 | 7 |  | CAPACITOR-FXD. 1UF +-10\% 50VDC CER | 28480 | 0160-4835 |
| A9C14 A9C15 | 0160-4835 | 7 |  | CAPACITOR-FXD . 1UF +-10\% 50VDC CER | 28480 | 0160-4835 |
| A9C15 | 0160-4835 | 7 |  | CAPACITOR-FXD . 1UF +-10\% 50VDC CER | 28480 | 0160-4835 |
| A9C16 | 0160-4835 | 7 |  | CAPACITOR-FXD . $1 \mathrm{UF}+-10 \%$ 50VDC CER |  |  |
| A9C17 | 0160-4835 | 7 |  | CAPACITOR-FXD. $14 \mathrm{~F}+-10 \%$ S0VDC CER | 28480 | $0160-4835$ |
| A9C18 | 0160-4835 | 7 |  | CAPACITOR-FXD. 1UF +-10\% 50VDC CER | 28480 | 0160-4835 |
| A9C19 | 0160-4835 | 7 |  | CAPACITOR-FXD . 1UF +-10\% 50VDC CER | 28480 | 0160-4835 |
| A9C20 | 0160-4835 | 7 |  | CAPACITOR-FXD. 1UF +-10\% 50VDC CER | 28480 | 0160-4835 |
| A9C21 | 0180-1745 | 4 | 1 | CAPACITTR-FXD 1.5UF+-10\% 20VDC TA | 56289 | 150D155X9020A2 |
| A9C22 | 0180-0116 | 1 |  | CAPACITOR-FXD 6.8UF+-10\% 35VDC TA | 56289 | $1500685 \times 9035 \mathrm{~B} 2$ |
| A9C23 | 0160-4835 | 7 |  | CAPACITOR-FXD . 1 UF +-10\% 50VDC CER | 28480 | 0160-4835 |
| A9C24 | 0160-4835 | 7 |  | CAPACITOR-FXD . IUF +-10\% 50VDC CER | 28480 | 0160-4835 |
| A9C25 | 0160-4835 | 7 |  | CAPACITOR-FXD. 1UF +-10\% 50VDC CER | 28480 | 0160-4835 |
|  | 0160-4835 | 7 |  | CAPACITOR-FXD . IUF +-10\% 50VDC CER | 28480 | 0160-4835 |
| A9C27 | 0160-4835 | 7 |  | CAPACITOR-FXD. IUF +-10\% 50VDC CER | 28480 | 0160-4835 |
| $\begin{aligned} & \text { A9C28 } \\ & \text { AOCP } \end{aligned}$ | 0160-4835 | $7$ |  | CAPACITOR-FXD. 1 IVF +-10\% 50VDC CER | 28480 | 0160-4835 |
| A9C29 A9C30 | $0160-4835$ $0160-4835$ | 7 |  | CAPACITOR-FXD. 1 UF +-10\% 50VDC CER | 28480 | 0160-4835 |
| А9С30 | 0160-4835 | 7 |  | CAPACITOR-FXD. IUF +-10\% 50VDC CER | 28480 | 0160-4835 |
| ASC31 A9C32 | $0160-4835$ | 7 |  | CAPACITOR-FXD . IUF +-10\% SOVDC CER | 28480 | 0160-4835 |
| A99C32 A9C33 | $0160-4835$ $0160-4835$ | 7 |  | CAPACITOR-FXD . 1UF +-10\% 50VDC CER | 28480 | 0160-4835 |
| A9C34 | 0160-4835 | 7 |  | CAPACIIOR-FXD . 1 UF +-10\% 50VDC CER CAPACITOR-FXD . $1 \mathrm{UF}+10 \%$ 50VDC CER | 28480 | 0160-4835 |
| A9C35 | 0160-4835 | 7 |  | CAPACITOR-FXD. .1UF +-10\% 50VDC CER | 28480 | -160-4835 |

Table 6-2. Replaceable Parts

| Reference Designation | HP Part Number | $\begin{aligned} & \mathrm{C} \\ & \mathrm{D} \end{aligned}$ | Qty | Description | $\begin{aligned} & \text { Mfr } \\ & \text { Code } \end{aligned}$ | Mir Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A9C36 | 0160-4835 | 7 |  | CAPACITOR-FXD . $1 \mathrm{UF}+$ +10\% SOVDC CER | 28480 | 0160-4835 |
| A9C37 | 0180-2620 | 6 |  | CAPACITOR-FXD 2.2UF+-10\% 50VDC TA | 25088 | D2R2GS1B50K |
| A9C38 | 0180-2620 | 6 |  | CAPACITOR-FXD 2.2UF+-10\% 50VDC TA | 25088 | D2R2GS1B50K |
| A9C39 | 0160-0571 | 0 |  | CAPACITOR-FXD 470PF +-20\% 100VDC CER | 28480 | 0160-0571 |
| A9C40 | 0180-0116 | 1 |  | CAPACITOR-FXD 6.8UF+-10\% 35VDC TA | 56289 | 1500685×9035B2 |
| A9CR1 | 1901-0376 | 6 | 1 | DIODE-GEN PRP 35V 50MA D0-35 | 28480 | 1901-0376 |
| AgDS 1 | 1990-0933 | 8 | 2 | LED-LAMP RED | 28480 | 1990-0933 |
| A9DS2 | 1990-0933 | 8 |  | LED-LAMP RED | 28480 | 1990-0933 |
| A9J1 | 1251-5615 | 7 |  | CONNECTOR 34-PIN M POST TYPE | 28480 | 1251-5615 |
| A9J2 | 1251-7335 | 2 | 1 | CONNECTOR | 28480 | 1251-7335 |
| A9J3 | 1251-8967 | 8 | 1 | CONN-POST TYPE . 100-PIN-SPCG 29-CONT | 28480 | 1251-8967 |
| A9J4 | 1251-4428 | 8 | 1 | CONNECTOR 50-PIN M POST TYPE | 28480 | 1251-4428 |
| A9L1 | 9100-1626 | 1 |  | INDUCTOR RF-CH-MLD 36UH 5\% . 166DX.385LG | 28480 | 9100-1626 |
| A9MP1 | 0361-0009 | 5 | 3 | RIVET-SEMITU日 OVH . 123 DIA .188LG | 00000 | ORDER BY DESCRIPIION |
| A9MP2 | 0361-0009 | 5 |  | RIVET-SEMITUB OVH . 123 DIA .188LG | 00000 | ORDER BY DESCRIPTION |
| A9MP3 | 0361-0009 | 5 |  | RIVET-SEMITUB OVH . 123 DIA .188LG | 00000 | ORDER BY DESCRIPTION |
| A9MP4 | 5040-1497 | 2 | 3 | HINGE-MOLDED | 28480 | 5040-1497 |
| A9MP5 | 5040-1497 | 2 |  | HINGE-MOLDED | 28480 | 5040-1497 |
| A9MP6 | 5040-1497 | 2 |  | HINGE-MOLDED | 28480 | 5040-1497 |
| A9MP7 | 0340-0944 | 3 | 1 | INSULATOR-IC NYLON BLACK | 28480 | 0340-0944 |
| A9R1 | 1810-0279 | 5 | 6 | NETWORK-RES 10-SIP4.7K OHM $\times 9$ | 01121 | 2104472 |
| A9R2 | 1810-0279 | 5 |  | NETWORK-RES 10-SIP4.7K OHM X 9 | 01121 | 2104472 |
| A9R3 | 0698-0084 | 9 | 1 | RESISTOR 2.15K 1\% .125W F TC $=0+-100$ | 24546 | C4-1/8-T0-2151-F |
| A9R4 | 1810-0279 | 5 |  | NETWORK-RES 10-SIP4.7K OHM $\times 9$ | 01121 | 2104472 |
| A9R5 | 0757-0280 | 3 |  | RESISTOR 1 K 1\% . 125 W F $\mathrm{TC}=0+-100$ | 24546 | C4-1/8-T0-1001-F |
| A9R6 | 1810-0279 | 5 |  | NETWORK-RES 10-SIP4.7K OHM $\times 9$ | 01121 | 2104472 |
| A9R7 | 0757-0199 | 3 | 2 | RESISTOR 21.5K 1\% .125w F TC $=0+-100$ | 24546 | C4-1/8-70-2152-F |
| A9R8 | 0757-0199 | 3 |  | RESISTOR 21.5K 1\% . 125 W F TC $=0+-100$ | 24546 | C4-1/8-T0-2152-F |
| A9R9 | 0757-0464 | 5 | 2 | RESISTOR 90.9K $1 \% .125 \mathrm{~W}$ F TC $=0+-100$ | 24546 | C4-1/8-70-9092-F |
| A9R10 | 0757-0464 | 5 |  | RESISTOR 90.9K 1\% . 125 W F TC $=0+-100$ | 24546 | C4-1/8-T0-9092-F |
| A9R11 | 1810-0279 | 5 |  | NETWORK-RES 10-SIP4.7K OHM $\times 9$ | 01121 | 2104472 |
| A9R12 | 1810-0279 | 5 |  | NETWORK-RES 10-SIP4.7K OHM $\times 9$ | 01121 | 2104472 |
| A9R13 | 1810-0273 | 9 | 1 | NETWORK-RES 10-SIP470.0 OHM X 9 | 01121 | 2104471 |
| A9R14 | 0757-0442 | 9 |  | RESISTOR 10K 1\% .125w F TC=0+-100 | 24546 | C4-1/8-70-1002-F |
| ASR15 | 1810-0269 | 3 | 1 | NETWORK-RES 9 -SIP 10.0 K OHM $\times 8$. | 28480 | 1810-0269 |
| A9R16 | $0757-0290$ | 5 | 1 | RESISTOR 6.19K 1\% .125W F TC=0+-100 | $19701$ | MF4C1/8-TO-6191-F |
| A9R17 | 0757-0401 | 0 |  | RESISTOR 100 1\% . 125 W F TC=0+-100 | $24546$ | $\mathrm{C} 4-1 / 8-\mathrm{TO}-101-\mathrm{F}$ |
| A9S1 | 3101-2126 | 4 | , | SWITCH-SL 5-SPDT DIP-SLIDE-ASSY . 1 A | 28480 | 3101-2126 |
| A9S2 | 3101-2172 | 0 | 1 | SWITCH-TGL DIP-RKR-ASSY SPDT .05A 30VDC | 28480 | 3101-2172 |
| A9TP1 | 0360-0535 | 0 |  | TERMINAL TEST POINT PCB | 00000 | ORDER EY DESCRIPIION |
| A9TP2 | 0360-0535 | 0 |  | TERMINAL TEST POINT PCB | 00000 | ORDER BY DESCRIPTION |
| A9TP3 | 0360-0535 | 0 |  | TERMINAL TEST POINT PCB | 00000 | ORDER BY DESCRIPTION |
| A9TP4 | 0360-0535 | 0 |  | TERMINAL TEST POINT PCB | 00000 | ORDER BY DESCRIPTION |
| A9TP5 | 0360-0535 | 0 |  | TERMINAL TEST POINT PCB | 00000 | ORDER BY DESCRIPTION |
| A9TP6 | 0360-0535 | 0 |  | TERMINAL TEST POINT PCB | 00000 | ORDER BY DESCRIPTION |
| ASTP7 | 0360-0535 | 0 |  | TERMINAL TEST POINT PCB | 00000 | ORDER BY DESCRIPTION |
| A9U1 | 1820-1212 | 9 | 1 | IC FF TTL LS J-K NEG-EDGE-TRIG | 01295 | SN74LS112AN |
| A9U2 | 1820-2549 | 7 | 1 | IC-8291A P HPIB | 28480 | 1820-2549 |
| A9U3 | 1818-1768 | 5 | 1 | IC, CMOS 16384 (16K) STAT RAM 150-NS 3-S | S0545 | UPD446C-1 (PER HP DUG) |
| ASU4 | 11729-80010 | 9 | 1 | EPROM | 28480 | 11729-80010 |
| A9U5 | 1820-2624 | 9 | 1 | IC-MPU; CLK FREQ=2MHZ, ENHANCED 6800 | 28480 | 1820-2624 |
| A9U6 | 1820-2081 | 2 | 1 | IC NMOS | 04713 | MC68A21P |
| A9U7 | 1820-1199 | 1 | 3 | IC INV TTL LS HEX 1-INP | 01295 | SN74LS04N |
| A9U8 | 1820-1216 | 3 | 3 | IC DCDR TTL LS 3-TO-8-LINE 3-INP | 01295 | SN74LS138N |
| A949 | 1820-1216 | 3 |  | IC DCDR TTL LS 3-T0-8-LINE 3-INP | 01295 | SN74LS138N |
| A9U10 | 1820-1216 | 3 |  | IC DCDR TTL LS 3-T0-8-LINE 3-INP | 01295 | SN74LS138N |
| A9U11 | 1820-1423 | 4 | 1 | IC MV TTL LS MONOSTEL RETRIG DUAL | 01295 | SN74LS123N |
| A Sul $^{2} 2$ | 1826-0138 | 8 | 1 | IC COMPARATOR GP QUAD 14-DIP-P PKG | 01295 | LM339N |
| APU13 | 1820-1730 | 6 | 2 | IC FF TTL LS D-TYPE POS-EDGE-TRIG COM | 01295 | SN74LS273N |
| A9U14 | 1820-1730 | 6 |  | IC FF TTL LS D-TYPE POS-EDGE-TRIG COM | 01295 | SN74LS273N |
| ASU15 | 1826-0175 | 3 | 1 | IC COMPARATOR GP DUAL 14-DIP-P PKG | 27014 | LM319N |

See introduction to this section for ordering information

Table 6-2. Replaceable Parts

| Reference Designation | HP Part Number | $\begin{aligned} & C \\ & D \end{aligned}$ | Qty | Description | Mfr Code | Mir Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A9U16 | 11729-80002 | 9 | 1 | PAL-ADRS. DECODER |  |  |
| A9U17 | 1820-1197 | 9 | 2 | IC GATE TTL LS NAND QUAD 2-INP | 28480 01295 | 11729-80002 SN74LS00N |
| A9U18 | 1820-2024 | 3 | 5 | IC DRVR TTL LS LINE DRVR OCTL | 01295 | SN74LS244N |
| A9U19 | 1820-2973 | 1 |  | IC DRVR TTL PRPHL HV DUAL | 28480 | 1820-2973 |
| A9U2O | 1820-2973 | 1 |  | IC DRVR TTL PRPHL HV DUAL | 28480 | 1820-2973 |
| A9U21 | 1820-2973 | 1 |  | IC DRVR TTL PRPHL HV DUAL | 28480 | 1820-2973 |
| Agu22 | 1820-2973 | 1 |  | IC DRVR TTL PRPHL HV DUAL | 28480 | 1820-2973 |
| A9U23 | 1820-1199 | 1 |  | IC INV TTL LS HEX 1-INP | 01295 | SN74LS04N |
| A9U24 | 1820-2024 | 3 |  | IC DRVR TTL LS LINE DRVR OCTL | 01295 | SN74LS244N |
| A9U25 | 1820-1858 | 9 | 3 | IC FF TTL LS D-TYPE OCTL | 01295 | SN74LS377N |
| A9U26 | 1820-1858 | 9 |  | IC FF TTL LS D-TYPE OCTL | 01295 | SN74LS377N |
| A9U27 | 1820-1858 | 9 |  | IC FF TTL LS D-TYPE OCTL | 01295 | SN74LS377N |
| Asu28 | $1820-2024$ $1820-2973$ | 3 |  | IC DRVR TTL LS LINE DRVR OCTL | 01295 | SN74LS244N |
| A9429 A9U30 | $1820-2973$ $1820-2973$ | 1 |  | IC DRVR TTL PRPHL HV DUAL | 28480 | 1820-2973 |
| A9U30 | 1820-2973 | 1 |  | IC DRVR TTL PRPHL HV DUAL | 28480 | 1820-2973 |
| A9U31 | 1820-2973 | 1 |  | IC DRVR TTL PRPHL HV DUAL | 28480 | 1820-2973 |
| A9432 | 1820-2024 | 3 |  | IC DRVR TTL LS LINE DRVR OCTL | 01295 | SN74LS244N |
| A9U33 | 1820-3513 | 7 | 1 | IC TRANSCEIVER TTL S INSTR-BUS IEEE-488 | 28480 | 1820-3513 |
| A9U34 | 1820-3431 | 8 | 1 | IC TRANSCEIVER TIL S INSTR-BUS IEEE-483 | 28480 | 1820-3431 |
| A9U35 | 1820-2024 | 3 |  | IC DRVR TTL LS LINE DRVR OCTL | 01295 | SN74LS244N |
| A9436 | 1820-2075 |  | 3 | IC TRANSCEIVER TTL LS BuS Octl | 28480 | 1820-2075 |
| A9437 | 1820-2075 | 4 |  | IC TRANSCEIVER TTL LS BUS OCTL | 28480 | 1820-2075 |
| A9438 | 1820-2075 | 4 |  | IC TRANSCEIVER TTL LS BUS OCTL | 28480 | 1820-2075 |
| A9U39 A9U40 | $1820-1197$ $1820-111$ | 9 |  | IC GATE TTL LS NAND QUAD 2-INP | 01295 | SN74LS00N |
| A9U40 | 1820-1112 | 8 | 1 | IC FF TTL LS D-TYPE POS-EDGE-TRIG | 01295 | SN74LS74AN |
| A9U41 | 1820-2973 | 1 |  | IC DRVR TTL PRPHL HV DUAL | 28480 | 1820-2973 |
| A9U42 | 1820-2973 | 1 |  | IC DRVR TTL PRPHL HV DUAL | 28480 | 1820-2973 |
| A9U43 | 1820-2973 | 1 |  | IC DRVR TTL PRPHL HV DUAL | 28480 | 1820-2973 |
| A9U44 | 1820-1199 | 1 |  | IC INV TTL LS HEX 1-INP | 01295 | SN74LS04N |
| A9U45 | 1820-1851 | 2 | 2 | IC ENCDR TTL LS | 01295 | SN74LS148N |
| A9U46 |  |  |  | IC ENCDR TTL LS | 01295 |  |
| A9447 | 1820-1587 | 1 | 4 | IC DRVR TTL LED DRVR HEX 1-INP | 27014 | DM8859N |
| A9U48 A9U49 | 1820-1587 | 1 |  | IC DRVR TTL LED DRVR HEX 1 -INP | 27014 | DM8859N |
| A9Y49 A9U50 | 1820-1587 | 1 |  | IC DRVR TTL LED DRVR HEX 1 -INP | 27014 | DM8859N |
| A9U50 | 1820-1587 | 1 |  | IC DRVR TTL LED DRVR HEX 1-INP | 27014 | DM8859N |
| A9U51 | 1820-0668 | 7 |  | IC BFR TTL NON-INV HEX 1 -INP | 01295 | SN7407N |
| A9U52 | 1820-1470 | 1 | 1 | IC MUXR/DATA-SEL TTL LS 2-TO-1-LINE QUAD | 01295 | SN74LS157N |
| A9U53 | $1820-1445$ $1820-2973$ |  | 1 | IC LCH TTL LS 4 -日IT | 01295 | SN74LS375N |
| A9U54 A9U55 | $1820-2973$ $1820-2973$ | 1 |  | IC DRVR TTL PRPHL HV DUAL | 28480 | 1820-2973 |
| A9U55 | 1820-2973 | 1 |  | IC DRVR TTL PRPHL HV DUAL | 28480 | 1820-2973 |
| A9456 | 1820-2973 | 1 |  | IC DRVR TTL PRPHL HV DUAL | 28480 | 1820-2973 |
| A9U57 | 1820-2973 | 1 |  | IC DRVR TTL PRPHL HV DUAL | 28480 | 1820-2973 |
| A9xu4 | 1200-0567 |  | 1 | SOCKET-IC 28-CONT DIP DIP-SLDR | 28480 | 1200-0567 |
| A9xU5 | 1200-0654 | 7 | 1 | SOCKET-IC 40-CONT DIP DIP-SLDR | 28480 | 1200-0654 |
| A9Y1 | 1813-0130 | 3 | 1 | XTAL-CLOCK-OSCILLATOR $16-\mathrm{MHZ}$ 0.05\% TTL | 28480 | 1813-0130 |
| A10 | 11729-60086 | 7 | 1 | IF AMPLIFIER ASSEMBLY | 28480 | 11729-60086 |
| A10FL1 | 9135-0174 | 5 |  | FILTER-LOW PASS LEADS-TERMS | 28480 | 9135-0174 |
| A10J1 A10J2 | $1250-1887$ | $5$ | 2 | SMA FEMALE CONNECTOR | 28480 | 1250-1887 |
| A10J2 | 1250-1887 | 5 |  | SMA FEMALE CONNECTOR | 28480 | 1250-1887 |
| A10MP1 | 0515-0104 | 8 | 37 | SCREW-MACH M3 $\times 0.5$ 8MM-LG PAN-HD | 28480 | 0515-0104 |
| A10MP2 | 0515-0104 | 8 |  | SCREW-MACH M3 $\times 0.5$ 8MM-LG PAN-HD | 28480 | 0515-0104 |
| A10MP3 A10MP4 | 0515-0104 | 8 |  | SCREL-MACH M3 $\times 0.58 \mathrm{MM}-\mathrm{LG}$ PAN-HD | 28480 | 0515-0104 |
| Al0MP4 Al0MPS | 0515-0104 | 8 |  | SCREW-MACH M3 $\times 0.5$ 8MM-LG PAN-HD | 28480 | 0515-0104 |
| Alomps | 0515-0104 | 8 |  | SCREW-MACH M3 $\times 0.5$ 8MM-LG PAN-HD | 28480 | 0515-0104 |
|  | 0515-0104 | 8 |  | SCREL-MACH M3 $\times 0.5$ 8MM-LG PAN-HD |  |  |
| Al0MP7 <br> A10MP8 | 0515-0104 | 8 |  | SCREW-MACH M3 $\times 0.58$ 8MM-LG PAN-HD | $28480$ | $0515-0104$ |
| A10MP8 | $0515-0104$ $0515-0207$ | 8 |  | SCREW-MACH M3 $\times 0.58$ 8MM-LG PAN-HD | 28480 | 0515-0104 |
| A10MP9 Al0MP10 | 0515-0207 $0515-0207$ | 2 | 10 | SCREW-MACH M2 $\times 0.4$ 6MM-LG PAN-HD SCREW-MACH | 28480 | 0515-0207 |
| Alomplo | 0515-0207 | 2 |  | SCREW-MACH M2 X 0.4 GMM-LG PAN-HD | 28480 | 0515-0207 |

Table 6-2. Replaceable Parts

| Reference Designation | HP Part Number | $\left\lvert\, \begin{aligned} & C \\ & D \end{aligned}\right.$ | Qty | Description | Mfr Code | Mir Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AIOMP11 | 0515-0207 | 2 | 12 | SCREW-MACH M2 $\times 0.4$ GMM-LG PAN-HD | 28480 | 0515-0207 |
| A10MP12 | 0515-0207 | 2 |  | SCREW-MACH M2 $\times 0.4$ 6MM-LG PAN-HD | 28480 | 0515-0207 |
| A10MP13 | 0515-0207 | 2 |  | SCREW-MACH M2 $\times 0.4$ 6MM-LG PAN-HD | 28480 | 0515-0207 |
| A10MP14 | 0515-0207 | 2 |  | SCREW-MACH M2 $\times 0.4$ 6MM-LG PAN-HD | 28480 | 0515-0207 |
| A10MP15 | 0515-0207 | 2 |  | SCREW-MACH M2 $\times 0.4$ 6MM-LG PAN-HD | 28480 | 0515-0207 |
| A10MP16 | 0515-0207 | 2 |  | SCREW-MACH M2 $\times 0.4$ GMM-LG PAN-HD | 28480 | 0515-0207 |
| A10MP17 | 0515-0207 | 2 |  | SCREW-MACH M2 $\times 0.4$ 6MM-LG PAN-HD | 28480 | 0515-0207 |
| A10MP18 | 0515-0207 | 2 |  | SCREW-MACH M2 $\times 0.4$ 6MM-LG PAN-HD | 28480 | 0515-0207 |
| A10MP19 | 0515-0276 | 5 |  | SCREW-MACH M2 $\times 0.4$ 8MM-LG $90-$ DEG-FLH-HD | 28480 | 0515-0276 |
| A10MP20 | 0515-0276 | 5 |  | SCREW-MACH M2 $\times 0.4$ 8MM-LG 90-DEG-FLH-HD | 28480 | 0515-0276 |
| Alomp 21 | 0515-0276 | 5 |  | SCREW-MACH M2 $\times 0.48 \mathrm{MM}$-LG $90-\mathrm{DEG}$-FLH-HD | 28480 | 0515-0276 |
| A10MP22 | 0515-0276 | 5 |  | SCREW-MACH M2 $\times 0.48 \mathrm{MM}$-LG $90-$ DEG-FLH-HD | 28480 | 0515-0276 |
| A10MP23 | 0515-0276 | 5 |  | SCREW-MACH M2 $\times 0.48 \mathrm{MM}$-LG $90-$ DEG-FLH-HD | 28480 | 0515-0276 |
| A10MP24 | 0515-0276 | 5 |  | SCREW-MACH M2 $\times 0.48 \mathrm{MM}$-LG $90-$ DEG-FLH-HD | 28480 | 0515-0276 |
| A10MP25 | 0515-0276 | 5 |  | SCREW-MACH M2 $\times 0.4$ 8MM-LG $90-$ DEG-FLH-HD | 28480 | 0515-0276 |
| A10MP26 | 0515-0276 | 5 |  | SCREW-MACH M2 $\times 0.48 \mathrm{MM}$-LG $90-\mathrm{DEG}$-FLH-HD | 28480 | 0515-0276 |
| A10MP27 | 0515-0276 | 5 |  | SCREW-MACH M2 $\times 0.4$ 8MM-LG 90-DEG-FLH-HD | 28480 | 0515-0276 |
| A10MP28 | 0515-0276 | 5 |  | SCREW-MACH M2 $\times 0.4$ 8MM-LG $90-$ DEG-FLH-HD | 28480 | 0515-0276 |
| A10MP29 | 0515-0276 | 5 |  | SCREW-MACH M2 $\times 0.48 \mathrm{MM}$-LG 90 -DEG-FLH-HD | 28480 | 0515-0276 |
| A10MP30 | 0515-0276 | 5 |  | SCREW-MACH M2 X 0.4 8MM-LG $90-$ DEG-FLH-HD | 28480 | 0515-0276 |
| Alomp31 | 2190-0584 | 0 |  | WASHER-LK HLCL 3.0 MM 3.1-MM-ID | 28480 | 2190-0584 |
| A10MP32 | 2190-0584 | 0 |  | WASHER-LK HLCL 3.0 MM 3.1-MM-ID | 28480 | 2190-0584 |
| A10MP33 | 2190-0584 | 0 |  | WASHER-LK HLCL 3.0 MM 3.1-MM-ID | 28480 | 2190-0584 |
| A10MP34 | 2190-0584 | 0 |  | WASHER-LK HLCL 3.0 MM 3.1-MM-ID | 28480 | 2190-0584 |
| A10MP35 | 2190-0584 | 0 |  | WASHER-LK HLCL 3.0 MM 3.1-MM-ID | 28480 | 2190-0584 |
| A10MP36 | 2190-0584 | 0 | 12 | WASHER-LK HLCL 3.0 MM 3.1-MM-ID | 28480 | 2190-0584 |
| A10MP37 | 2190-0584 | 0 |  | WASHER-LK HLCL 3.0 MM 3.1-MM-ID | 28480 | 2190-0584 |
| A10MP38 | 2190-0584 | 0 |  | WASHER-LK HLCL 3.0 MM 3.1-MM-ID | 28480 | 2190-0584 |
| A10MP39 | 2190-0654 | 5 |  | WASHER-LK HLCL $2.0 \mathrm{MM} \mathrm{2.1-MM-ID}$ | 28480 | 2190-0654 |
| A10MP40 | 2190-0654 | 5 |  | WASHER-LK HLCL $2.0 \mathrm{MM} \mathrm{2.1-MM-ID}$ | 28480 | 2190-0654 |
| A10MP41 | 2190-0654 | 5 | 10 | UASHER-LK HLCL 2.0 MM 2.1-MM-ID | 28480 | 2190-0654 |
| A10MP42 | 2190-0654 | 5 |  | WASHER-LK HLCL $2.0 \mathrm{MM} \mathrm{2.1-MM-ID}$ | 28480 | 2190-0654 |
| A10MP43 | 2190-0654 | 5 |  | WASHER-LK HLCL $2.0 \mathrm{MM} \mathrm{2.1-MM-ID}$ | 28480 | 2190-0654 |
| A10MP44 | 2190-0654 | 5 |  | WASHER-LK HLCL $2.0 \mathrm{MM} \mathrm{2.1-MM-ID}$ | 28480 | 2190-0654 |
| A10MP45 | 2190-0654 | 5 |  | WASHER-LK HLCL 2.0 MM 2.1-MM-ID | 28480 | 2190-0654 |
| A10MP46 | 2190-0654 | 5 |  | WASHER-LK HLCL 2.0 MM 2.1-MM-ID | 28480 | 2190-0654 |
| A10MP47 | 2190-0654 | 5 |  | WASHER-LK HLCL 2.0 MM 2.1-MM-ID | 28480 | 2190-0654 |
| A10MP48 | 2190-0654 | 5 |  | WASHER-LK HLCL $2.0 \mathrm{MM} \mathrm{2.1-MIT-ID}$ | 28480 | 2190-0654 |
| A10MP49 | 3050-1066 | 0 |  | WASHER-FL MTLC 2.0 MM 2.28-MM-ID | 28480 | 3050-1066 |
| A10MP50 | 3050-1066 | 0 |  | WASHER-FL MTLC $2.0 \mathrm{MM} \mathrm{2.28-MM-ID}$ | 28480 | 3050-1066 |
| A10MPS 1 | 3050-1066 | $0$ |  | WASHER-FL MTLC $2.0 \mathrm{MM} \mathrm{2.28-MM-ID}$ | 28480 | 3050-1066 |
| A10MPS 2 | 3050-1066 | $0$ |  | WASHER-FL MTLC $2.0 \mathrm{MM} \mathrm{2.28-MM-ID}$ | 28480 | 3050-1066 |
| A10MP53 | 3050-1066 | 0 |  | WASHER-FL MTLC $2.0 \mathrm{MM} \mathrm{2.28-MM-ID}$ | 28480 | 3050-1066 |
| A10MP54 | 3050-1066 | 0 |  | WASHER-FL MTLC $2.0 \mathrm{MM} \mathrm{2.28-MM-ID}$ | 28480 | 3050-1066 |
| A10MP55 | 3050-1066 | 0 |  | WASHER-FL MTLC 2.0 MM 2.28-MM-ID | 28480 | 3050-1066 |
| A10MPS6 | 3050-1066 | 0 |  | WASHER-FL MTLC 2.0 MM 2.28-MM-ID | 28480 | 3050-1066 |
| A10MPS 7 | 3050-1066 | 0 |  | WASHER-FL MTLC 2.0 MM 2.28-MM-ID | 28480 | 3050-1066 |
| A10MP58 | 3050-1066 | 0 |  | WASHER-FL MTLC 2.0 MM 2.28-MM-ID | 28480 | 3050-1066 |
| A10MP59 | 11729-00032 | 7 | 1 | COVER IF AMP | 28480 | 11729-00032 |
| A10MP60 | 11729-20049 | 8 | 1 | HOUSING IF AMP | 28480 | 11729-20049 |
| A10MP61 A10MP62A10MP67 | 0360-0374 | 5 | 1 | TERMINAL-SLDR LUG PL-MTG FOR-\#4-SCR | 79963 | 9-120 |
|  | $0515-0264$ | $1$ | 16 | SCREW-MACH M3 $\times 0.5$ 30MM-LG PAN-HD | $28480$ | $0515-0264$ |
|  | 0515-0264 | 1 |  | SCREW-MACH M3 $\times 0.5$ 3OMM-LG PAN-HD (USED TO MOUNT IF AMPLIFIER TO THE DECK. | $28480$ | $0515-0264$ |
|  | 2190-0584 | 0 |  | WASHER-LK HLCL 3.0 MM 3.1-MM-ID USED TO MOUNT IF AMPLIFIER TO THE DECK. | 28480 | 2190-0584 |
| A11 | 11729-60071 | 0 | 1 | POWER AMPLIFIER ASSEMBLY | 28480 | 11729-60071 |
| Al1MP1 A1 1 MP2 | $\begin{aligned} & 11729-00034 \\ & 11729-00034 \end{aligned}$ | $\begin{aligned} & 9 \\ & 9 \end{aligned}$ | 2 | GASKET | $\begin{aligned} & 28480 \\ & 28480 \end{aligned}$ | $\begin{aligned} & 11729-00034 \\ & 11729-00034 \end{aligned}$ |
| Al 1 MP3 | 0960-0665 | 9 | 1 | ER DIVISION | 28480 | 0960-0665 |
|  | 0515-0264 | 1 |  | SCREW-MACH M3 $\times 0.5$ 3OMM-LG PAN-HD (USED TO MOUNT POWER AMP TO DECK) | 28480 | 0515-0264 |
|  | 2190-0584 | 0 |  | WASHER-LK HLCL 3.0 MM 3.1-MM-ID (USED TO MOUNT POWER AMP TO DECK) | 28480 | 2190-0584 |
|  | 3050-0105 | 6 | 51 | WASHER-FL MTLC NO. 4 . 125-IN-ID (USED TO MOUNT POWER AMP TO DECK) | 28480 | 3050-0105 |

See introduction to this section for ordering information

Table 6-2. Replaceable Parts


Table 6-2. Replaceable Parts



Figure 6-1. External Mechanical Parts

Table 6-2. Replaceable Parts


See introduction to this section for ordering information


Figure 6-2. Chassis Parts

Table 6-2. Replaceable Parts



Figure 6-3. Front Panel Parts

Table 6-2. Replaceable Parts



Figure 6-4. Rear Panel Parts

Table 6-2. Replaceable Parts



Figure 6-5. Switch Assembly Mechanical Parts

Table 6-2. Replaceable Parts


See introduction to this section for ordering information


Figure 6-6. Power Supply and Low Noise Amplifier Mechanical Parts

Table 6-2. Replaceable Parts


See introduction to this section for ordering information


Figure 6-7. A9 Assembly Mechanical Parts

Table 6-2. Replaceable Parts


Table 6-2. Replaceable Parts

| Reference Designation | HP Part Number | $\left\|\begin{array}{l} C \\ D \end{array}\right\|$ | Qty | Description | Mfr Code | Mir Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| W14 | 11729-60023 | 2 | 1 | CABLE ASSEMBLY |  |  |
| W15 | 11729-60059 | 4 | 1 | CABLE ASSEMBLY | 28480 28480 | $\begin{aligned} & 11729-60023 \\ & 11729-60059 \end{aligned}$ |
| 416 $W 17$ | 11729-60057 $11729-60022$ | 2 | 1 | CABLE ASSEMBLY | 28480 | 11729-60057 |
| $W 17$ $W 18$ | $11729-60022$ $11729-60032$ | 1 3 | 1 | CABLE ASSEMBLY CABLE ASSEMELY | 28480 28480 | $11729-60022$ $11729-60032$ |
| W19 | 11729-60035 | 6 | 1 | CABLE ASSEMBLY | 28480 |  |
| W20 $W 21$ | 11729-60033 | 4 | 1 | CABLE ASSEMBLY | 28480 28480 | $11729-60035$ $11729-60033$ |
| W22 | 11729-60025 | 4 | 1 | NOT ASSIGNED |  |  |
| W23 | 11729-20038 | 5 | 1 | CABLE ASSY (OPT. 130 ONLY) | 28480 28480 | $11729-60025$ $11729-20038$ |
| W24 | 11729-20073 | 8 | 1 | CABLE ASSEMBLY | 28480 | 11729-20073 |
| W25 | 08672-20157 | 4 | 7 | CABLE ASSEMBLY | 28480 | 08672-20157 |
| W26 | $08672-20157$ $11729-20070$ | 4 | 7 | CABLE ASSEMBLY | 28480 | 08672-20157 |
| W28 | 8120-1378 | 1 | 1 | ASSEMBLY-CABLE (POWER CABLE) | 28480 28480 | $11729-20070$ $8120-1378$ |
| W29 |  |  |  | NOT ASSIGNED |  |  |
| W30 | $\begin{aligned} & 11729-60101 \\ & 1400-0510 \end{aligned}$ | $7$ | $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | CABLE ASSY(FOR IF \& LOW NOISE AMP) | 28480 | 11729-60101 |
| W31 | $11720-0510$ $11729-20070$ | 8 |  | CLAMP-CABLE ${ }^{\text {a }}$ - $15-$ IIA .62-WD NYL CABLE ASSEMBLY | 28480 28480 | $1400-0510$ $11729-20070$ |
| W32 | 08672-20157 | 4 |  | CABLE ASSEMBLY | 28480 | 08672-20157 |
| $W 33$ $W 34$ | 11729-20070 $08672-20157$ | 5 4 |  | CABLE ASSEMBLY | 28480 | 11729-20070 |
| W34 W35 | 08672-20157 $11729-20070$ | 4 |  | CABLE ASSEMBLY | 28480 | 08672-20157 |
| 436 | 08672-20157 | 4 |  | CABLE ASSEMBLY | 28480 28480 | 11729-20070 |
| W37 | 11729-20070 | 5 |  | CABLE ASSEMBLY | 28480 | 11729-20070 |
| W38 | 08672-20157 | 4 |  | CABLE ASSEMBLY | 28480 | 08672-20157 |
| W39 $W 40$ | 11729-20070 | 5 |  | CABLE ASSEMBLY | 28480 | 11729-20070 |
| W41 | 11729-20070 | 4 |  | CABLE ASSEMBLY CABLE ASSEMELY | 28480 | 08672-20157 |
| W42 | 11729-20068 | 1 | 1 | CABLE ASSEMBLY | 28480 28480 | $\begin{aligned} & 11729-20070 \\ & 11729-20068 \end{aligned}$ |
| W43 |  |  |  | NOT ASSIGNED |  |  |
| W44 W45 |  |  |  | NOT ASSIGNED |  |  |
| W46 |  |  |  | NOT ASSIGNED |  |  |
| W47 | 11729-20069 | 2 | 1 | CABLE ASSEMBLY CABLE ASSEMBLY | 28480 28480 | 11729-20066 $11729-20069$ |
|  | 11729-20095 | 4 | 1 | CABLE ASSEMBLY (W47; OPTION 140) | 28480 | 11729-20095 |
| $W 48$ $W 49$ |  |  |  | NOT ASSIGNED |  |  |
| W49 W50 | 11729-60060 | 7 | 1 | CABLE ASSEMBLY | 28480 | 11729-60060 |
| W50 | 11729-60050 | 5 | 1 | CABLE ASSEMBLY (HP-IB INTERCONNECT TO MICROPROCESSOR) | 28480 | 11729-60050 |
| W51 | 11729-60058 | 3 | 1 | CABLE ASSY (CABLE FROM MICROPROCESSOR TO SWITCHES) | 28480 | 11729-60058 |
|  | $1400-0619$ $0515-0054$ | $8$ | 5 | CABLE CLAMP-HFCL . 312-DIA . $5-\mathrm{WD}$ | 28480 |  |
|  | 0515-0054 | $7$ |  | SCREW-MACH M3 $\times 0.5$ 10MM-LG PAN-HD | 28480 | $0515-0054$ |
| W52 | $\begin{aligned} & 11729-60045 \\ & 1400-0611 \end{aligned}$ | 8 | 1 | CABLE ASSEMBLY CLAMP-FL-CA 1-WD | 28480 | 11729-60045 |
| W53 | $11720-0611$ $11729-60052$ | 7 | 2 | CLAMP-FL-CA 1-WD CABLE ASSEMBLY (FROM MICROPROCESSOR | 06915 | CFCC-8 |
|  | 11729-60052 | 7 | 1 | TO FRONT PANEL) (FROM MICROPROCESSOR | 28480 | 11729-60052 |
|  | 1400-0611 | 0 |  | CLAMP-FL-CA 1-WD | 06915 | CFCC-8 |
| W54 W55 | 11729-60051 | 6 | 1 | CABLE ASSEMBLY | 28480 | 11729-60051 |
| U55 W56 | $11729-60107$ $11729-60077$ | 3 | 1 | CABLE ASSEMBLY (OPTION 140; 640MHZ IN) | 28480 | 11729-60107 |
| 456 | 11729-60077 | 6 | 1 | CABLE ASSEMBLY (OPTION 140; LOOP TEST PORT OUT) | 28480 | 11729-60077 |
| $\omega 57$ | 11729-60105 | 1 | 1 | CABLE ASSEMBLY (OPTION 140; AUX NOISE) | 28480 | 11729-60105 |
| W58 | 11729-60076 | 5 | 1 | CABLE ASSEMBLY (OPTION 140; NOISE SPECTRUM <1MHZ) | 28480 | 11729-60076 |
| W59 | 11729-60081 | 2 | 1 | CABLE ASSEMBLY (OPTION 140; IF OUTPUT) | 28480 | 11729-60081 |
| W60 | 11729-60080 | 1 | 1 | CABLE ASSEMBLY (OPTION 140; 5 TO 1280 MHZ IN) | 28480 | 11729-60080 |
| W61 | 11729-60075 | 4 | 1 | CABLE ASSEMBLY (OPTION 140; FREQ-CONT X -OSC) | 28480 | 11729-60075 |
| W62 | 11729-60074 | 3 | 1 | CABLE ASSEMBLY (OPTION 140; FREQ-CONT DC-FM) | 28480 | 11729-60074 |
| W63 | 11729-60078 | 7 | 1 | CABLE ASSEMBLY (OPTION 140; LOOP TEST PORT IN) | 28480 | 11729-60078 |

Table 6-2. Replaceable Parts


Table 6-3. Code List of Manufacturers


## SECTION VII MANUAL CHANGES

## 7-1. INTRODUCTION

This section normally contains information for adapting the manual to older instruments. However, no manual changes existed when this manual was printed.
If your instrument's serial number prefix is not listed on the title page of this manual, it may be
documented in a separate MANUAL CHANGES supplement. For more information about serial number prefixes, refer to INSTRUMENTS COVERED BY MANUAL in Section I.


## SECTION VIII SERVICE

## 8-1. INTRODUCTION

This section contains information for troubleshooting and repairing the Carrier Noise Test Set. Included are troubleshooting tests, schematic and block diagrams, and principles of operation.

## 8-2. SERVICE SHEETS

The foldout pages (Service Sheets) in the last part of this section are a block diagram (BD1) and schematics (1 through 7).

## 8-3. Block Diagrams

Block Diagram 1 (BD1) is an overall block diagram that breaks the instrument into functional sections. It serves as an index to the schematic Service Sheets and as a starting point for troubleshooting.

## 8-4. Schematics

Service Sheets 1 through 7 consist of assembly schematic diagrams. Symbols used in the schematic diagrams are defined in Table 8-2, Schematic Diagram Notes.

## 8-5. SAFETY CONSIDERATIONS

## 8-6. Before Applying Power

Verify that the instrument is set to match the available line voltage and that the correct fuse is installed. An uninterrupted safety earth ground must be provided from the main power source to the instrument input wiring terminals, power cord, or supplied power cord set.

## 8-7. Safety

Pay attention to WARNINGS and CAUTIONS. They must be followed for your protection and to avoid damage to the equipment.

## WARNINGS

Maintenance described herein is performed with power supplied to the instrument and with protective covers removed. Such maintenance should be performed only by servicetrained personnel who are aware of the
hazards involved (for example, fire and electrical shock). Where maintenance can be performed without power supplied, the power should be removed.

Any interruption of the protective (grounding) conductor (inside or outside the instrument) or discionnection of the protective earth terminal will create a potential shock hazard that could result in personal injury. Grounding one conductor outlet is not sufficient. Whenever it is likely that the protection has been impaired, the instrument must be made inoperative (that is, secured against unintended operation).

If this instrument is to be energized via an autotransformer, make sure that the autotransformer's common terminal is connected to the earth terminal of the power source.

Capacitors inside the instrument can still be charged even if the instrument is disconnected from its source of supply.

Make sure that only 250 volt fuses with the required rated current and of the specified type (normal blow, time delay, etc.) are used for replacement. Do not use repaired fuses or short-circuited fuse-holders. To do so could create a shock or fire hazard.

## 8-8. RECOMMENDED TEST EQUIPMENT

Test equipment required to maintain the Carrier Noise Test Set is listed in Table 1-4. Equipment other than that listed may be used if it meets the listed critical specifications.

## 8-9. SERVICE TOOLS, AIDS AND INFORMATION

## 8-10. Pozidriv Screwdrivers

Many screws in the Carrier Noise Test Set appear to be Phillips types, but are not. To avoid damage to the screw slots, Pozidriv screwdrivers should be used. HP 8710-0899 is the No. 1 Pozidriv. HP 87100900 is the No. 2 Pozidriv.

## 8-11. Tuning Tools

For adjustments requiring non-metalic tuning tools, use the HP 8710-0033 blade tuning tool or the HP 8710-1010 (JFD Model No. 5284) hex tuning tool. For other adjustments an ordinary small screwdriver or suitable tool is sufficient. No matter which tool is used, never force any adjustment control.

## 8-12. Heat Staking Tools

The pushbutton switches on the front panel have small plastic pins protruding from the back. These tabs fit through holes in the front panel printed
circuit boards (A1 and A2) and are melted down to hold the switch in place. This process is known as heat staking. The heat staking tool is a standard soldering iron with a special tip attached.

## 8-13. Hardware

Both Unified National (inch) and metric screws are used in the Carrier Noise Test Set.

## 8-14. Maintenance

Hewlett-Packard recommends the dust that may accumulate inside the Carrier Noise Test Set to be blown out periodically.

Table 8-1. Etched Circuit Soldering Equipment

| Item | Use | Specification | Item Recommended | HP Part No. |
| :---: | :---: | :---: | :---: | :---: |
| Soldering Tool | Soldering, <br> Heat Staking | Wattage: 35W <br> Tip Temp.: 390-440 ${ }^{\circ} \mathrm{C}$ (735-825 ${ }^{\circ} \mathrm{F}$ ) | Ungar No. 135 <br> Ungar Division Eldon Ind. Corp. <br> Compton, CA 90220 | 8690-0167 |
| Soldering Tip | Soldering, Unsoldering | *Shape: Chisel | *Ungar PL113 | 8690-0007 |
| Soldering Tip | Heat Staking | Shape: Cupped | HP 5020-8160 or modified Ungar PL11 | 5020-8160 |
| De-Solder Aid | To remove molten solder from connection | Suction Device | Soldapullt by Edsyn Co., Van Nuys, CA 91406 | 8690-0060 |
| Rosin (flux) <br> Solvent | To remove excess flux from soldered area before application of protective coating | Must not dissolve etched circuit base board. | Freon TF | 8500-0232 |
| Solder | Component replacement, Circuit Board repair wiring | Rosin (flux core, high tin content ( $63 / 37 \mathrm{tin} /$ lead), 18 gauge (AWG) 0.040 in. diameter preferred. |  | 8090-0607 |
| *For working on circuit boards; for general purpose work, use No. 555 Handle ( $8690-0261$ ) and No. 4037 Heating Unit 47 $1 / 2$ - $561 / 2$ W (HP 8690-0006); tip temperature of $850-900^{\circ} \mathrm{F}$; and Ungar No. PL113 $1 / \mathrm{s}^{\prime \prime}$ chisel tip. |  |  |  |  |

Table 8-2. Schematic Diagram Notes (1 of 8)


Table 8-2. Schematic Diagram Notes (2 of 8)

## SCHEMATIC DIAGRAM NOTES



## Table 8-2. Schematic Diagram Notes (3 of 8)

## SCHEMATIC DIAGRAM NOTES



Indicates multiple paths represented by only one line. Letters or names identify individual paths. Numbers indicate number of paths represented by the line.

Coaxial or shielded cable.

Relay. Contact moves in direction of arrow when energized.

Indicates a pushbutton switch with a momentary (ON) position.

Indicates a PIN diode.

Indicates a current regulation diode.

Indicates a voltage regulation diode.

Indicates a Schottky (hot-carrier) diode.




Multiple transistors in a single package-physical location of the pins is shown in package outline on schematic.

Identification of logic families as shown (in this case, ECL).

Indicates an opto-isolator of a LED and a photoresistor packaged together. The resistance of the photoresistor is a function of the current flowing through the LED.

Table 8-2. Schematic Diagram Notes (4 of 8)

## DIGITAL SYMBOLOGY REFERENCE INFORMATION

## Input and Output Indicators



Implied Indicator-Absence of polarity indicator (see below) implies that the active state is a relative high voltage level. Absence of negation indicator (see below) implies that the active state is a relative high voltage level at the input or output.

Polarity Indicator-The active state is a relatively low voltage level.

Dynamic Indicator-The active state is a transition from a relative low to a relative high voltage level.

Inhibit Input-Input that, when active, inhibits (blocks) the active state outputs of a digital device.

Analog Input-Input that is a continuous signal function (e.g., a sine wave).

Polarity Indicator used with Inhibit Indicator-Indicates that the relatively low level signal inhibits (blocks) the active state outputs of a digital device.
m


Output Delay-Binary output changes state only after the referenced input ( m ) returns to its inactive state ( m should be replaced by appropriate dependency or function symbols).

Open Collector Output-Output that must form part of a distributed connection.

## DIGITAL SYMBOLOGY REFERENCE INFORMATION

## Input and Output Indicators (Cont'd)

3-STATE Three-state Output-Indicates outputs that can have a high impedance (disconnect) state in addition to the normal binary logic states.

## Combinational Logic Symbols and Functions

\&
$\geq 1$
$\geq m \quad$ Logic Threshold-m or more inputs being active will cause the output to be active (replace $m$ with a number).
$=1$
$=\mathrm{m} \quad \mathrm{m}$ and only m -Output will be active when m (and only m ) inputs are active (replace $m$ with a number).
$=\quad$ Logic Identity-Output will be active only when all or none of the inputs are active (i.e., when all inputs are identical, output will be active).

Amplifier-The output will be active only when the input is active (can be used with polarity or logic indicator at input or output to signify inversion).

Signal Level Converter-Input level(s) are different than output level(s).

Bilateral Switch-Binary controlled switch which acts as an on/off switch to analog or binary signals flowing in both directions. Dependency notation should be used to indicate affecting/affected inputs and outputs. Note: amplifier symbol (with dependency notation) should be read to indicate unilateral switching.
$X \rightarrow Y$
(Functional Labels)

MUX

DEMUX

CPU
Central Processing Unit
PIO Peripheral Input/Output
SMI
AND-All inputs must be active for the output to be active.
OR-One or more inputs being active will cause the output to be active.

EXCLUSIVE OR-Output will be active when one (and only one) input is active.

Coder-Input code ( X ) is converted to output code ( Y ) per weighted values or a table.

The following labels are to be used as necessary to ensure rapid identification of device function.

Multiplexer-The output is dependent only on the selected input.
Demultiplexer-Only the selected output is a function of the input.

Static Memory Interface

Table 8-2. Schematic Diagram Notes (6 of 8)

## DIGITAL SYMBOLOGY REFERENCE INFORMATION

## Sequential Logic Functions

Monostable-Single shot multivibrator. Output becomes active when the input becomes active. Output remains active (even if the input becomes inactive) for a period of time that is characteristic of the device and/or circuit.

Oscillator-The output is a uniform repetitive signal which alternates between the high and low state values. If an input is shown, then the output will be active if and only if the input is in the active state.

Flip-Flop-Binary element with two stable states, set and reset. When the flip-flop is set, its outputs will be in their active states. When the flip-flop is reset, its outputs will be in their inactive states.

Toggle Input-When active, causes the flip-flop to change states.
Set Input-When active, causes the flip-flop to set.
Reset Input-When active, causes the flip-flop to reset.
J Input-Analogous to set input.
K Input-Analogous to reset input.
D Data Input-Always enabled by another input (generally a C input-see Dependency Notation). When the $D$ input is dependency-enabled, a high level at $D$ will set the flip-flop; a low level will reset the flip-flop. Note: strictly speaking, D inputs have no active or inactive states-they are just enabled or disabled.

Count-Up Input-When active, increments the contents (count) of a counter by " m " counts ( m is replaced with a number).

Count-Down Input-When active, decrements the contents (count) of a counter by " $m$ " counts ( $m$ is replaced with a number).

Shift Right (Down) Input-When active, causes the contents of a shift register to shift to the right or down " $m$ " places ( $m$ is replaced with a number).

Shift Left (Up) Input-When active, causes the contents of a shift register to shift to the left or up " $m$ " places ( $m$ is replaced with a number).

## NOTE

For the four functions shown above, if $m$ is one, it is omitted.
(Functional
Labels)

The following functional labels are to be used as necessary in symbol build-ups to ensure rapid identification of device function.

Table 8-2. Schematic Diagram Notes (7 of 8)

## DIGITAL SYMBOLOGY REFERENCE INFORMATION

## Sequential Logic Functions (Cont'd)

mCNTR

REG

SREG
ROM
RAM Random Access Memory-Addressable memory with read-in and read-out capability.

## Dependency Notation

mAm Address Dependency-Binary affecting inputs of affected outputs. The $m$ prefix is replaced with a number that differentiates between several address inputs, indicates dependency, or indicates demultiplexing and multiplexing of address inputs and outputs. The m suffix indicates the number of cells that can be addressed.

Gm Gate (AND) Dependency-Binary affecting input with an AND relationship to those inputs or outputs labeled with the same identifier. The $m$ is replaced with a number or letter (the identifier).
$\mathrm{Cm} \quad$ Control Dependency-Binary affecting input used where more than a simple AND relationship exists between the $C$ input and the affected inputs and outputs (used only with D-type flip-flops).

OR Dependency-Binary affecting input with an OR relationship to those inputs or outputs labeled with the same identifier. The $m$ is replaced with a number or the letter (the identifier).

Fm Free Dependency-Binary affecting input acting as a connect switch when active and a disconnect when inactive. Used to control the 3 -state behavior of a 3 -state device.

## NOTE

The identifier ( $m$ ) is omitted if it is one-that is, when there is only one dependency relationship of that kind in a particular device. When this is done, the dependency indicator itself ( $G, C, F$, or $V$ ) is used to prefix or suffix the affected (dependent) input or output.

Table 8-2. Schematic Diagram Notes (8 of 8)

## DIGITAL SYMBOLOGY REFERENCE INFORMATION

## Miscellaneous


#### Abstract

Schmitt Trigger-Input characterized by hysteresis; one threshold for positive going signals and a second threshold for negative going signals.

Active ActiveState-A binary physical or logical state that corresponds to the true state of an input, an output, or a function. The opposite of the inactive state.

Enable Enabled Condition-A logical state that occurs when dependency conditions are satisfied. Although not explicitly stated in the definitions listed above, functions are assumed to be enabled when their behavior is described. A convenient way to think of it is as follows:


A function becomes active when:

- it is enabled (dependency conditions-if any-are satisfied)
- and its external stimulus (e.g., voltage level) enters the active state.


## SERVICE SHEET BD1 OVERALL FUNCTIONAL BLOCK DIAGRAM .PRINCIPLES OF OPERATION

General. The HP Model 11729C Carrier Noise Test Set performs four (4) major tasks:

- Up converts an external (or internal) reference signal
- Down converts the signal under test to an intermediate frequency (IF)
- Phase demodulates the phase noise of the test signal using the Phase Detector Method.
- When the Phase Detector Method is used the signal under test is phase locked to a reference signal.
-The signal under test is then phase detected against the same reference signal.
- Frequency demodulates the phase noise of the test signal using the Frequency Discriminator Method.

These four operations allow the Carrier Noise Test Set to be used as an integral part of a phase noise measurement system. With Option 130 installed, the Carrier Noise Test Set has AM noise measurement capabilities. The Carrier Noise Test Set accepts test signals from $10 \mathrm{MHz}-18 \mathrm{GHz}$, at a level of +7 dBm to +20 dBm and -5 to +10 dBm for test signals $<1.28 \mathrm{GHz}$.

For the Carrier Noise Test Set to be completely operational it may require one or two drive signals(a fixed 640 MHz signal and/or a tunable 5 MHz to 1280 MHz signal) that are supplied from an external RF source.
One of the drive signals $(640 \mathrm{MHz})$ can be supplied by the Carrier Noise Test Set. The Carrier Noise Test Set can be configured to provide an internally generated 640 MHz signal; the 640 MHz signal is made available by connecting the provided cableattenuator assembly (HP 11729-60096 or HP 1172960098 [Option 140] ) between two rear panel connectors. The absolute system noise floor will be degraded close-in to the carrier when using the internally generated 640 MHz signal, compared to the 640 MHz signal being supplied by the HP 8662A Synthesized Signal Generator.
The following discussion describes the purpose of Service Sheets 1-6.

## Service Sheet 1-Reference Up-Conversion, Test Signal Down-Conversion and Phase Detecting Circuits

Service Sheet 1 has all the circuitry necessary to
up-convert the reference signal, and down-convert and phase detect the signal under test.
The signal under test ( $10 \mathrm{MHz}-18 \mathrm{GHz}$ ) is downconverted to $5 \mathrm{MHz}-1280 \mathrm{MHz}$. For test signals from $10 \mathrm{MHz}-1280 \mathrm{MHz}$ down-converting is not required. To achieve the down-converted signal a fixed 640 MHz signal us up-converted to microwave frequencies by being input to a comb generator (step recovery diode multiplier). The comb generator outputs harmonics of the 640 MHz signal. One of the harmonics is selected with a passband filter. The filter is user selectable from the front panel (local) or by using the Hewlett-Packard Interface Bus (remote). The harmonic selected is mixed with the signal under test. The result produces a down-converted signal under test from 5 $\mathrm{MHz}-1280 \mathrm{MHz}$. The resulting signal (or direct test signal from $10 \mathrm{MHz}-1280 \mathrm{MHz}$ ) is input to a mixer/phase detector along with a tunable 5 to 1280 MHz signal. The end product is a dc signal with ac components directly proportional to the phase detected difference between the signal under test and the tunable $5 \mathrm{MHz}-1280 \mathrm{MHz}$ signal.
All circuitry necessary for AM detecting the signal under test, to make an AM noise measurement, is on Service Sheet 1.

## Service Sheet 2-Low Pass Filter and Low Noise Amplifier Circuits

The de signal from the mixer/phase detector on Service Sheet 1 is filtered and output for connection to a spectrum analyzer.

The Low Noise Amplifier amplifies the filtered signal so it can be seen on a laboratory spectrum analyzer.

## Service Sheet 3—Phase Lock Circuits

With the Phase Detector Method of making a phase noise measurement, the signal under test and the tunable $5 \mathrm{MHz}-1280 \mathrm{MHz}$ signal must stay in phase quadrature (that is, 90 degrees out-of-phase). A phase lock loop is used to maintain this phase relationship.
Phase lock loops consist of the following three components:

> - A Voltage Controlled Oscillator (VCO)
> - A Phase Detector
> - A Loop Filter

The VCO of the phase lock loop can be either the external RF source supplying the tunable $5 \mathrm{MHz}-$

## SERVICE SHEET BD1 (cont'd)

1280 MHz signal or it can be the device under test. The other two components of the phase lock loop are supplied by the Carrier Noise Test Set. The phase detector is shown on Service Sheet 1.

The loop filter circuitry for controlling the phase lock loop bandwidth is shown on this Service Sheet. The main input to the Phase Lock Circuits is from the mixer/phase detector through a low pass filter (on Service Sheet 2). The signal from the mixer/phase detector is input to a series of amplifiers with variable gain. The gain (loop bandwidth) is user selectable in local (front panel) or remote (HP-IB) by selection of the Lock Bandwidth Factor. The signal from the mixer/phase detector is processed through the series of amplifiers and the following signals are output:

- FREQ CONT DC-FM
- FREQ CONT X-OSC

These two signals are supplied to control the frequency of the VCO. The signal chosen will depend on the tuning voltage required by the VCO. FREQCONT X-OSC has an output voltage of $\pm 10$ Volts dc. FREQ-CONT DC-FM has an output voltage of $\pm 1$ Volt dc. When locked, the VCO will now track these control signals.

A CAPTURE control is supplied to widen the loop bandwidth, when first trying to acquire phase lock. The CAPTURE control causes the gain of the amplifiers to be fixed. The CAPTURE control overrides any gain that was set by the Lock Bandwidth Factor.

The LOOP TEST PORTS are used to characterize the frequency response of the phase lock loop. This characterization determines how much the loop suppresses noise at different frequency offsets from the signal under test.

## Service Sheet 4—Data Input Circuits

Service Sheet 4 shows how data is input to the Carrier Noise Test Set. The data can be input using the front panel or Hewlett-Packard Interface Bus (remote). All necessary circuitry for encoding the front panel keys and interfacing with the microprocessor in local is documented on Service Sheet 4.

## Service Sheet 5-Data Processing Circuits

Service Sheet 5 contains the microprocessor, ROM
and RAM. Information entered into the Carrier Noise Test Set is processed by this circuitry.

## Service Sheet 6-Switch and LED Control Circuits

Data is entered in local or remote (HP-IB). Next it is processed by the circuitry shown on Service Sheet 5, then output to the circuitry shown on Service Sheet 6. Service Sheet 6 consists mainly of data latches and drivers. The data output from Service Sheet 5 is available to all latches in parallel. The data in the latches is used to control the filter switches and front panel LEDs.

## TROUBLESHOOTING

The troubleshooting procedures are referenced to the Block Diagram by a hexagon with a checkmark and a number inside.

For example, $\sqrt{1}$

## Test Equipment

Digital Multimeter .................. HP 3456A
Microwave Synthesized Source ......HP 8340A
Oscilloscope . .......................... HP 1740A
Spectrum Analyzer . . . . . . . . . . . . . . . . . HP 8566B
Power Meter . . . . . . . . . . . . . . . . . . . . . HP 436A
RF Synthesized Signal Generator . . .HP 8662A
(Option 003)

## AM SWITCH OPERATION VI

The following troubleshooting will help to isolate an AM switch problem to the Microprocessor Circuits or the Reference Up-conversion, Test Signal Down-conversion and Phase Detecting Circuits.

## AM Switch Drive Circuitry Verification

1. Remove the top cover of the Carrier Noise Test Set.
2. Locate the AM switch. The switch on the far right next to the IF amplifier (A10), as viewed from the front, is the AM switch.
3. Verify +24 volts is on pin 2 (center pin of the switch). If the voltage is correct, proceed to step 4. If the voltage is incorrect, inspect the switch wiring, then if necessary troubleshoot the power supply circuitry on Service Sheet 7.
4. Monitor the voltage on pin 3 (top pin of the AM switch) while pressing the MODE switch repeatedly on the front panel. The voltages measured should change as follows:

## SERVICE SHEET BD1 (cont'd)

| AM Switch | MODE |  |
| :---: | :---: | :---: |
|  | AM <br> [CW or pulsed] | Phase Noise <br> [CW or pulsed] |
|  | +0.7 V | +23.8 V |
| pin 2 | +23.8 V | +23.8 V |
| pin 3 | +23.8 V | +0.7 V |

5. If the voltages measured are correct proceed to step 6. If the voltages are incorrect, check the wiring to the switch or the AM switch circuitry on Service Sheet 6.
6. Check the operation of the AM switch. The proper operating conditions of the AM switch are listed below:
A clicking sound can be heard when the MODE switch on the front panel is repeatedly pushed.

The AM modulation on a microwave test signal input can be viewed from the $<10 \mathrm{MHz}$ output when the AM noise measurement mode is enabled.

## MICROWAVE FILTER SWITCH OPERATION (V2)

The following troubleshooting will help to isolate a microwave filter switch problem to the Microprocessor Circuits or the Reference Up-conversion, Test Signal Down-conversion and Phase Detecting Circuits.

## NOTE

Before starting to troubleshoot be sure to confirm that the 640 MHz IN signal is $640 \mathrm{MHz} \pm 32 \mathrm{kHz}$ at a level of +1 dBm minimum.

## Microwave Filter Switch Drive Circuitry Verification

1. Remove the top cover of the Carrier Noise Test Set.
2. Locate the microwave switch that is not properly operating. The group of switches for bands 2 through 8 are located on the left side of the instrument as viewed from the front. The switches for bands 2 through 8 are setup consecutively from left to right.
The switch for band 1 is located on the right side of the instrument as viewed from the
front. If there are two (2) switches on the right side, the switch located closest to the side of the instrument is the switch for band one (1).
3. Verify that +24 volts is on pin 2 (the center pin of the switch in question).
If the voltage is correct, proceed to step 4. If the voltage is incorrect, inspect the switch wiring, then if necessary troubleshoot the power supply circuitry on Service Sheet 7.
4. Monitor the voltage on pin 3 (top pin of switch). Select the button on the front panel that controls the band in question. Select another band to switch out the band in question. The voltages measured should change as follows:

| Microwave <br> Filter <br> Switch | Bands 2-8 |  | Band 1 |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Selected | Not Selected | Selected | Not Selected |
| pin 1 | +0.7 V | +23.8 V | +23.8 V | +0.7 V |
| $\operatorname{pin} 2$ | +23.8 V | +23.8 V | +23.8 V | +23.8 V |
| $\operatorname{pin} 3$ | +23.8 V | +0.7 V | +0.7 V | +23.8 V |

5. If the voltages measured are correct proceed to step 6. If the voltages are incorrect troubleshoot the wiring to the switch or the microwave filter switch circuitry on Service Sheet 6.

## Microwave Filter Switch Verification

6. Proper operation of the microwave filter switch is listed below:

Input a microwave test signal at a frequency of 400 MHz above the BAND CENTER frequency of the BAND RANGE in question. The level of the microwave test signal in band one should be 0 dBm . In bands $2-8$ the level should be +10 dBm .

Observe the IF OUTPUT, on the front panel, with a spectrum analyzer. A 400 MHz IF signal should be seen if the band is operating properly.

## AM NOISE DETECTOR (V3)

## (Option 130 Only)

The following troubleshooting will isolate an AM Noise Detector problem to either the Reference Upconversion, Test Signal Down-conversion and Phase Detecting Circuits or the Low Pass Filter

## SERVICE SHEET BD1 (cont'd)

and Low Noise Amplifier circuits. Use the following test conditions to verify that the AM Noise Detector is operating properly:

1. Connect a 10 GHz signal at a level of +10 dBm to the MICROWAVE TEST SIGNAL INPUT connector on the front panel.
2. Push the MODE button until the AM, CW LED is illuminated.
3. Disconnect cable (W5) from the AM-DET (J2) connector on the Low Pass Filter Board Assembly. Connect a multimeter to the end of cable (W5). Set the multimeter to volts dc. The voltage on the multimeter should read typically -0.8 volts dc.
4. Push the MODE button so the $\phi$, CW LED is illuminated. The multimeter should now read 0 volts dc.
5. If these voltages are correct troubleshoot the Low Pass Filter Circuits on Service Sheet 2. If these voltages are incorrect, disconnect the AM detector (CR2) from the AM switch (S9). Measure the power out of port one (1) of the AM switch. The power measured should be $>+9.5$ dBm .
6. If the measured power is correct check the AM detector and associated wiring. If the measured power is incorrect, refer to the AM switch operation.

## IF INPUT TO LOW PASS FILTER (V4)

The following troubleshooting will isolate an IF problem to either the Reference Up-conversion, Test Signal Down-conversion and Phase Detecting Circuits or the Low Pass Filter and Low Noise Amplifier circuits.

1. Set the following initial conditions:

## Carrier Noise Test Set

BAND CENTER FREQUENCY: $9.6 \mathrm{GHz}^{*}$ LOCK BANDWIDTH FACTOR: 10 k MODE: $\phi$, CW
Disconnect cable from frequency control (X-OSC or DC-FM) on the rear panel.

Microwave Source (See critical specifications in Section I)

```
FREQUENCY: 10 GHz (CW)*
LEVEL: +10 dBm
MODULATION: Off
ALL OTHER FUNCTIONS: Off
```

Tunable 5 to 1280 MHz Source (See critical specifications in Section I)

FREQUENCY: 400.01 MHz (CW)*
LEVEL: 0 dBm
MODULATION: Off
ALL OTHER FUNCTIONS: Off
2. Verify that the voltage out of the IF port on the U7 mixer (Phase Detector) is 0.25 Vpp into 50 ohms.
3. If the voltage is correct troubleshoot the Low Pass Filter and Low Noise Amplifier Circuits. If the voltage is incorrect, troubleshoot the Reference Up-conversion, Test Signal Downconversion and Phase Detecting Circuits.

## PHASE LOCK DETECTOR SIGNAL (V5)

The following troubleshooting will isolate a Phase Lock Detector Signal problem to the Low Pass Filter and Low Noise Amplifier circuits or the Phase Lock Circuits.

1. Connect a $10 \mathrm{GHz}^{*}$ signal at a level of +10 dBm to the MICROWAVE TEST SIGNAL INPUT connector (J6) on the front panel.
2. Connect a 400.1 MHz * signal at a level of -40 dBm to the 5 to 1280 MHz INPUT connector on the front panel.
3. On the front panel select the BAND RANGE with a BAND CENTER frequency of $9.6 \mathrm{GHz}^{*}$. Enable $\phi$, CW MODE and a Lock Bandwidth Factor of 100 .
4. On the Low Pass Filter Board Assembly disconnect cable (W10) at LNA (J4).
5. On the A7 Power Supply Board Assembly disconnect cable (W6) to the PHASE LOCK IN connector J9.
6. Connect cable W6 to a spectrum analyzer. Measure the power of the 100 kHz beat note. The power should be -48 dBm typical.
7. If the power is correct troubleshoot the Phase Lock circuits on Service Sheet 3. If the power is incorrect troubleshoot the Low Pass Filter and
[^9]
## SERVICE SHEET BD1 (cont'd)

Low Noise Amplifier circuits on Service Sheet 2.

## BANDWIDTH CONTROL (V6)

The following troubleshooting will isolate a bandwidth control problem to either the Microprocessor Circuits or the Phase Lock Circuits.
On the A9 Microprocessor Board Assembly monitor the TTL logic levels at J2 pins 4,6 and 8 while changing the Lock Bandwidth Factor on the front panel. The TTL logic levels should be as shown below:

| Lock Bandwidth Factor |  |  |  | A9 Microprocessor Board |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 10 | 100 | $1 k$ |  |  |
| 0 | 0 | 0 | 0 | 1 | J2 pin 4 |
| 0 | 0 | 1 | 1 | 0 | J2 pin 6 |
| 0 | 1 | 0 | 1 | 0 | J2 pin 8 |

If the logic levels are incorrect troubleshoot the A9 Microprocessor Board Assembly. If the logic levels are correct troubleshoot the Phase Lock Circuits.

## CAPTURE CONTROL (V7)

The following troubleshooting will isolate a Capture Control problem to either the Microprocessor Circuits or the Phase Lock Circuits.
On the A9 Microprocessor Board Assembly monitor the TTL logic level at J2 pin 10 with the CAPTURE button, on the front panel, pressed and released.
The logic level should be:

$$
\begin{aligned}
& \text { Capture released }=1 \\
& \text { Capture pressed }=0
\end{aligned}
$$

If the logic level is incorrect troubleshoot the Microprocessor circuits. If the logic level is correct troubleshoot the Phase Lock Circuits.

## OUT-OF-LOCK CONTROL(V)

The following troubleshooting will isolate an Out-of-Lock Control problem to either the Microprocessor circuits or the Phase Lock circuits.

1. Connect a signal of $10 \mathrm{GHz}^{*}$ at a level of +10 dBm to the MICROWAVE TEST SIGNAL INPUT connector on the front panel.
2. Connect a signal of $400 \mathrm{MHz}^{*}$ at a level of 0 dBm to the $5-1280 \mathrm{MHz}$ INPUT connector on the front panel.
3. On the Carrier Noise Test Set select the BAND RANGE with a BAND CENTER frequency of $9.6 \mathrm{GHz}^{*}$. Press the MODE button to enable $\phi$, CW. Select a LOCK BANDWIDTH FACTOR of 100 .
4. Press and release CAPTURE, on the Carrier Noise Test Set, to phase lock the microwave source (D.U.T.) to the tunable 5 to 1280 MHz source.

If the sources do not phase lock (green bar does not remain illuminated on the front panel phase lock indicator) the tunable 5 to 1280 MHz source must be tuned closer in frequency to the IF frequency ( $f_{\text {IF }}=f_{\text {D.U.T. }}-f_{\text {band center }}$ frequency). Press CAPTURE while tuning the tunable 5 to 1280 MHz source in 1 kHz steps. Watch the phase lock indicator on the Carrier Noise Test Set. When the LED's on the indicator all light up, reduce the resolution of the tunable 5 to 1280 MHz source by a factor of 10 .

## NOTE

Connect the spectrum analyzer to the $<10 \mathrm{MHz}$ OUTPUT, on the Carrier Noise Test Set, if difficulties occur in determining the direction to tune the tunable 5 to 1280 MHz source to acquire phase lock.
The signals displayed on the spectrum analyzer represent the frequency difference between the two inputs to an internal mixer/phase detector in the Carrier Noise Test Set. The signals will decrease in frequency to dc when tuning towards phase lock and increase in frequency when tuning away from phase lock.
Press CAPTURE and tune in this reduced resolution. Watch the red LEDS on the Carrier Noise Test Set phase lock indicator step through one side of the display - to the green bar - then to the other side of the display. Again reduce the resolution on the tunable 5 to 1280 MHz source by a factor of 10 . Tune in this finer resolution until the green LED is illuminated. When the green LED is illuminated release CAPTURE.

[^10]
## SERVICE SHEET BD1 (cont'd)

5. On the A9 Microprocessor Board Assembly monitor connector J2 pin 12 with a multimeter. The microwave source and the tunable 5 to 1280 MHz source should be phase locked. When phase locked 5 volts dc should be measured at J2 pin 12.
6. Now increase the tunable 5 to 1280 MHz source by 500 kHz . The microwave source and the tunable 5 to 1280 MHz source should no longer be phase locked. Measure the voltage at J2 pin 12 again it should be 1 volt dc typically.
7. If the voltages measured at J 2 pin 12 were found to be incorrect, troubleshoot the phase lock circuits. If the voltages were correct, troubleshoot the microprocessor circuits.

## NAM (Not AM) ( $\sqrt{9}$

The following procedure will help to determine if the "not AM" control signal is being enabled by the Switch and LED Control Circuits.

1. If the "not AM" control signal is being enabled the AM, CW annunciator will be illuminated when the MODE button on the front panel is pressed.
2. If the $\mathrm{AM}, \mathrm{CW}$ annunciator will not light measure the voltage at A2J1 pin 25. A2J1 is located on the A2 assembly, which is the printed circuit board attached to the rear of the center front panel. To service the A2 assembly the center front panel is removed in the following manner:
a. Remove the plastic strip on the top of the front panel.
b. Remove the two screws that hold the top of the center front panel in place.
c. Remove the two screws that hold the bottom of the center front panel in place.
d. Pull the panel out slowly.
e. To re-install the panel reverse the steps for removing the panel.
When AM, CW is enabled the voltage measured should be +2.4 volts dc. When AM, CW is not enabled the voltage should be +4.3 volts dc.
3. If the AM, CW annunciator will not light and the voltage is incorrect troubleshoot the Switch
and LED Control Circuits. If the AM, CW annunciator will light and the voltage is correct troubleshoot the Front Panel Key and Display Board Assembly.

## N $\phi$ PU (Not Phase Pulse) $\sqrt{\sigma 10}$

The following procedure will help to determine if the "not phase pulse" control signal is being enabled by the Switch and LED Control Circuits.

1. If the "not phase pulse" control signal is being enabled the $\phi$, PULSE annunicator will be illuminated when the MODE button on the front panel is pressed.
2. If the $\phi$, PULSE annunciator will not light measure the voltage at A2J1 pin 43. A2J1 is on the A2 assembly, which is the printed circuit board located on the rear of the center front panel. To service the A2 assembly the center front panel is removed in the following manner:
a. Remove the plastic strip on the top of the front panel.
b. Remove the two screws that hold the top of the center panel in place.
c. Remove the two screws that hold the bottom of the center panel in place.
d. Pull the panel out slowly.
e. To re-install the panel reverse the steps for removing the panel.

When $\phi$, PULSE is enabled the voltage measured should be +2.4 volts dc. When $\phi$, PULSE is not enabled the voltage measured should be +4.2 volts dc.
3. If the $\phi$, PULSE annunciator will not light and the voltage is incorrect troubleshoot the Switch and LED Control Circuits. If the $\phi$, PULSE annunciator will light and the voltage is correct troubleshoot the Front Panel Key and Display Board Assembly.

## NAMPU (Not AM Pulse) (vi1

The following procedure will help to determine if the "not AM pulse" control signal is being enabled by the Switch and LED Control Circuits.

1. If the "not AM pulse" control signal is being enabled the AM, PULSE annunciator will be illuminated when the MODE button on the front panel is pressed.


SERVICE SHEET 1
REFERENCE UP-CONVERSION, TEST SIGNAL DOWN CONVERSION AND PHASE DETECTING CIRCUITS

## PRINCIPLES OF OPERATION

Service Sheet 1 provides the circuitry for converting a 10 MHz to 18
Service Sheet 1 provides the circuitry for converting a 10 MHz to 18 to 1280 MHz do not have to be down converted. These signale are input directly to the IF amplifier.
The 640 MHz IN reference signal enters the Carrier Noise Test Set The 640 MHz IN reference signal enters the Carrier Noise Test Set
from the rear panel. The level of this signal is $>+1$ dBm. This signal from the rear panel. The level of this signal is $>+1 \mathrm{dBm}$. This signal drive the comb generator. The comb generator is basically a step recovery diode. Its output is a series of signals that are spaced 640 MHz apart. An isolator prevents signals from being reflected back to the comb generator. A microwave bandpass filter is selected via comb line is then mixed with the microwave signal under test (entered from the front panel) to produce an intermediate frequency (IF) between 5 and 1280 MHz . The IF signal is amplified and fed through a power splitter. One output of the power splitter goes to the front panel IF OUTPUT connector. The other output provides one pares the IF signal to a reference signal of the same frequency from an external RF source (or the delayed IF OUTPUT) to detect the phase difference.

## 640 MHz Bandpass Filter

The purpose of this filter is to reduce any $120 \mathrm{MHz}, 520 \mathrm{MHz}$ or 760 MHz reference spurs from the 640 MHz IN signal The insertion loss is approximately 2 dB .

Power Ampllifer Assembly
After the bandpass filter, the 640 MHz signal goes into the All Power Amplifier Assembly. The power amplifier boosts the signa level to a minimum of +26.5 dBm . A level between +26.5 and +28 dBm is required to drive the comb generator. The power amplifier has an auxiliary output (AUX OUT) that is available on the rea to supply one of the drive signals ( 640 MHz ) when the 640 MHzOUT is connected to the 640 MHz IN on the rear panel using the cable attenuator assembly (HP 11729-6096 or HP 11729-60098 [Option

Comb Generator and Isolator
The next item in the chain is comb generator G1. The comb generator is a step recovery diode and uses the 640 MHz input signal to Thent 18 GHz.
The comb generator is followed by an isolator. The isolator provide

SERVICE SHEET 1 (conf'd)
lines rejected by the following band pass filters from reflecting back into the comb generator. The isolator exhibits low insertion los dB . This is not a problem, however, because the comb lines at lowe frequencies have more power than the higher frequency comb lines.

## Microwave Switches and Bandpass Filters

Following the isolator is a series of microwave switches and band pass filters. There is a microwave switch associated with each filter A standard Carrier Noise Test Set has 7 switches and 7 filters. sections may exist.
The filters select one comb line (harmonic of 640 MHz ) and reject al thers. Rejected frequencies are attenuated at least 30 dB below the selected combline. The insertion loss through the filter bank is 5 dB or less.

## Microwave Mixer (U5)

The output from the microwave bandpass filters goes to the RF port of the microwave mixer. The signal level must be a least -20 dBm . In bands 2 through 8, the microwave test signal provides the LO drive signal to the mixer. It should be at least 7 dBm , but measurements may also be done with input levels as low as $\mathbf{- 1 0} \mathbf{d B m}$ with ome potential degradation of the noise floor.
The microwave test signal is mixed with the comb line to produce an IF (difference frequency), which goes to the IF amplifier. The IF frequency is between 5 and 1280 MHz . The insertion loss of the the mixer is -33 dBm .
In band 1, the microwave test signal bypasses the microwave mixer and goes to the IF amplifier directly. The optimum microwave test bands 2 through 8.) Slightly degraded phase noise performance ccurs with greater than 2 or 3 dBm into the microwave test signal ort because of the action of the limiters inside the IF amplifier

IF Amplifier Assembly
The IF amplifier boosts the signal level up to at least 14 dBm . This ignal drives the LO port of the mixer/phase detector.. The fresignal drives the
quency into the amplifier ranges from 5 to 1280 MHz .

## Power Splitter and Mixer/Phase Detector

The output of the IF amplifier goes to a power splitter. The purpose of the power splitter is to provide an IF output to the front panel. This output is identical in level to the other signal coming out of the plitter, which drives the LO port 1 the mixer/phase delector. This level is specified to be at least $+7 \mathbf{d B m}$.

SERVICE SHEET 1 (cont'd)
The RF input to the mixer/phase detector, 5 to 1280 MHz , is entered via the front panel. For mea urements, the typical level is 0 dBm ; for calibre tion, a lower level signal is used. The lower leve ignal is used during calibration so the Low Nois Amplifier is not overdriven. In phase noise mee urement mode (Phase Detector Method), the mixer phase detects the RF and LO signals and outputs mixer/phase detector has the baseband noise superimposed on it.
The output of the mixer/phase detector goes to the A3 Low Pass Filter Board Assembly, covered on Phase Lock Board Assembly, covered on Service Sheet 3.

## aM Option (Option 130 )

The AM option (Option 130) measures AM noise instead of phase noise. This option bypasses the microwave mixer and takes the microwave tes se dictor Board Assembly, shown on Service Sheet 2.

## TROUBLESHOOTING

Troubleshooting procedures are listed on the schematic.

## Test Equipment

Microwave Synthesized Source .......HP 8340A
RF Synthesized Signal Generator.......HP 8662A
Power Meter .........................HP 436A
Oscilloscope .............................HP 1740A



SERVICE SHEET 2 (contra)



Low Noise Amplilier Assembly
Generai. The Low Noise Amplifier Assembly consisits of a pre
gmplifier and a owewe



 $E 1$ and E 2 (on the base of $Q 1$ and $Q$, respectively) prevent secille
 the frequency reponge that would otherwiee be lopst beacase of the
inductance of the path, thus fattening the gain beyond 20 MHz
 cascode amplific
of 01 and $\mathrm{Q}_{2}$ ?




## oubleshootina


Test Equipment
 Oscillosocope
Digital Mulimeter

ERVICE SHEET 2 (contrd)
LOW NOISE AMPLIFIER ASSEMBLY TROUBLESHOOTIN Connet $\mathbf{1}$. 640 MHz peecturally pure eignal to the 660 MHz rear
2. Connect 10GHzsyntheized dignal ata a levelof $1+10$ dBm othe INPUT connector on the front
3. Connecta 40.1 MHz synthesized dignal ata a evel of- 40 dBm to
4. Set the Carrier Noise Test Set as follows:

Meagrement mode e................ CW
BAND Range
.............3
to
10.88 GH
Remove the top cover of the Carrier Noise Test Sel
6. Disconnect the input cable e (Wio) th the Low Noise Amplifer:
7. Verify that there is 1 io kHz beat onte. Adiast the pectrum he input power level 1 othe Low Noise Amplifere shoulabe:-4
 Reconnect the input cable (W10) to the Low Noise Amplififer
9. Connect the output connector (J)2) on the Low Noise A Amplifiert Noise Amplifierer The outuut powe The outpot power level of
folows
-8 dBm typical
the output power level mensured is the typical value the Low
2. Turn off the Carrier Noise Test Set. Connect an SMC ( 550 obm termination



SERVICE SHEET 2 (contd)
12. Measure the voltage peak topepak at TP1 and TP4 uaing an $\mathfrak{c c c}$
Use the voltages measurred to isolate the failure to a particular


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| :---: | :---: |
| ${ }^{91}$ | ${ }^{\text {+ } 7.6 .6 \mathrm{Vdc}}$ |
| ${ }_{83}^{82}$ |  |
| ${ }^{\text {Q }}$ |  |
| ${ }_{97}^{96}$ |  |
| ${ }_{8} 8$ | +13.1. vdc |
| ¢99 | +11. ${ }_{\text {vde }}$ <br> +11.0 vdc |

FRONT PANEL KEV AND DISPLAY BOARD
ASSEmBLY TROUBLESHOOTING The foliowwing table can be wesed to verity proper operation of the $A$ Proni Parned on using the MODE awich on the front anane the the ypical tranasistor voltages should be as showi the the below





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SERVICE SHEET 3 (contid)
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Comparatot When CAPTURE i.p preaed, the microporocesor seadi




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overe the range of the amplified oigional from the mixecer phase
 bock loop (if reequered).
Thendromth conotrol

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A I Iadicatoi Baoard Assembiby

and R2eeth



oubleshooting

Test Eaupment

Connect the following tese set vas ahown.




Set hef function generatur sa solows:
Wave forms Sine wave

Set the Carier Noise Test Sec as Sollow.

Tuna the Carier Noiere Tees Se off and remove the top cover

3. On the A5 Phase Lock Board Aseembly puta shortacriose ACCL

5. On the oscillosecpe set the coupling control, for channel one to
6. Adiust the evel of the finction generator for 5 VPp as read on

1. On the oscillosocope set channet two $t$ DC coupling.
2. Connect channel two to Test Point 1on the A5 Phase Lock
3. Adjust the DC Cffose on the function generator to center the
4. Measure the typical peakk top peak voltagesat T Test Points $1,2,3$


senvice shetr 3 (conta)

## 



| Copure butan | Implat Peateratel voluge |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | aspr | asim | astr |  |
| Presead | sv | sv | ${ }^{\text {ev }}$ |  |

12. Using channel one est the e evel of of he fucction generator to 0
mpop
000
13. Set the LOCKK BANDWIDTH FACTOR, on the front panel, to

14. Adjust the DC of fitat on the function generator to center the




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## service sheet (conird)



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Figure 8-14. HP-IB Interconnect Board Assembly Component Locations


Figure 8-15. Front Panel Key and Display Board Assembly Component Locations






## SERVICE SHEET 5 (cont'd)

Table 8-7. Signatures for Verifying Microprocessor, ROM, RAM and Data Buffer Operation

| Pin | U3 | U4 | U5 | U7 | 48 | U16 | 017 | 418 | U36 | 437 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 5A86 | - | - | - | H826 | UHU1 | - | 0000 | UHU1 | UHU1 |
| 2 | 60H5 | U9U8 | - | - | AF9P | - | - | H826 | 8AFA | 7997 |
| 3 | 00H6 | 5A86 | - | - | 00H6 | - | - | UHU1 | 3915 | 718H |
| 4 | AF9P | 60H5 | - | - | 3A56 | - | - | CP56 | 55F6 | 91C9 |
| 5 | H826 | 00H6 | - | - | - | 1 HCU | - | - | 630C | FH20 |
| 6 | CP56 | AF9P | 0000 | - | - | 1HCU | - | 1P44 | 9U26 | HA4H |
| 7 | 1P44 | H826 | - | - | - | F69F | - | - | 4A9C | HCAH |
| 8 | 9900 | CP56 | 9900 | - | - | 4732 | P04P | 9900 | 6386 | 5U7U |
| 9 | 7997 | 1 P 44 | 1 P 44 | - | - | 2567 | - | - | 83F2 | C8H9 |
| 10 | 718N | 9900 | CP56 | - | - | 4A99 | UHU1 | - |  |  |
| 11 | 91C9 | 7997 | H826 | - | - | U9U8 | UHU1 | - | 83F2 | 83F2 |
| 12 | - | 718H | AF9P | P04P | - | - | - | 9900 | 6386 | 6386 |
| 13 | FH20 | 91C9 | 00H6 | UHU1 | 1 HCU | 0000 | 1HCU | - | 4A9C | 4A9C |
| 14 | HA4H | - | 60H5 | - | 3361 | - | - | 1P44 | 9U26 | 9U26 |
| 15 | HCAH | FH20 | 5A86 | - | 6978 | $2 \mathrm{PC1}$ | - | - | 630C | 630C |
| 16 | 5U7U | HA4H | C320 | - | - | 1HCU | - | CP56 | 55F6 | 55F6 |
| 17 | C8H9 | HCAH | ACUH | - | - | 1HCU | - | UHU1 | 3915 | 3915 |
| 18 | 4C46 | 5U7U | 1HU2 | - | - | - | - | H826 | 8AFA | 8AFA |
| 19 | 1HU2 | C8H9 | 2567 | - | - | - | - | 0000 | - | - |
| 20 | P04P | 2 PC 1 | U9U8 | - | - | 4C46 | - | - | - | - |
| 21 | UHU1 | - | 4A99 | - | - | 3A56 | - | - | - | - |
| 22 | ACUH | - | 4732 | - | - | 1HCU | - | - | - | - |
| 23 | C320 | - | F69F | - | - | FP0F | - | - | - | - |
| 24 | - | - | 83F2 | - | - | - | - | - | - | - |
| 25 | - | - | 6386 | - | - | - | - | - | - |  |
| 26 | - | - | 4A9C | - | - | - | - | - | - |  |
| 27 | - | - | 9U26 | - | - | - | - | - | - | - |
| 28 | - | - | 630C | - | - | - | - | - | - | - |
| 29 | - | - | 55F6 | - | - | - | - | - | - | - |
| 30 | - | - | 3915 | - | - | - | - | - | - | - |
| 31 | - | - | 8AFA | - | - | - | - | - | - | - |
| 32 | - | - | UHU1 | - | - | - | - | - | - | - |

Turn the Carrier Noise Test Set off and disconnect the Timing Pod.

Reset the Diagnostic Switch A9S2 to the Normal Operation position shown below:

| Diagnostic Switch S2 | Normal Operation Logic Level |
| :---: | :---: |
| 1 | 1 |
| 2 | 1 |
| 3 | 1 |
| 4 | 1 |



Figure 8-18. HP-IB Interconnect Board Assembly Component Locations


| SERVICE SHEET 6 <br> PRINCIPLES OF OPERATION |  |
| :---: | :---: |
| Genoral |  |
| The switch and LED control circuits perform tha. decode addresses of latches,b. load data from data bus into latches, andc. drive front panel LEDs. |  |
|  |  |
| Smumen Dorwer Enate Llect |  |
|  |  |
|  |  |
|  |  |
|  |  |
| Switch Relay Driver Latches <br> Latches U25 and U26 store data for the relays. These latches turn on and off |  |
|  |  |
| These drivers generateswitches (see Service Sh |  |
| Dlagnostic LED Latch <br> U27 drives DS1 and DS2. The individual LEDs within DS1 and DS2 are numbered <br> DO-D7. D7 is closest to the hinged portion of the Microprocessor The LEDS Lhard An |  |
|  |  |
|  |  |
| setting of the diagnostfor an explanation of thin the following table. |  |
| aremat | Maxal |
| mureat |  |
| $\begin{aligned} & \text { ROM Test } \\ & \text { Signature Analysis } \\ & \text { Self Test (power-up) } \end{aligned}$ | DStion end daloh |
|  |  |
|  |  |
|  |  |

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## SERVICE SHEET 6 (cont'd)

Table 8-10. Signatures Verifying Microprocessor and Relay Circuitry Operation (2 of 3)

| Pin | U25 | U26 | U27 | U29 | U30 | U31 | U38 | U41 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | H344 | 3819 | $79 C 0$ | $28 H 1$ | HUC9 | 2077 | UHU1 | AHFC |
| 2 | UF5F | $673 F$ | - | - | - | - | 9130 | - |
| 3 | 9130 | 9130 | 9130 | - | - | - | 7097 | - |
| 4 | 8A90 | 8A90 | 8 A90 | - | - | - | $8 A 90$ | - |
| 5 | F4U9 | 28 H 1 | - | - | - | - | HPCP | - |
| 6 | HP61 | 2F86 | - | 356 P | F206 | 3HF8 | HUH9 | C074 |
| 7 | HUH9 | HUH9 | HUH9 | - | - | - | 586A | - |
| 8 | PPF7 | PPF7 | PPF7 | - | - | - | PPF7 | - |
| 9 | 4H18 | H10U | - | - | - | - | 1P1U | - |
| 11 | - | - | - | - | - | - | $83 F 2$ | - |
| 12 | F5H3 | 8494 | - | - | - | - | 6386 | - |
| 13 | 1P1U | 1P1U | 1P1U | - | - | - | 4A9C | - |
| 14 | 586A | $586 A$ | $586 A$ | - | - | - | 9 U26 | - |
| 15 | A55P | HUC9 | - | - | - | - | $630 C$ | - |
| 16 | 09AA | 2077 | - | - | - | - | 55F6 | - |
| 17 | HPCP | HPCP | HPCP | - | - | - | 3915 | - |
| 18 | 7097 | 7097 | 7097 | - | - | - | 8AFA | - |
| 19 | 5C41 | AHFC | - | - | - | - | U585 | - |

Table 8-10. Signatures Verifying Microprocessor and Relay Circuitry Operation (3 of 3)

| Pin | U42 | U43 | U44 | U47 | U48 | U49 | U50 | U54 | U55 | U56 | U57 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | UF5F | 8494 | - | - | - | - | - | 09AA | F4U9 | 673F | 5C41 |
| 2 | - | - | - | 9130 | 9130 | 9130 | 9130 | - | - | - | - |
| 3 | - | - | 09AA | - | - | - | - | - | - | - | - |
| 4 | - | - | 1415 | 7097 | 7097 | 7097 | 7097 | - | - | - |  |
| 5 | - | - | F4U9 | - | - | - | - | - | - | - | - |
| 6 | P1P3 | 992C | H946 | 8A90 | 8A90 | 8A90 | 8A90 | 1415 | H946 | 7A83 | 46UP |
| 8 | - | - | 46UP | - | - | - | - | - | - | - | - |
| 10 | - | - | 7A83 | HPCP | HPCP | HPCP | HPCP | - | - | - | - |
| 11 | - | - | 673F | - | - | - | - | - | - | - | - |
| 12 | - | - | 992C | HUH9 | HUH9 | HUH9 | HUH9 | - | - | - | - |
| 13 | - | - | 8494 | - | - | - | - | - | - | - | - |
| 14 | - | - | - | 586A | 586A | 586A | 586A | - | - | - |  |

Turn the Carrier Noise Test Set off. Disconnect the Timing Pod.
Reset the Diagnostic Switch S2 to the normal operation position shown as follows:

| Diagnostic Switch S2 | Normal Operation Logic Level |
| :---: | :---: |
| 1 | 1 |
| 2 | 1 |
| 3 | 1 |
| 4 | 1 |



Figure 8-21. Front Panel Key and Display Board Assembly Component Locations


## SERVICE SHEET 7

## POWER SUPPLY CIRCUITS

## PRINCIPLES OF OPERATION

## General

The Carrier Noise Test Set requires four power supply voltages $+24 \mathrm{~V},+15 \mathrm{~V},+5 \mathrm{~V}$, and -15 V . The transformer supplies all the secondary voltages for the power supply. The secondary is wound as one coil and is center tapped. All the power supplies take the sam form. They have a fil-wave bridge rectifir thatconsists of 2 rectify a cuit and an indicator that lights when that powe supply is on

## +24V Power Supply

The output of the voltage regulator is dependent on the reference voltage which is set with R11 and R12

The overvoltage protection circuit consists of a zener diode (VR2) in series with a standard rectifying diode (CR9). When the voltag across VR2 exceeds the threshold of 30 volts, the zener diode turn on. CR11 protects against any reverse voltages that may be applied or negative voltages that may get on the supply line. It protects not only the power supply but also any circuits that may be connected to the +24 V supply
The +24V supply runs the A6 Low Noise Amplifier Assembly and all the microwave switches ( see Service Sheet 1)
+15V Power Supply
There are two +15 volt supplies: one supply is used for the A5 Phase Lock Board Assembly and the A10 IF Amplifier; the other supply is for the A11 Power Amplifier Assembly. Due to higher sensitivity to dc bias noise, the power amplifier needs a separate +15 volt supply.
The supply that consists of U5, Q5 and associated components is used to bias the Power Amplifier. R35 and VR10 set a reference volage for U. R34 and C23 fiter that reference voltage mainly to maintain a constant +15 volts at the emitter of Q5. Q5 is a current ource for the Power Amplifier since U5 cannot supply the neces sary current needed by the Power Amplifier L2 and C19 form a filter; it filters both noise and line spurs. CR15 supplies neg ative voltage protection.

The overvoltage protection circuit (for both supplies) consists of R14, R15, VR3 and Q3. The zener diode(VR3) begins to conduct if the voltage exceeds the threshold of 16 volts. Enough current is drawn through R15 to cause the SCR (Q3) to begin conducting. This blows the +15 volt supply fuse. It may also blow the fuse of any other supply that may be connected to the 15 V supply. CR12 protects Phase Lock Board Assembly and the A10 IF Amplifier Assembly

Switch and LED Control Circuits

## SERVICE SHEET 7 (cont'd)

## +5V Power Supply

The +5 V supply has a 2 -diode rectifier configuation. It uses a large TO-3 dual rectifier, which is part of the heat sink assembly.
The voltage regulator is adjustable. The voltage reference is set by R9, CR8, R10, and R13. Adjustment R10 is provided to set the regulator very close to +5 V , which is necessary for the digital circuits.

The overvoltage protection circuit is similar to one used for the +15 V supply

The +5 V supply is the digital supply and is used only on the A9 Microprocessor Assembly.

## -15V Power Supply

Following the 2 diode rectifier is an overvoltage protection circuit for the entire instrument. This circuit protects against incorrect line voltages. For circuit protects against incorrect line voltages. For example, if high voltage, such as 220 or 240 V , is
plugged in when the line card is set for 100 V or plugged in when the line card is set for 100 V or
120 V , this circuit will cause the fuse( F 1 ) to blow. If any voltage above 150 Vrms appears on the input to the transformer, this circuit will cause Q4 to begin conducting. This, in turn, blows the main fuse.

The overvoltage protection circuit for the -15 V supply is similar to the one used for the +24 V supply.

The -15 V supply provides voltage to the A 5 Phase Lock Board assembly and the fan.

## TROUBLESHOOTING

As an aid in troubleshooting the Power Supply typical input voltages to the voltage regulators have been placed on the schematic. The voltages are dependent on the line voltage.

## Test Equipment

Digital Multimeter HP 3456A

The tolerance of each of the voltage regulators is shown in the following table.

| Voltage Regulator | Voltage Tolerance |
| :---: | :---: |
| U1 TP4 | $-15 \mathrm{~V} \pm .5 \mathrm{~V}$ |
| U2 TP3 | $+5 \mathrm{~V} \pm .25 \mathrm{~V}$ |
| U3 TP2 | $+15 \mathrm{~V} \pm .5 \mathrm{~V}$ |
| U4 TP1 | $+24 \mathrm{~V} \pm .5 \mathrm{~V}$ |



## APPENDIX A Phase Noise Measurement Correction Factors

Once the phase noise measurement system is set up, calibrated and the signal at the NOISE SPECTRUM OUTPUT is measured on a spectrum analyzer, correction factors are added to express the output in terms of $\mathcal{L}(\mathrm{f}) . \mathcal{L}(\mathrm{f})$ is defined as follows:

$$
\mathcal{L}(\mathrm{f})=\frac{\text { power density (in one phase modulation sideband) }}{\text { total signal power }}
$$

This appendix explains the correction factors, that are summed with the measured noise level to give the actual amount of phase noise.

## NORMALIZATION TO 1 Hz EQUIVALENT NOISE BANDWIDTH

A spectrum analyzer's resolution bandwidth is not necessarily equivalent to the noise bandwidth. It is possible for a spectrum analyzer to have a resolution bandwidth which equals the noise bandwidth. The Fast Fourier Transform (F.E.T.) spectrum analyzer is one example where the resolution bandwidth of the spectrum analyzer equals the noise bandwidth. The noise bandwidth is defined as the bandwidth of an ideal rectangular filter having the same power response as the actual IF filter in the spectrum analyzer. The definition of $\mathcal{L}(f)$ requires normalization of the single sideband phase noise to an equivalent 1 Hz noise bandwidth. For a first approximation, most Hewlett-Packard spectrum analyzers have a noise bandwidth approximately 1.2 times the nominal 3 dB resolution bandwidth setting. Therefore the resolution bandwidth multiplied by 1.2 is the equivalent noise bandwidth.

The equivalent noise bandwidth is expressed as a 1 Hz equivalent noise bandwidth by using the relationship shown below:

Correction factor to convert the spectrum analyzer's resolution bandwidth to a 1 Hz equivalent noise bandwidth $=10 \log [(\mathrm{BW} \times 1.2) / 1 \mathrm{~Hz}]$.
where: BW is the resolution bandwidth in Hz that the spectrum analyzer is set to during the measurement.

Therefore, the resolution bandwidth used to make the phase noise measurement is normalized to a 1 Hz equivalent noise bandwidth by the following equation:

Correction factor to convert the spectrum analyzer's resolution bandwidth to a 1 Hz equivalent noise bandwidth $=10 \log (\mathrm{BW} \times 1.2)$.

The 1 Hz equivalent noise bandwidth correction is then subtracted from the measured noise level.

This correction factor is for Hewlett-Packard spectrum analyzers only. If another spectrum analyzer is being used, the noise bandwidth of that spectrum analyzer will have to be determined. The 1 Hz equivalent noise bandwidth can then be calculated, for the resolution bandwidth being used to make the phase noise measurement.

## NOTE

For best accuracy, the equivalent noise bandwidth should be measured. Hewlett-Packard has an application note that describes how to measure the equivalent noise bandwidth. To receive the application note order AN 150-4 using part number HP 5952-1147.

## CALIBRATION ATTENUATION

The response of the system (Mixer/Phase Detector, Low Pass Filter and Low Noise Amplifier) is calibrated before each phase noise measurement. The 5 to 1280 MHz input is offset from the frequency of the IF output (signal under test minus the center frequency of the Band Range chosen). This produces a beat note signal at the NOISE SPECTRUM OUTPUTS. From this beat note signal, the mixer/phase detector constant $\mathrm{K} \phi$ is determined. $\mathrm{K} \phi$ is the slope of the sine wave at the zero crossings.
Attenuation is added during the calibration process to avoid overloading the Low Noise Amplifier (LNA) or the baseband spectrum analyzer. The LNA is designed to amplify lower level signals, not high level beat notes. Also, best accuracy is obtained if the spectrum analyzer settings are not changed during calibration and measurement. This can be accomplished by setting the attenuation, so the noise floor will be in the upper portion of the spectrum analyzer display.
The amount of attenuation added in the R path ( 5 to 1280 MHz signal) of the mixer/phase detector is translated to the output. Thus, the attenuation applied to the 5 to 1280 MHz input reduces the mixer/phase detector output by that amount. After calibration the attenuation is removed and a noise measurement is made. The amount of attenuation added during calibration must be subtracted from the measured noise level.

## £ (f) CONVERSION FACTOR

Two signals at identical frequencies and nominally 90 degrees out of phase (known as phase quadrature) are input to the mixer/phase detector. At quadrature, the output spectrum of the mixer/phase detector is the sum of the inputs, which is filtered out, and a dc signal with a small fluctuating ac voltage. The small fluctuating ac voltage is linearly proportional to the fluctuating phase difference between the input signals.
The mixer/phase detector has a conversion factor, $\mathrm{K}_{\phi}$ that is called the phase detector constant. This $K \phi$ factor is the ratio of the ac voltage fluctuations, out of the mixer/phase detector, and the phase fluctuations between the two signals input to the mixer/phase detector.
A beat note condition is set up during calibration for use in determining the $K \phi$ phase constant or V peak. The value of $\mathrm{K} \phi$ is equal to the slope of the sine wave output from the mixer/phase detector when a beat note is present. The slope of a sine wave at the zero crossings is equal to the peak amplitude of the signal. A spectrum analyzer measures the root mean square value of a signal instead of the peak amplitude. The equation "V peak = $\sqrt{2} \times \mathrm{V}$ rms" is used to correct the spectrum analyzer reading. The preceding equation expressed logarithmically to correspond to the power readings on the spectrum analyzer is as follows:

$$
\begin{aligned}
10 \log \left(\mathrm{~V}_{\text {peak }}\right)^{2} & =10 \log \left(\sqrt{2} \mathrm{~V}_{\mathrm{rms}}\right)^{2} \\
& =10 \log \mathrm{~V}_{\text {rms }}{ }^{2}+10 \log (\sqrt{2})^{2} \\
& =10 \log \mathrm{~V}_{\text {rms }}{ }^{2}+3 \mathrm{~dB}
\end{aligned}
$$

The logarithmically expressed equation shows that the spectrum analyzer display is 3 dB less than the peak signal. Since $\mathcal{L}(\mathrm{f})$ is the ratio of the power in one phase modulation side band to the power in the carrier, 3 dB is subtracted from the noise power level on the spectrum analyzer display.
When the two inputs to a mixer are in phase quadrature and the sum product is filtered out, the mixer operates as a phase detector. All energy in the phase modulated sidebands is detected by the mixer. The detected phase modulation sidebands represent the phase modulation on the test signal (to within 0.2 dB ) when the following condition is met:

The energy in the phase modulation sidebands of the reference signal, is at least 15 dBm lower, than the energy in the phase modulation sidebands of the test signal.

## NOTE

When the noise of the reference signal is less than $15 d B$ below the test signal, the measurement error will have to be determined. To determine the measurement error, use the following formula:

$$
\operatorname{error}(d B)=10 \log \left(1+\operatorname{antilog} \frac{\mathcal{L}_{r e f}-\AA_{d u t}}{10}\right.
$$

$\mathcal{\delta}_{\text {ref }}=$ noise power of the reference
$\mathcal{£}_{\text {dut }}=$ noise power of the device under test
The error has been tabulated in the following table for several values of the noise power differences.

| $\mathcal{L}_{\text {dut }}-\mathcal{L}_{\text {ref }}(d B)$ | 0 | 1 | 2 | 3 | 4 | 5 | 10 | 15 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| correction $(d B)$ | 3.0 | 2.5 | 2.1 | 1.8 | 1.5 | 1.2 | 0.4 | 0.2 |

The output of the mixer is then the spectral density of the phase modulation sidebands on the test signal frequency which is called $S \phi(f)$. A more familiar quantity is the ratio of the energy in one phase modulating sideband to total power in the test signal, $\mathcal{L}(f)$. To convert from $S \phi(f)$ to $\mathcal{L}(f)$ we use the following equation:

$$
\mathcal{L}(\mathbf{f})=1 / 2 \mathrm{~S} \phi(\mathbf{f})
$$

Therefore another 3 dB is subtracted from the measured noise power level.
The total $\mathcal{L}(\mathrm{f})$ conversion factor is -6 dB . For the $\mathcal{L}(\mathrm{f})$ conversion factor subtract 6 dB from the measured noise level.

## CORRECTION FOR LOG AMPLIFIERS AND PEAK DETECTORS IN ANALOG SPECTRUM ANALYZERS

The spectrum analyzer's detection system is optimized for sine waves; for noise measurements some corrections must be made. In most analog spectrum analyzers there is a log amplifier followed by a peak detector. A peak or envelope detector used to measure random noise results in a reading lower than the true rms value of the average noise (typically about 1.05 dB lower). The $\log$ shaping tends to amplify noise peaks less than the rest of the noise signal, resulting in a detected signal which is smaller than its true rms value. The correction for the log display mode combined with the detector characteristics gives a total correction for Hewlett-Packard analog spectrum analyzers of 2.5 dB . The correction of 2.5 dB is added to any random noise measured in the log display. For spectrum analyzers other than those made by Hewlett-Packard, the correction factor for the log amplifier and peak detector will have to be determined.

## FREQUENCY DISCRIMINATOR CORRECTION FACTOR

The frequency discriminator method outputs a voltage variation proportional to the frequency deviations of the signal under test. The proportionality of the discriminator output changes linearly with frequency offsets from the carrier. Calibration is performed at one modulating frequency to find the sensitivity of the discriminator. The discriminator output is then normalized for all modulating frequencies with the following equation:

Correction to convert frequency fluctuations at any offset to $\mathcal{L}(f)=-20 \log \left(f_{\text {off }} / f_{\text {cal }}\right)$ where:
$f_{\text {cal }}$ is the modulating frequency used to calibrate the frequency discriminator.
$\mathrm{f}_{\text {off }}$ is the modulating frequency where the phase noise information is desired (offset frequency from the carrier).

## FREQUENCY DISCRIMINATOR CORRECTION FACTOR (cont'd)

After the frequency discriminator is calibrated at one frequency ( $f_{\text {cal }}$ ) and the phase noise information is measured at the desired offset frequency from the carrier ( $\mathrm{f}_{\text {off }}$ ), the correction factor is calculated. Insert the calibration frequency ( $f_{\text {cal }}$ ) and the modulating frequency offset ( $\mathrm{f}_{\text {off }}$ ) into the above equation. Sum this quantity with the measured noise level.

## APPENDIX B Phase Lock Loop Characterization

A Phase Lock Loop forces the voltage controlled oscillator (VCO) to phase-track the reference for frequency offsets less than the bandwidth of the Phase Lock Loop. This tracking inside the phase lock loop bandwidth results in suppression of phase noise at the output of the phase detector. This property normally limits a phase noise measurement to offsets from the carrier greater than the loop bandwidth. However, the Carrier Noise Test Set enables the Phase Lock Loop to be characterized. When the phase lock loop is characterized the bandwidth of the phase lock loop and the amount of noise suppression within the phase lock loop can be determined.

The Carrier Noise Test Set's Loop Test Port Input allows a signal-for example, a random noise source, a tracking generator or a variable frequency sine wave-to be applied to the loop. Then, by measuring the response of the loop to the signal being input, the transfer characteristic of the phase lock loop can be determined. During characterization, the VCO and reference remain locked and in quadrature; that is, the loop is characterized in the same state that it was in during the phase noise measurement.

The characterized phase lock loop yields two important pieces of information, the phase lock loop bandwidth and the amount of noise suppression within the phase lock loop. The loop bandwidth designates the offset frequencies for which an uncorrected phase noise measurement can be made. The measured loop noise suppression versus offset frequency is used to correct the value of noise measured on the device under test, when the measurement was made inside the loop bandwidth.

## PROCEDURE

The following discussion describes two methods for determining the loop transfer characteristic of the phase lock loop.

Use the following procedure when the signal input at the LOOP TEST PORT IN connector is from a random noise source or a tracking generator:

1. Calculate the nominal loop bandwidth using one of the following formulas. The formula used will depend on the method used for phase locking.
nominal loop bandwidth $=\frac{\mathrm{LBF} \times \mathrm{f}_{\text {dut }}}{10^{10}}$
(Using the 10 MHz crystal oscillator, that drives the 640 MHz reference, for phase locking. The crystal must have a tuning range
of one (1) part in $10^{7} \mathrm{~Hz}$.)
nominal loop bandwidth $=\frac{\text { LBF } \times \text { FM peak deviation }}{10^{3}}$
(Using the DC-FM of the 5 to 1280 MHz tunable source for phase locking)

$$
\begin{aligned}
& \text { LBF = Lock Bandwidth Factor } \\
& \mathrm{f}_{\text {dut }}=\text { Frequency of device under test }
\end{aligned}
$$

With the nominal loop bandwidth known it will be easier to set the controls on the spectrum analyzer to view the loop transfer characteristic.
2. When determining the loop transfer characteristic, the loop must be in the same condition it was in when the phase noise measurement was made. For example, the loop should be locked and in phase quadrature; the Lock Bandwidth Factor must be set to the same position it was set to during the phase noise measurement.
3. Using a random noise source or tracking generator, input a signal at the LOOP TEST PORT IN connector, on the rear panel of the Carrier Noise Test Set. Adjust the input level, so the front panel phase lock indicator displays the center green LED with a red LED on either side.
4. Connect the LOOP TEST PORT OUT connector, on the rear panel of the Carrier Noise Test Set, to a spectrum analyzer with an appropriate frequency range and bandwidth. Adjust the spectrum analyzer controls, such as frequency span, to view the loop transfer characteristic. The nominal loop bandwidth, calculated in step 1, should give a good indication of where to set the frequency span.
5. Determine the amount of noise suppression using the following example:

Figure D-1 shows a typical phase lock loop transfer characteristic, with a bandwidth of about 90 Hz . At a 10 Hz offset, the loop suppresses the noise 20 dB . Prior to adding the signal, the device under test yielded a noise measurement of $-90 \mathrm{dBc} / \mathrm{Hz}$ at 10 Hz . The loop noise suppression correction is added to this number, yielding the actual phase noise of the device under test at a 10 Hz offset:
measured noise level: $\quad-90 \mathrm{dBc} / \mathrm{Hz}$
loop suppressed noise:
actual noise level: $\quad \overline{-70 \mathrm{dBc} / \mathrm{Hz}}$


Figure B-1. Typical Phase Lock Loop Filter Transfer Characteristic.

## PROCEDURE

Use the following procedure when the signal input at the LOOP TEST PORT IN connector is from a signal source that does not track the spectrum analyzer.

1. Calculate the nominal loop bandwidth using one of the following formulas. The formula used will depend on the method used for phase locking.
nominal loop bandwidth $=\frac{L B F \times f_{\text {dut }}}{10^{10}}$
(Using the 10 MHz crystal
oscillator, that drives the 640 MHz reference, for phase locking. The crystal must have a tuning range of one (1) part in $10^{7} \mathrm{~Hz}$.)
nominal loop bandwidth $=\frac{\text { LBF } \times \text { FM peak deviation }}{10^{3}}$
(Using the DC-FM of the
5 to 1280 MHz tunable
source for phase locking)
LBF = Lock Bandwidth Factor
$f_{\text {dut }}=$ Frequency of device under test
With the nominal loop bandwidth known it will be easier to set the controls on the spectrum analyzer to view the loop transfer characteristic.
2. When determining the loop transfer characteristic, the loop must be in the same condition it was in when the phase noise measurement was made. For example, the loop should be locked and in phase quadrature; the Lock Bandwidth Factor must be set to the same position it was set to during the phase noise measurement.
3. Using the signal source, input a signal at the LOOP TEST PORT IN connector, on the rear panel of the Carrier Noise Test Set. Adjust the input level, so the front panel phase lock indicator displays the center green LED with a red LED on either side.
4. Connect the LOOP TEST PORT OUT connector, on the rear panel of the Carrier Noise Test Set, to a spectrum analyzer with an appropriate frequency range and bandwidth.
5. Plot the loop transfer characteristic by taking point to point readings starting at 0 Hz and going out to the loop bandwidth limit. The offset from point to point is up to the user. The spectrum analyzer may have to be adjusted each time a reading is taken for best accuracy.
6. Determine the amount of noise suppression using the following example:

Figure B-1 shows a typical phase lock loop transfer characteristic, with a bandwidth of about 90 Hz . At a 10 Hz offset, the loop suppresses the noise 20 dB . Prior to adding the signal, the device under test yielded a noise measurement of $-90 \mathrm{dBc} / \mathrm{Hz}$ at 10 Hz . The loop noise suppression correction is added to this number, yielding the actual phase noise of the device under test at a 10 Hz offset:

$$
\begin{array}{ll}
\begin{array}{l}
\text { measured noise level: } \\
\text { loop suppressed noise: } \\
\text { actual noise level: }
\end{array} & -90 \mathrm{dBc} / \mathrm{Hz} \\
{ } } \\
\hline-70 \mathrm{dBc} / \mathrm{Hz}
\end{array}
$$


[^0]:    ${ }^{1}$ For a complete explanation of the correction factors see Appendix A.
    ${ }^{2}$ See Appendix B to determine the phase lock loop transfer characteristic and the amount of loop noise suppression.

[^1]:    ${ }^{1}$ For a complete explanation of the correction factors see Appendix A.

[^2]:    ${ }^{1}$ For a complete explanation of the correction factors see Appendix A.

[^3]:    *Because of the power requirements of the internal mixer, the upper and lower ends of the bands with center frequencies of 14.72 GHz and 17.28 GHz are verified to be within specified limits. The comb generator's output power is lowest at the higher 640 MHz harmonics.

[^4]:    ${ }^{2}$ For a complete explanation of the correction factors see Appendix A.

[^5]:    ${ }^{2}$ For a complete explanation of the correction factors see Appendix A.

[^6]:    ${ }^{2}$ For a complete explanation of the correction factors see Appendix A.

[^7]:    ${ }^{2}$ For a complete explanation of the correction factors see Appendix A.

[^8]:    ${ }^{2}$ For a complete explanation of the correction factors see Appendix A.

[^9]:    *Use the following procedure if the 9.6 GHz BAND CENTER frequency is not installed:
    -Select an available BAND RANGE.
    -Set the microwave source to 400 MHz above the BAND CENTER frequency of the BAND RANGE selected.
    -The tunable 5 to 1280 MHz source is left set to 400.01 MHz .

[^10]:    *Use the following procedure if the 9.6 GHz BAND CENTER frequency is not installed:

    - Select an available BAND RANGE.
    - Set the microwave source to 400 MHz above the BAND CENTER frequency of the BAND RANGE selected.
    - The tunable 5 to 1280 MHz source is left set to 400 MHz .

